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MHD (SWCNTS + MWCNTS)/H₂O-Based Williamson Hybrid Nanofluids Flow Past Exponential Shrinking Sheet in Porous Medium

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ABSTRACT

The present study numerically investigates the flow and heat transfer of porous Williamson hybrid nanofluid on an exponentially shrinking sheet with magnetohydrodynamic (MHD) effects. The nonlinear partial differential equations which governed the model are first reduced to a set of an ordinary differential equations by using the similarity transformation. Next, the BVP4C solver is applied to solving the equations by considering the pertinent fluid parameters such as the permeability parameter, the magnetic parameter, the Williamson parameter, the nanoparticle volume fractions and the wall mass transfer parameter. The single (SWCNTs) and multi-walled carbon nanotubes (MWCNTs) nanoparticles are taken as the hybrid nanoparticles. It is found that the increase in magnetic parameter in SWCNT + MCWNT hybrid nanofluid results to the increase of 72.2% on skin friction compared to SWCNT nanofluid while maintaining reducing a small number of Nusselt number. This shows the potential of the Williamson hybrid nanofluid as a friction application purposes especially in transportation like braking system, flushing fluid and mechanical engineering.

KEYWORDS

Hybrid nanofluid; MHD; porous medium; BVP4C method

Nomenclature

B_0	Magnetic field strength, Wb
Cf	Local skin friction coefficient
c_p	Specific heat capacity, $Jkg^{-1}K^{-1}$
Ŕ	Permeability parameter, tma ⁻¹
ν	Vaniable manne ability of manage

K Variable permeability of porous medium

 ℓ Length of sheet, M M Magnetic parameter Nu Nusselt number Pr Prandtl number q Heat flux, Wm^{-2}



Re	Local reynolds number
S	Wall mass transfer parameter
T	Temperature, K
T_o	Reference temperature, K
u_w	Variable shrinking velocity, Ms^{-1}
$V_{\scriptscriptstyle W}$	Variable velocity of suction/injection, Ms^{-1}
v_1	Velocity component along x-axis, Ms^{-1}
v_2	Velocity component along Y-axis, Ms^{-1}
We	Williamson parameter
μ	Dynamic viscosity, $Kgm^{-1}s^{-1}$
v	Kinematic viscosity, M^2s^{-1}
P	Density, <i>Kgm</i> ⁻³
$oldsymbol{\Sigma}$	Electrical conductivity, $A^2s^3kg^{-1}m^{-3}$
Ψ	Stream function, $Kgm^{-1}s^{-1}$
$\overline{\tau}_{\scriptscriptstyle X}$	Wall shear stress, $Kgm^{-1}s^{-2}$
χ	Nanoparticle volume fraction

Subscripts

f	Base fluid
SW	SWCNTs
MW	MWCNTs

hnf Hybrid Nanofluid Wall/Surface

∞ Ambient Environment

1 Introduction

Nanofluid played a vital role in industrial and automotive applications. It is widely used as the radiator coolant, brake fluid and as a smart fluid in battery devices. Nanofluid is also applied as a coolant medium at a nuclear reactors, geothermal power, tire plant as well as in very small electronic applications such as microchip coolers [1].

Historically, the term nanofluid has first been coined by Choi et al. [2] to express the term nanofluid (nanoparticles fluid suspension). The nano size (<100 nm) solid particles in the fluid later known as the nanoparticles are usually made from metal or oxide. Metal nanoparticles such as zinc Zn, copper Cu and silver Ag are popular because of their high in thermal conductivities [3–5]. On the other side, these metal nanoparticles are high in density and thus promoted high friction between fluid and surface which cause corrosion. Furthermore, it is expensive. Meanwhile, the oxide nanoparticles are cheap and economical to be produced in mass production, but the oxide nanoparticles have low thermal conductivities. Increasing the percentage of nanoparticles in the fluid may increase the thermal behavior performance, but too many nanoparticles in the fluid will promote clogging.

Hybrid nanofluids can be considered as a new generation of Nanofluids. It is a very new idea. This is the composition of two variant types of dispersed nanoparticles in base fluids. This phenomenon have tale features that might make them helpful in many heat transfer organizations, like microelectronics, components of energy, pharmaceutical equipment, half breed powdered engines, engine cooling, car warming Administration, home cooler, chiller, thermal exchanger, atomic reactor coolant, grinding machinery, space innovation [6]. Sundar et al. [7] have proposed a thorough process

for generating hybrid nanofluids, including their advantages and disadvantages. Waini et al. [8] have investigated the stretching and contracting of a sheet-induced hybrid nanofluid created by adding copper nanoparticles to an Al₂O₃/water nanofluid. To explore the impact of thermal radiation, chemical reaction, suction, and slip condition on the heat and mass transfer of an unsteady MHD flow across a stretched surface, researchers Sreedevi et al. [9] have combined both carbon nanotubes and silver nanoparticles in the base fluid (water). The influence of radiation and suction on the dynamics of an MHD hybrid nanofluid moving through a stretching sheet has been studied by Yashkun et al. [10].

With the rising era of graphene, the carbon nanotube (CNT) seems to be the alternative for the high-density issue of metal nanoparticles while providing better thermal conductivity than oxide nanoparticles. Anuar et al. [11] studied the stability analysis of flow and heat transfer of carbon nanotubes over a moving plate. The heat transfer capabilities between the single (SWCNTs) and multi-walled carbon nanotubes (MWCNTs) nanoparticles in water as a based fluid are numerically examined. Next, Hayat et al. [12] investigated the carbon nanotube effects represented by SWCNTs and MWCNTs nanoparticles in the melting heat transfer over an impermeable stretchable surface in a nanofluid. Zaki et al. [13] concluded that the presence of SWCNTs nanoparticles in the Cu/water nanofluid so-called SWCNTs-Cu/water hybrid nanofluid dramatically raised the surface temperature and the heat transfer coefficient. Recently, Idrees et al. [14] studied the 3D rotational flow and heat transfer dynamics of a hybrid (SWCNT-MWCNT) nanofluid.

Considering the stretching/shrinking sheet in industrial processes, the heat transfer rate on the stretching/shrinking components plays an important factor in the quality of the product produces. Since half a century ago, the investigation of convection flow past a stretching/shrinking sheet has attracted the researcher's attention [15]. The investigation evolved by including various physical external forces on a fluid flow such as the magnetic effects, the thermal radiation effects, the chemical reaction, the viscous dissipation, the heat generation/absorption and the permeability effects [16–20]. Recently, the bio-convection and activation energy across of Prandtl nanofluid flow on a stretching cylinder has been investigated by Shah et al. [21].

The study flows on a stretching sheet then are extended by considering the industrial fluid such as the Maxwell fluid, the Williamson hybrid ferrofluid, the micropolar nanofluid, the second-grade nanofluid, the Casson nanofluid and the viscoelastic nanofluid as recently studied by [22–28].

Motivated by the above literature, the present study investigates the carbon nanotube Williamson hybrid nanofluid flow on an exponentially stretching sheet with MHD effects. The SWCNTs and MWCNTs nanoparticles are taken as the hybrid particles. Such investigation has never been done before, so the reported result in this study is new. This research will be answering whether the blended carbon nanotube performs better than the single carbon nanotube nanofluid and the effects of the magnetic, shrinking surface, and the porosity in the fluid on the fluid flow and heat transfer performance.

2 Mathematical Formulations

Consider a steady 2-dimensional Williamson hybrid nanofluid boundary layer flow with single (SWCNTs) and multi-walled carbon nanotubes (MWCNTs) nanoparticles with water H₂O as a based-fluid on an exponentially shrinking sheet. The porous surface is considered, with variable wall mass suction/injection applied through it. Fig. 1 shows a physical representation of this situation. Physical model of the fluid flow can be modelled to a basic equation for motion and energy distribution are as follows [28]:

$$\frac{\partial v_1}{\partial x} + \frac{\partial v_2}{\partial v} = 0,\tag{1}$$

$$v_1 \frac{\partial v_1}{\partial x} + v_2 \frac{\partial v_1}{\partial y} = \frac{\mu_{hnf}}{\rho_{hnf}} \left(\frac{\partial^2 u_1}{\partial y^2} - \frac{v_1}{k^*} \right) - \frac{\sigma_{hnf}}{\rho_{hnf}} B_0^2 v_1 + \sqrt{2} \Gamma \frac{\partial v_1}{\partial y} \frac{\partial^2 v_1}{\partial y^2}, \tag{2}$$

$$v_1 \frac{\partial T}{\partial x} + v_2 \frac{\partial T}{\partial y} = \frac{k_{lnf}}{(\rho C_P)_{lnf}} \frac{\partial^2 T}{\partial y^2},\tag{3}$$

subjected to

$$v_1 = -u_w(x) = ae^{x/2\ell}, \quad v_2 = -V_w(x) = V_0 e^{x/2\ell} \quad T = T_w = T_\infty + T_o e^{x/2\ell} \quad \text{at } y = 0,$$

 $v_1 \to 0, \quad T \to T_\infty \text{ as } y \to \infty,$ (4)

where v_1 and v_2 denotes respectively velocity components along x- and y-directions, $k = k_o/e^{x/2\ell}$ gives variable permeability of porous medium with k_o being a non-negative constant, T represents temperature of hybrid nanofluid, $u_w = ae^{x/2\ell}$ is variable shrinking velocity with a being positive constant having dimension ℓT^{-1} . Next, $V_w = V_0 e^{x/2\ell}$ is variable velocity of suction/injection, T_0 and ℓ denote reference temperature and length. Furthermore, (ρ_{hnf}) , (μ_{hnf}) , (σ_{hnf}) , and $(\rho c_p)_{hnf}$ are the density, dynamic viscosity, electrical conductivity, thermal conductivity and heat capacity of hybrid nanofluid, respectively, which are defined as [29].

$$\begin{split} \rho_{hnf} &= (1 - \chi_{SW}) \left[(1 - \chi_{MW}) \, \rho_f + \chi_{SW} \rho_{SW} \right] + \chi_{MW} \rho_{MW}, \\ \mu_{hnf} &= \frac{\mu_f}{\left(1 - \chi_{SW} \right)^{2.5} \left(1 - \chi_{MW} \right)^{2.5}}, \\ \left(\rho c_p \right)_{hnf} &= (1 - \chi_{MW}) \left[(1 - \chi_{SW}) \left(\rho c_p \right)_f + \chi_{SW} \left(\rho c_p \right)_{SW} \right] + \chi_{GO} \left(\rho c_p \right)_{GO}, \\ \frac{k_{hnf}}{k_{bf}} &= \frac{\left(k_{MW} + 2k_{bf} \right) - 2\chi_{MW} \left(k_{bf} - k_{MW} \right)}{\left(k_{MW} + 2k_{bf} \right) + \chi_{MW} \left(k_{bf} - k_{MW} \right)}, \end{split}$$

where

$$rac{k_{bf}}{k_f} = rac{\left(k_{SW} + 2k_f\right) - 2\chi_{SW}\left(k_f - k_{SW}\right)}{\left(k_{SW} + 2k_f\right) + \chi_{SW}\left(k_f - k_{SW}\right)},$$
 $lpha_{hnf} = rac{k_{hnf}}{\left(
ho c_p\right)_{hnf}},$
 $2\left[\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}\right]$

$$\frac{\sigma_{hnf}}{\sigma_{f}} = 1 + \frac{3\left[\frac{\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}}{\sigma_{f}} - (\chi_{SW} + \chi_{MW})\right]}{\left[\frac{\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}}{\sigma_{f}} + 2\right] - \left[\frac{\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}}{\sigma_{f}} - \left[\frac{\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}}{\sigma_{f}}\right]\right]}.$$

Note that the properties related to base fluid, the SWCNTs and MWCNTs nanoparticles are denoted with subscript $f_{f,SW}$ and f_{MW} . Next, the continuity Eq. (1) is satisfied with the introduction of

the stream function Ψ so that $v_1 = \frac{\partial \Psi}{\partial y}$ and $v_2 = -\frac{\partial \Psi}{\partial x}$. To simply, the dependent variable in Eqs. (2) and (3) can be reduced. It is introduced the following self-similar transformations:

$$v_{1} = ae^{x/\ell}F'(\eta), \quad v_{2} = -\sqrt{\frac{av_{f}}{2\ell}}\left(F(\eta) + \eta F'(\eta)\right),$$

$$\theta(\eta) = \frac{T - T_{\infty}}{T_{w} - T_{\infty}}, \quad \eta = ye^{x/2\ell}\sqrt{\frac{a}{2\ell v_{f}}}.$$
(5)

Using Eq. (5), the Eqs. (2) and (3) can be expressed in the form of self-similar nonlinear equations as follows:

$$\frac{P_1}{P_2}(F''' - KF') + FF'' - 2(F')^2 - \frac{P_3}{P_2}MF' + WeF''F''' = 0,$$
(6)

$$P_4\theta'' + \Pr(F\theta' - F'\theta) = 0, (7)$$

where $K = \frac{2\ell v_f}{ak^*}$ is the permeability parameter, $\Pr = \frac{v_f(\rho C_p)_f}{k_f}$ is the Prandtl number.

 $We = x\sqrt{2}\Gamma\sqrt{\frac{a^3}{v_f}}$ is the Weissenberg number and $M = \left(\frac{\sigma_f B_0^2}{a\rho_f}\right)$ is the magnetic parameter. Also

$$P_1 = \frac{1}{(1 - \chi_{SW})^{2.5} (1 - \chi_{MW})^{2.5}},$$

$$P_2 = (1 - \chi_{SW}) \left[(1 - \chi_{MW}) \rho_f + \chi_{SW} \rho_{SW} \right] + \chi_{MW} \rho_{MW},$$

$$P_{3} = 1 + \frac{3\left[\frac{\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}}{\sigma_{f}} - (\chi_{SW} + \chi_{MW})\right]}{\left[\frac{\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}}{\sigma_{f}} + 2\right] - \left[\frac{\chi_{SW}\sigma_{SW} + \chi_{MW}\sigma_{MW}}{\sigma_{f}} - (\chi_{SW} + \chi_{MW})\right]},$$

$$P_{4} = \frac{k_{lnnf}/k_{bf}}{(1 - \chi_{SW})[(1 - \chi_{SW})(\rho c_{p})_{f} + \chi_{SW}(\rho c_{p})_{SW}/(\rho c_{p})_{f}] + \chi_{MW}(\rho c_{p})_{MW}/(\rho c_{p})_{f}}$$

The boundary conditions in Eq. (4) is reduced to the following forms:

$$F = S, F' = -1, \quad \theta = 1, \quad \text{at} \quad \eta = 0,$$

 $F' \to 0, \quad \theta \to 0, \quad as \quad \eta \to \infty.$ (8)

Here, $S = V_0 \sqrt{2\ell/av_f}$ is the wall mass transfer parameter, The physical quantities interested in this study are the local skin friction coefficient Cf and the Nusselt number Nu which can be expressed as [28]

$$Cf = \frac{\overline{\tau}_x}{\rho_{hmf} U_w^2}, \ Nu = \frac{x \overline{q}_w}{k_f (T_w - T_\infty)}, \tag{9}$$

where

$$\overline{\tau}_{x} = \mu_{hnf} \left(\frac{\partial v_{1}}{\partial y} \right)_{y=0}, \ \overline{q}_{w} = -k_{hnf} \left(\frac{\partial T}{\partial y} \right)_{y=0}. \tag{10}$$

Using the definitions described above then the Cf and Nu are reduced as

$$\sqrt{\text{Re}}Cf = \frac{K_1}{K_2} \left[F''(0) + We(F''(0))^2 \right], \frac{Nu}{\sqrt{\text{Re}}} = -\frac{k_{hnf}}{k_f} \theta'(0).$$
 (11)

with $\sqrt{\text{Re}} = x \sqrt{\frac{a}{v_f}}$ where Re is the local Reynolds number.

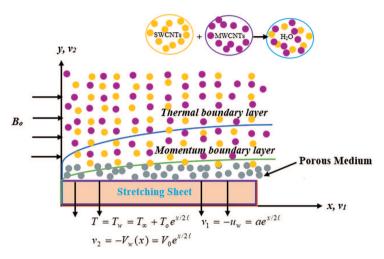


Figure 1: Physical geometry of the fluid flow

3 Numerical Simulation

The transformed ordinary differential Eqs. (6) and (7) with the boundary conditions (8) were solved numerically considering the water-based Williamson nanofluid SWCNTs/H₂O and the water-based Williamson hybrid nanofluid (SWCNTs + MWCNTs)/H₂O. Results from the study are presented in a graphic and tabular format, with a focus on the model's mathematical components and their effects on velocity, temperature, and physical interest quantities. This study used the numerical technique from bvp4c function in MATLAB. bvp4c is the finite difference code implements the well-known three-stage Lobatto IIIA formula. Named after Rehuel Lobatto, this method is a collocation formula as Runge-Kutta method and provides a fourth-order accurate uniformly results. Related works that implements the bvp4c method included [30,31] and recently by [32,33].

To use this approach, the transformed ordinary differential equations are converted into the system of 1st order differential equations, which is followed as

$$\begin{cases} y_1 = F, \ y_2 = F', \ y_3 = F'', \ yy_a = F''', \\ y_4 = \theta, \ y_5 = \theta', \ yy_b = \theta'' \end{cases}$$
(12)

with

$$yy_a = \left[1/\left(\left(\frac{P_1}{P_2}\right) - Wey_3\right)\right] \left[\left(\frac{P_1}{P_2}\right)Ky_2 + 2y_2^2 + \left(\frac{P_3}{P_2}\right)My_2\right]$$
 (13)

$$yy_b = -\left(\frac{\Pr}{P_4}\right)[y_1y_5 - y_2y_4]. \tag{14}$$

Corresponding boundary condition are converted as

$$\begin{cases} y_{1}(0) - S \\ y_{2}(0) + 1 \\ y_{2}(\infty) \end{cases}$$

$$\begin{cases} y_{4}(0) - 1 \\ y_{4}(\infty) \end{cases}$$
(15)

The resulting transformation above with the suitable IVP are coded into MATLAB software to compute numerically, see Fig. 2.

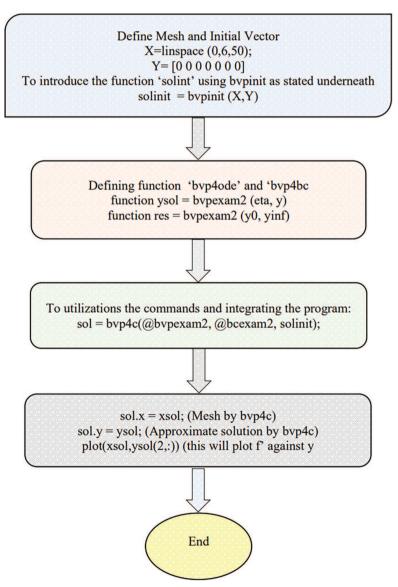


Figure 2: Flow chart of bvp4c method

4 Results and Discussion

The transformed ordinary differential Eqs. (6) and (7) with boundary conditions (8) were solved numerically using the BVP4C function in MATLAB software. The numerical computation considers the changes of pertinent parameters such as the permeability parameter K, the magnetic parameter M, the Williamson parameter We, the nanoparticle volume fractions of SWCNTs χ_{SW} and MWCNTs nanoparticles χ_{MW} , respectively and the wall mass transfer parameter S in the fluid flow. Further, the Prandtl number Pr is taken as 7 considering the Pr values for water. Table 1 shows the thermos-physical properties of water as a based fluid with carbon nanotube nanoparticles.

1 7 1	1		1 [/]			
Thermo-physical properties	$\rho \left(\text{kg m}^{-3} \right)$	$C_P \left(J k g^{-1} K^{-1} \right)$	$k (W m^{-1} K^{-1})$	$\sigma \left(S m^{-1} \right)$		
H_2O	997.1	4179	0.613	5.5×10^{-6}		
SWCNTs	2600	425	6600	10^{-6}		
MWCNTs	1600	796	3000	1.9×10^{-4}		

Table 1: Thermo-physical properties of water and carbon nanotube nanoparticles [13,14]

The effects of fluid parameters on the reduced skin friction coefficient $\sqrt{\text{Re}}Cf$ is tabulated in Table 2. From Table 2, it is found that the increase in magnetic parameter M, the permeability parameter K, the nanoparticle volume fractions of MWCNTs χ_{MW} and the wall mass transfer parameter S results in enhanced friction between the fluid and the plate surface. This is physically realistic due to the effects of M and K attracting the fluid particle or giving the suction effects towards the plate surface which contributing extra force from fluid to a surface thus increased friction. Meanwhile, the increase in Williamson parameter We have reduced the skin friction coefficient. Crossing Table 2, it is concluded that, the water-based Williamson hybrid nanofluid (SWCNTs + MWCNTs)/H₂O produced high in $\sqrt{\text{Re}}Cf$ values compared to the water-based Williamson nanofluid SWCNTs/H₂O.

M	K	S	$\chi_{\scriptscriptstyle MW}$	We	$(SWCNTs + MWCNTs)/H_2O$	(SWCNTs)/H ₂ O
1	1	2		1	2.7557	1.8173
2					3.3411	2.0245
3					3.7808	2.1953
1	1	2		1	2.7557	1.8173
	2				2.9608	2.1088
	3				3.1423	2.3355
1	1	2		1	2.7557	1.8173
		3			3.0631	2.2108
		4			3.3751	2.5909
1 1	1	2		1	2.7557	1.8173
				2	2.3332	1.5258
				3	2.0892	1.3565
			0.05		1.5557	_

Table 2: Influence of M, K, We, S and χ_{MW} on $\sqrt{\text{Re}}Cf$

(Continued)

Table 2 (continued)								
\overline{M}	K	S	χ_{MW}	We	(SWCNTs + MWCNTs)/H ₂ O	(SWCNTs)/H ₂ O		
			0.1	3	2.0892	_		
			0.2		2.8384	_		

Table 3 tabulated the effects of fluid parameters on the reduced Nusselt number $Nu/\sqrt{Re_x}$. It is suggested that a small increment on $Nu/\sqrt{Re_x}$ was found as M and K increased. On the other hand, the increase in S has boosting the values of $Nu/\sqrt{Re_x}$ drastically. Physically the suction effect produced by the wall mass transfer parameter S reduced the fluid particle, providing the convection process between the fluid and plate surface occurs effectively thus boosted the reduced Nusselt number $Nu/\sqrt{Re_x}$. Meanwhile, the increase in Williamson parameter We and χ_{MW} has slightly reduced the values of $Nu/\sqrt{Re_x}$. Comparing the performance between the nanofluid, the water-based Williamson hybrid nanofluid (SWCNTs + MWCNTs)/H₂O has lower in $Nu/\sqrt{Re_x}$ values compared to the water-based Williamson nanofluid SWCNTs/H₂O. Physically, carbon nanotube nanoparticles have high thermal conductivity properties. The increase in carbon nanotube nanoparticles in the fluid has enhanced the fluid thermal conductivity, thus raising the fluid conductive properties, therefore reducing the convective heat transfer capabilities of the fluid.

Table 3: Influence of M, K, We, S and χ_{MW} on $Nu/\sqrt{Re_x}$

M	K	S	χ_{MW}	We	$(SWCNTs + MWCNTs)/H_2O$	(SWCNTs)/H ₂ O
1	1	2		1	11.3665	11.5472
2					11.4083	11.5586
3					11.5472	11.5677
1	1	2		1	11.3665	11.5472
	2				11.3816	11.5631
	3				11.3946	11.5750
1	1	2		1	11.3665	11.5472
		3			17.9208	18.0513
		4			24.2903	24.3920
1	1	2		1	11.3665	11.5472
				2	11.3352	11.5310
				3	11.3155	11.5210
			0.05		11.4248	_
			0.1	3	11.3155	_
			0.2		11.0460	

In discussing the fluid flow behavior across the boundary layer, Figs. 3–7 are illustrated. From Figs. 3 and 5, it is found that the increase of *M*, *K* and *S* has slightly increased the fluid flow velocity while reducing the velocity boundary layer thickness. The reduction in the thickness of the boundary layer physically leads to the increase in velocity gradient which derives to the increase in skin friction

coefficient as found in Table 2. The same pattern occurs in Fig. 7 where the increase in χ_{MW} results in an increase in velocity distribution while reducing the boundary layer thickness. The increase in χ_{MW} enhanced the fluid momentum thus speeds up the fluid flow velocity. This outcome is agreed by the fluid comparison achieved in Figs. 3–6 where the water-based Williamson hybrid nanofluid (SWCNTs + MWCNTs)/H₂O has higher fluid flow velocity as well as the skin friction coefficient compared to the water-based Williamson nanofluid SWCNTs/H₂O. Meanwhile, the Williamson parameter We gives negative effects on the fluid flow. As seen in Fig. 6, it is found that the velocity distribution decreases as the We increases.

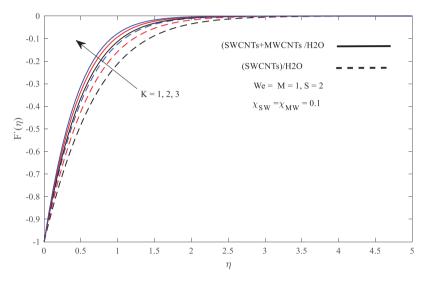


Figure 3: Influence of K on velocity profiles $F'(\eta)$

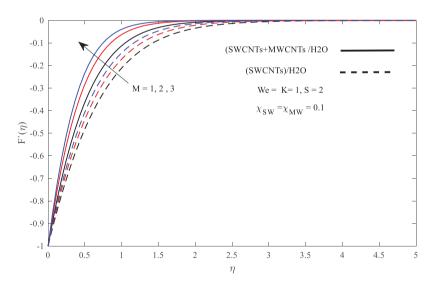


Figure 4: Influence of M on velocity profiles $F'(\eta)$

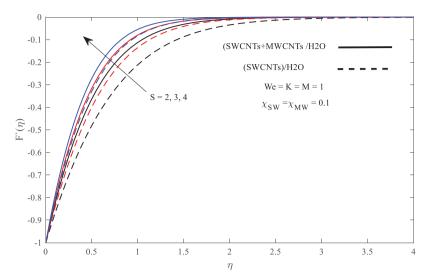


Figure 5: Influence of *S* on velocity profiles $F'(\eta)$

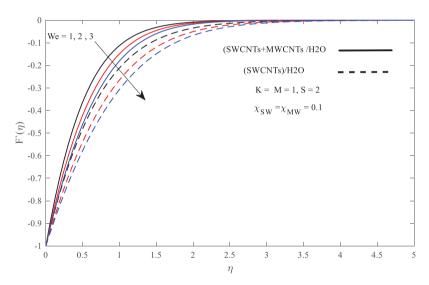


Figure 6: Influence of We on velocity profiles $F'(\eta)$

Lastly, Figs. 8 and 9 depicted the temperature profiles $\theta(\eta)$ for different values of S and χ_{MW} , respectively. From Fig. 8, it is observed that the increase in S results in a reduction in the thermal boundary layer thickness. This implies shortening the depth for the fluid with wall temperature to achieve the stream temperature outside the boundary layer. Shortening the thickness refers to the increase in the temperature gradient, thus physically reflecting the increase in Nusselt number as supported by Table 3. Meanwhile, the increase in χ_{MW} in Fig. 8 has widened the thermal boundary layer thickness as well as the temperature distributions. This is realistic because the increase in χ_{MW} leads to an increase in nanofluid thermal conductivities, thus enhancing the fluid thermal capabilities. The comparison between the temperature distributions for the water-based Williamson hybrid nanofluid (SWCNTs + MWCNTs)/H₂O and the water-based Williamson nanofluid SWCNTs/H₂O are shown in

Fig. 8. It is clearly shown the advantages of high χ_{SW} and χ_{MW} in the fluid enhanced temperature and its thermal boundary layer thickness.

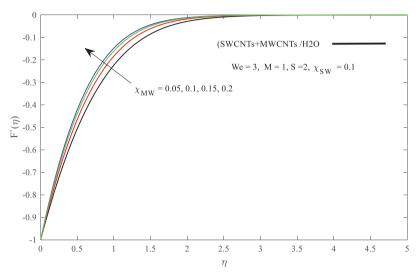


Figure 7: Influence of χ_{MW} on velocity profiles $F'(\eta)$

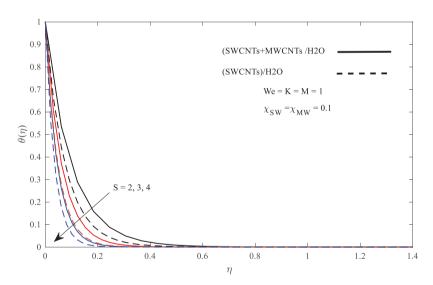


Figure 8: Influence of *S* on temperature profiles θ (η)

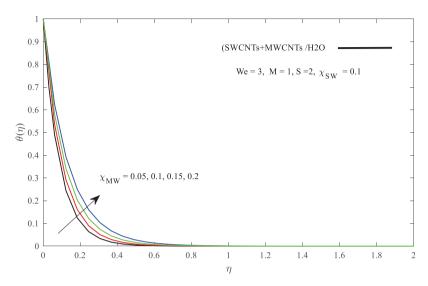


Figure 9: Influence of χ_{MW} on temperature profiles $\theta(\eta)$

5 Conclusions

The study on the flow and heat transfer of porous Williamson hybrid nanofluid on an exponentially shrinking sheet with magnetohydrodynamic (MHD) effects are numerically studied. The influence of the fluid parameters such as the permeability parameter K, the magnetic parameter M, the Williamson parameter We, the nanoparticle volume fractions of SWCNTs χ_{SW} and MWCNTs nanoparticles χ_{MW} , respectively and the wall mass transfer parameter S on the fluid flow and heat transfer characteristic are analyzed and discussed. In conclusion, it is found that:

- The increase in M, K, χ_{MW} , and S has promoted the increase in skin friction coefficient while We do the contrary.
- The small increase has been recorded on a Nusselt number as M and K increase.
- S played an important role as it increased may boost the values of Nusselt number drastically. Meanwhile, the Nusselt number reduced with the increase of We and χ_{MW} .
- The water-based Williamson hybrid nanofluid (SWCNTs + MWCNTs)/H₂O has a lower Nusselt number compared to the water-based Williamson nanofluid SWCNTs/H₂O. This might be explained by the increase in fluid thermal conductivity in the fluid thus increasing the domination of conduction over the convection heat flow.
- The increase in magnetic paramater in SWCNTs + MCWNTs hybrid nanofluid results to the increase of 72.2% on skin friction compared to SWCNT nanofluid.

We note that this analysis may be extended for the Jeffrey fluid, Oldroyd-B fluid and other non-Newtonian fluids.

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Availability of Data and Materials: The data used in this paper can be requested from the corresponding author upon request.

Conflicts of Interest: The authors declare that they have no conflicts of interest to report regarding the present study.

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