

Comparative Thermal Performance in SiO₂-H₂O and (MoS₂-SiO₂)-H₂O Over a Curved Stretching Semi-Infinite Region: A Numerical Investigation

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Abstract: The investigation of Thermal performance in nanofluids and hybrid nanofluids over a curved stretching infinite region strengthens its roots in engineering and industry. Therefore, the comparative thermal analysis in SiO₂–H₂O and (MoS₂–SiO₂)–H₂O is conducted over curved stretching surface. The model is reduced in the dimensional version via similarity transformation and then treated numerically. The velocity and thermal behavior for both the fluids is decorated against the preeminent parameters. From the analysis, it is examined that the motion of under consideration fluids declines against Fr and λ . The thermal performance enhances for higher volumetric fraction and λ . Further, it is noticed that thermal performance prevailed in (MoS₂–SiO₂)–H₂O throughout the analysis. Therefore, (MoS₂–SiO₂)–H₂O is better for industrial and engineering uses where high heat transfer is required to accomplished different processes of production.

Keywords: Thermal performance; curved surface; SiO_2-H_2O and $(MoS_2-SiO_2)-H_2O$; shear stresses; Nusselt number; numerical scheme

1 Introduction

Carbon nanotubes illustrate the minimally complicated existence of graphene surface structures climbed in barrel form and atomic contour. CNTs demonstrate remarkable chemical, electrical, wet, engineered, and mechanical properties due to their combination of the small-scale, tubular structure, and large surface area. Based on the volume of graphene atoms, the carbon nanotubes are subdividing into single walled (SWCNT) and multi-walled carbon nanotubes (MWCNT). More essential efforts in this area can be made through attempts [1–8] and various studies. Convective fluid flow and heat transfer are used for nuclear reactors owing to permeable space in geology applications, cleaning and liquid plastic molding, microbial, and combustion.



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Darcy has developed an essential semi-experimental groundbreaking equation for low porosity and low-velocity flux. By increasing Reynolds number, nonlinearity occurs from the expansion of inertial force in the semi-observational equation. In particular, the Darcy–Forchheimer flow model used and predicted a modified meaning in the energy equation by using the nonlinear concept of velocity. The Darcy–Forchheimer hybrid convection with thermophoresis and viscous dissipation in a liquid vacuum filled with air. This way, tests and numerous investigations [9–15] tracked the development of new attempts on the Darcy–Forchheimer model. Besides, some nanofluid-related studies can be found in [16–17]. Esfe et al. [18] explored the use of COOH–functionalized carbon nanotubes and nanofluid based on ethylene glycol-water in the heating and cooling system for heat transfer efficiency.

Experimental and computational experiments are still ongoing surrounding the hybrid nanofluids. Dardan et al. [19] presented the analysis of hybrid nanofluids. Esfe et al. [20] analyzed, the hybridization of carbon nanotubes with silicon oxide and silver nanoparticles in the presence of plasma. Sarkar et al. [21] characterized the nanofluid by aluminum containing the Copper water base. In the presence of hybrid nanoparticles, they addressed the thermo-physical action of the material and concluded about the attitude of efficacy in that thermal conduction. Nanofluids are a nowadays popular area of research. The concept of nanofluids was introduced by Choi's [22]. In the existence of CuO nanoparticles throughout the water and Al_2O_3 particles in ethylene glycol and soil, Suresh et al. [23] performed experimental heat transfer experiments.

We also observed that heat transfer experimentally through the use of individual particles improves the one-fifth time. Nine et al. [24] and Toghraie et al. [25] experimented with the help of copper oxide found that the thermal conductivity was improved. Khan et al. [26] addressed the transportation of a nanofluid to a stretched surface at the boundary layer. They concluded that there are opposing effects for Prandtl number, Lewis number, Brownian motion parameter, and thermophoresis parameter, Nusselt number and Sherwood number, respectively. Using the applications in the electrically conductive fluid and magnetic field will monitor the cooling rate and the desired end product properties. The use of the magnetic field was used to purify non-metallic inclusions of the molten metals. Two examples of this type of effect are fusing metals into an electric furnace by applying a magnetic field and cooling the first wall within a nuclear reactor containment vessel where the hot plasma is separating from the ground by using a magnetic field. Considering thermal radiation, Sheikholeslami et al. [27] performed a statistical study of Al₂O₃ water-based nanofluid free convection with MHD. The properties of Cu-water nanofluid stagnation point flow and heat transfer over a horizontal pipe that extends/ shrinks were studied by Sulochana et al. [28].

This work aims at investigating the heat transfer change due to the existence of hybrid nanofluid flow over a curved stretching sheet. The suspension of two different nanoparticles known as sand called (MoS_2) and (SiO_2) is defined as a hybrid nanofluid. Water is actually used as the base fluid. This is evaluated for heat transfer and thermal stability, with the introduction of MoS_2/SiO_2 nanoparticles as the base fluid of liquids. Curvilinear coordinates perform a mathematical approximation of the physical flow problem and numerically solved nonlinear coupled differential equations using shooting algorithms after simplification. The effect of new essential parameters on the velocity and temperature distributions are discussed using graphs. The skin friction coefficient and the Nusselt number are tabulated for different values of the basic parameters.

2 Statement Geometry and Nanofluid Models Formulation

2.1 Statement and Geometry

We consider the steady two-dimensional, incompressible flow of the nanofluid coiled into R-circle radius over a stretching sheet. By preserving steady roots, the sheet is stretched through the forces exerted along the s-direction, and the direction of r is perpendicular to it. The stretching velocity of the surface is u = as, where a is constant (a > 0). The surface temperature is held stable at $T_w(s) = A(s/l)$,

where $T_w > T_{\infty}$ is a constant with T being the atmospheric uniform temperature of the fluid. The empirical flow explanation of the present problem in engineering is shown in Fig. 1



Figure 1: Physical model of the problem

Under these conditions together with the approximations of boundary layers, the governing equations are;

$$\frac{\partial}{\partial r}(r+R) + v + R\frac{\partial u}{\partial x} = 0,\tag{1}$$

$$\frac{u^2}{r+R} = \frac{1}{\rho_{hnf}} \frac{\partial p}{\partial r},\tag{2}$$

$$v\frac{\partial u}{\partial r} + \frac{R}{r+R}u\frac{\partial u}{\partial s} + \frac{uv}{r+R} = -\frac{1}{\rho_{hnf}}\frac{R}{r+R}\frac{\partial p}{\partial s} + v_{hnf}\left(\frac{\partial^2 u}{\partial r^2} + \frac{1}{r+R}\frac{\partial u}{\partial r} - \frac{u}{r+R^2}\right) - \frac{v_{hnf}}{K^*} - Fu^2$$
(3)

$$v\frac{\partial T}{\partial r} + u\frac{\partial T}{\partial s}\frac{R}{r+R} = \alpha_{hnf}\left(\frac{\partial^2 T}{\partial r^2} + \frac{1}{r+R}\frac{\partial T}{\partial r}\right),\tag{4}$$

subject to boundary conditions

$$u = U_w(s) = ae^{\frac{s}{L}}, \ v = 0, \ T = T_w = T_\infty + T_0 e^{\frac{ds}{2l}}$$
 at $r = 0,$ (5)

$$u \to 0, \ \frac{\partial u}{\partial r} \to 0, \ T \to T_{\infty} \text{ when } r \to \infty.$$
 (6)

where Eq. (1) preserves the mass, transverse and axial components expressed in Eqs. (2) and (3) respectively. Through the given energy equation Eq. (4), the heat transfer shall be investigated as well. However, u and v denote the components of velocity in s and r directions respectively, p is pressure, R denotes radius of curvature, ρ_{hnf} is hybrid nanofluid density, u and v denote the velocity components in s and r direction, p is pressure, K* is porous permeability of space, and C_b is the drag coefficient. F = C_b/(LK)^{*1/2} is the non-uniform coefficient of inertia, while T_w and T_∞ are the wall and ambient temperatures respectively.

We implement the following a similarity transformation to further promote this process;

$$u = U_w = ae^{\frac{s}{L}}f'(\zeta),\tag{7}$$

$$T = T_{\infty} + T_0 e^{\frac{4s}{2L}} \theta(\zeta), \tag{8}$$

$$p = \rho_f a^2 e^{\frac{2s}{L}} H(\zeta), \tag{9}$$

$$\zeta = \left(\frac{ae^{s/L}}{2v_f L}\right)^{\frac{1}{2}}r,\tag{10}$$

$$v = -\frac{R}{r+R}\sqrt{\frac{av_f e^{\dot{\tilde{z}}}}{2L}}(f(\zeta) + \zeta f'(\zeta)).$$
(11)

2.2 Effective Nanofluid Models

The following nanofluid models are used to improve the thermal performance

$$\rho_{nf} = (1 - \emptyset)\rho_f + \emptyset\rho_s \tag{12}$$

$$\left(\rho C_p\right)_{nf} = (1 - \emptyset) \left(\rho C_p\right)_f + \emptyset \left(\rho C_p\right)_s \tag{13}$$

$$\mu_{nf} = \frac{\mu_f}{(1 - \emptyset)^{2.5}} \tag{14}$$

$$\frac{k_{nf}}{k_f} = \frac{k_s + (n-1)k_f - (n-1)\phi(k_f - k_s)}{k_s + (n-1)k_f + \phi(k_f - k_s)}$$
(15)

2.3 Effective Hybrid Nanofluid Models

The following hybrid nanofluid models are implemented to improve the thermal performance in the hybrid nanofluid

$$\rho_{hnf} = (1 - \emptyset_2) \left[\left((1 - \emptyset_1) \rho_f + \emptyset_1 \rho_{s1} \right) \right] + \emptyset_2 \rho_{s2}$$
(16)

$$(\rho_{cp})_{hnf} = (1 - \emptyset_2) \left[(1 - \emptyset_1) (\rho_{cp})_f + \emptyset_1 (\rho_{cp})_{s_1} \right] + \emptyset_2 (\rho_{cp})_{s_2}$$
(17)

$$\mu_{hnf} = \frac{\mu_f}{(1 - \emptyset_1)^{2.5} (1 - \emptyset_2)^{2.5}}$$
(18)

$$\frac{k_{hnf}}{k_{bf}} = \frac{k_{s_2} + (n-1)k_{bf} - (n-1)\phi_2(k_{bf} - k_{s_2})}{k_{s_2} + (n-1)k_{bf} + \phi_2(k_{bf} - k_{s_2})}$$
(19)

Where $\frac{k_{bf}}{k_f} = \frac{k_{s_1} + (n-1)k_f - (n-1)\phi_1(k_f - k_{s_1})}{k_{s_1} + (n-1)k_f + \phi_1(k_f - k_{s_1})}$

Surely, Eq. (1) automatically validates and (2)-(4) transforms the ordinary differential equation into nondimensional equation as follows;

$$\left(\frac{1}{\psi_1}\right)H'(\zeta) = \frac{1}{\zeta + B}f^{\prime 2},\tag{20}$$

$$\left(\frac{1}{\psi_2}\right) \left(f''' + \frac{1}{\zeta + B}f'' - \frac{1}{(\zeta + B)^2}f' - 2\lambda f^{2'}\right) - \frac{\zeta + 2B}{(\zeta + B)^2}B(f')^2 + \frac{B}{\zeta + B}ff''$$
(21)

$$+ff'\frac{B}{(\zeta+B)^2} - 2F_r f^{2'} = \left(\frac{1}{\psi_1}\right)\frac{B}{\zeta+B}(4H+\zeta H'),$$

$$1\left(\frac{1}{\zeta}\right)k_{hnf}\left(\frac{g}{\chi_1} + \frac{1}{\zeta+B}-g\right) + \frac{B}{\zeta+B}(\zeta g) + \zeta f^{2}(0) = 0$$
(22)

$$\frac{1}{P_r} \left(\frac{1}{\psi_3}\right) \frac{k_{hnf}}{k_{bf}} \left(\theta'' + \frac{1}{\zeta + B}\theta'\right) + \frac{B}{\zeta + B} (f\theta' - Af'\theta) = 0,$$
(22)

where

$$\psi_1 = \frac{\rho_{hnf}}{\rho_f} = (1 - \emptyset_2) \left[\left((1 - \emptyset_1) + \emptyset_1 \frac{\rho_{s1}}{\rho_f} \right) \right] + \emptyset_2 \frac{\rho_{s2}}{\rho_f},$$
(23)

$$\psi_2 = \frac{v_f}{v_{hnf}} = (1 - \emptyset_1)^{2.5} \left\{ \left((1 - \emptyset_2)^{2.5} \left\{ \left((1 - \emptyset_2)(1 - \emptyset_1) + \emptyset_1 \frac{\rho_{s1}}{\rho_f} \right) \right\} + \emptyset_2 \frac{\rho_{s2}}{\rho_f}, \right\}$$
(24)

$$\psi_{3} = \frac{(\rho_{cp})_{hnf}}{(\rho_{cp})_{f}} = (1 - \emptyset_{2}) \left[(1 - \emptyset_{1}) + \emptyset_{1} \frac{(\rho_{cp})_{s_{1}}}{(\rho_{cp})_{f}} \right] + \emptyset_{2} \frac{(\rho_{cp})_{s_{2}}}{(\rho_{cp})_{f}}.$$
(25)

Once we obtain fluid velocity pressure, then H can be determined from Eqs. (20) and (21) and can be written as

$$\left(\frac{1}{\psi_2}\right) \left[f^{i\nu} + \frac{2}{(\zeta+B)} f''' - \frac{1}{(\zeta+B)^2} f'' + \frac{1}{(\zeta+B)^3} f' - 2\lambda \left(f'' + \frac{1}{(\zeta+B)} f' \right) \right] - \frac{K}{(\zeta+B)^2} ff'' + \frac{B}{(\zeta+B)^2} ff'' - \frac{3K}{(\zeta+B)^2} f'^2 - \frac{3K}{(\zeta+B)^2} f'f'' - 2F_r \left(2f'f'' + \frac{1}{(\zeta+B)} f'^2 \right) = 0.$$

$$(26)$$

The transformed boundary conditions are;

$$f = 0, f' = 1, \ \theta = 1 \ at \ \zeta = 0,$$
 (27)

$$f' \to 0, \ f'' \to 0, \ \theta \to 0 \ as \ \zeta \to \infty.$$
 (28)

In the relationships above, Pr represents the Prandtl number, Fr is the Forchheimer number, λ is the local porosity parameter, and the curvature parameter is B. These are defined by the following formulas:

$$B = \left(\frac{ae^{s/L}}{2v_f L}\right)^{\frac{1}{2}} R, \ \lambda = \frac{v_f L}{B^* U_w}, \ F_r = \frac{C_b}{B^{*1/2}}, \ P_r = \frac{v_f}{\alpha_f}$$
(29)

2.4 Quantity for Thermal Performance

The physical quantities of interest are skin friction coefficient C_f and local Nusselt number Nu_s , which are defined as

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$$C_f = \frac{\tau_{rs}}{\rho_{hnf} u_w^2},\tag{30}$$

$$Nu_s = \frac{sq_w}{k_{hnf}(T_w - T_\infty)},\tag{31}$$

Where τ_{rs} and q_w along the s-direction are defined as

$$\tau_{rs} = \mu_{hnf} \left(\frac{\partial u}{\partial r} - \frac{u}{r+R} \right) \Big|_{r=0}, \quad q_w = -k_{hnf} \left(\frac{\partial T}{\partial r} \right) + (q_r)_w \Big|_{r=0}.$$
(32)

The skin fraction coefficient and the local number Nusselt shall be

$$C_f R e_s^{\frac{1}{2}} = \left(\frac{1}{\psi_2}\right) \left(f''(0) - \frac{1}{B}f'(0)\right),\tag{33}$$

$$\frac{L}{s}\left(\frac{Re_s}{2}\right)^{-1/2} Nu_s = -\frac{k_{hnf}}{k_f} \left[\theta'(0)\right],\tag{34}$$

where $Re_s = \frac{U_{ws}}{v_f}$ elucidates local Reynolds number.

3 Results and Discussion

This section dedicates to the graphical analysis of the effect on the velocity and temperature distributions of several critical emerging parameters. Nanofluid based diagrams are shows using SiO₂ and MoS₂–SiO₂ water-based hybrid nanofluid. The comparative study of nanofluids and hybrid nanofluids is giving special consideration. Static lines show the results for nanofluid and pointed lines in the following diagrams show the results for hybrid nanofluid. Figs. 2–14 are shown for velocity and temperature distributions for specific Forchheimer number Fr values, curvature parameter B, local porosity parameter λ , hybrid volumetric fractions \emptyset_2 , of nanofluid, and temperature exponent A respectively.

3.1 The Velocity Against Preeminent Parameters

Fig. 2 shows to investigate the effect on the velocity of Forchheimer number Fr. It is a note from Fig. 2 that Forchheimer number Fr plays a part in increasing velocity. It is because the surface's expansion causes the fluid movement, and therefore, any fluid flow shifts on the expanding surface will decelerate the flow.



Figure 2: The variations of velocity for varying Fr

Fig. 3 indicates the opposite trend for the increased velocity. From this figure, it shows that velocity decreases as curvature parameter B increases. However, it is apparent from this calculation that for hybrid nanofluid, the change in velocity is substantially more significant.



Figure 3: The variations of velocity for varying B

For the velocity profile, the effect of the local porosity parameter λ is demonstrated by Fig. 4, the fluid flow is shown to intensify, and as the curvature parameter increases. At the same time, the thickness of the boundary layer decreases. Physically, this means that the bent surface bendiness helps to speed up fluid flow over it. For hybrid nanofluid, this speed increase is marginally more significant.



Figure 4: The variations of velocity for varying λ

Fig. 5 shows to analyze the velocity influence of the volumetric fraction \emptyset_2 for hybrid nanofluid. From this figure, it is discovering that for large volumetric fraction \emptyset_2 of MoS₂–SiO₂, hybrid nanofluid flows faster than nanofluid.

3.2 The Temperature Against Preeminent Parameters

The effect on the temperature profile of similar emergent parameters shows in Figs. 6 to 10. Graphs are demonstrating for better representation of nano and hybrid nanofluids. Additionally, each figure illustrates

five distinct forms of variables. Solid and pointed lines show the efficiency of nano and hybrid nanofluids, respectively. Pointed and solid lines also reflect increasing parameters including temperature exponent A for non-zero values, curvature parameter B, Forchheimer number Fr, hybrid nanofluid volumetric fractions \emptyset_2 , and local porosity parameter, respectively.



Figure 5: The variations of velocity for varying \emptyset_2



Figure 6: The variations of temperature for varying A

Fig. 6 diagrammed to study the temperature influence of temperature exponent A. It is revealed from this figure that temperature increases when temperature exponent A decreasing. It is because the value increase in A enhances the results of the conduction and thus raises the temperature. This increase is widespread away from the surface in the field and adds to the air heat flux. Nanoparticles with a hybrid nanofluid shaped blade have the maximum temperature. In comparison, these results are more reliable than nanofluid in the case of hybrid nanofluid, since hybrid nanofluid has more thermal conductivity than nanofluid.

Fig. 7 shows the influence of curvature parameter B on nano and hybrid nanofluid temperature, reducing the thickness of the surface and the thermal limit layer with curvature B increasing. That is because the curvature parameter contributes to the fluid flow deceleration and consequently contributes to the extent of the rising temperature. From this observation, it is also apparent that the temperature magnitude for hybrid nanofluid is higher for nanofluid for that values of B.



Figure 7: The variations of temperature for varying B

The temperature operation for Forchheimer number Fr shows in Fig. 8. The temperature increases by Forchheimer number Fr.



Figure 8: The variations of temperature for varying Fr

Fig. 9 plotted to analyze the influence on the temperature of the volumetric fraction \emptyset_2 of hybrid nanofluid. This figure shows that for sizeable volumetric fraction \emptyset_2 , hybrid nanofluid flows more rapidly than nanofluid.

Fig. 10 indicates the results of the local porosity parameter λ . From this Figure, it inferred that the parameter of local porosity affects the distribution of temperature by increasing it. It is because the atmosphere temperature is greater than that place far from the earth, and more heat is transferred from the ground into the air which adds to the thickness of the maximum thermal layer. This increase in temperature is also assumed to be influential in the case of hybrid nanofluid.

3.3 Nusselt Number

Figs. 11 and 12 drawn to study the Nusselt number influence of the local porosity parameter λ , volumetric fraction \emptyset_2 of the nanoparticles, and the Forchheimer number Fr. The tests for hybrid

nanofluid shows in Fig. 11. This equation elucidates that the Nusselt number decreases with an increase in the Forchheimer number Fr and volumetric fractions \emptyset_2 of nanoparticles (MoS₂–SiO₂).



Figure 9: The variations of temperature for varying \emptyset_2



Figure 10: The variations of temperature for varying λ

From Fig. 12 shows that the amount of the local heat transfer decreases with an increase in volumetric fractions \emptyset_2 of local porosity parameters λ and nanoparticles. Comparison of Figs. 11 and 12 showed that Nusselt number magnitude is greater for (MoS₂–SiO₂) than (SiO₂).

3.4 Skin Friction Coefficient

Figs. 13 and 14 show the variation for the effect of these changing parameters on the skin friction coefficient for nanofluid and hybrid nanofluid, respectively. Discussion of these figures reveals that the local porosity λ feature, the volumetric fraction \emptyset_2 of nanoparticles, and the Forchheimer number Fr contribute to a decrease in the skin friction coefficient's magnitude, decreasing the significance of the skin friction coefficient for nano and hybrid nanofluids. By contrast, in the case of nanofluid, the importance of the coefficient of skin friction is marginally higher than the hybrid nanofluid.



Figure 11: The variation of Nu_s for varying \emptyset_2 and Fr



Figure 12: The variation of Nu_s for varying \emptyset_2 and λ



Figure 13: The variation of C_f for varying \emptyset_2 and Fr

And from Fig. 14, it is inferred that the skin friction coefficient decreases with an increase in volumetric fractions \emptyset_2 of local porosity parameters λ and nano particles. The comparison of Figs. 13 and 14 showed that the magnitude of the skin friction coefficient is marginally higher than that of hybrid nanofluid.



Figure 14: The variation of C_f for varying \emptyset_2 and λ

4 Conclusions

The comparative study of the nanofluid and hybrid nanofluid is conducting over a curved stretching surface. The numerical analysis of the physical problem was work out in curvilinear coordinates. For specific parameter values \emptyset_2 , λ , B, A, and Fr, the governing Eqs. (9) and (10) with similar boundary conditions (11) are numerically treated. We used Mathematica package ND Solver. Detailed numerical calculations aimed at giving the flow problem a physical imagination for different estimations of the parameters displaying the flow qualities. The results for $f'(\zeta)$, $\theta(\zeta)$, C_f and Nu are graphically representing. Below are the interesting concluding highlights from this article.

- It should remember that during the increase of the SiO₂ and MoS₂–SiO₂ fraction of nanoparticle thickness, the thermal boundary layer, and the velocity boundary layer increase.
- $f'(\zeta)$ increases, and $\theta(\zeta)$ decreases with rising values of Fr.
- As far as the first solution is concerned, we found that $\theta(\zeta)$ magnifies for higher λ values while $f'(\zeta)$ responds to the contrary.
- Both fields of velocity and temperature demonstrate opposite correlations for more significant percentages of reliable nanoparticulate content \emptyset_2 .
- A different activity is observed in the fields of velocity and temperature when the parameter of local porosity π is rising.

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