

DOI: 10.32604/jrm.2022.017506

ARTICLE



Understanding the Impacts of Plant Capacities and Uncertainties on the Techno-Economic Analysis of Cross-Laminated Timber Production in the Southern U.S.

Zhenzhen Zhang¹ and Kai Lan^{2,*}

¹Department of Forestry and Environmental Resources, North Carolina State University, Raleigh, 27606, USA

²Department of Forest Biomaterials, North Carolina State University, Raleigh, 27606, USA

*Corresponding Author: Kai Lan. Email: klan2@ncsu.edu

Received: 15 May 2021 Accepted: 04 June 2021

ABSTRACT

Understanding the economic feasibility of cross-laminated timber (CLT), an emerging and sustainable alternative to concrete and steel, is critical for the rapid expansion of the mass timber industry. However, previous studies on economic performance of CLT have not fully considered the variations in the feedstock, plant capacities, manufacturing parameters, and capital and operating costs. This study fills this gap by developing a techno-economic analysis of producing CLT panels in the Southern United States. The effects of those variations on minimum selling price (MSP) of CLT panels are explored by Monte Carlo simulation. The results show that, across all the plant capacities from 30,000 to 150,000 m³/year, the MSP ranges from \$345 to \$609/m³ with a \pm 6%–9% range caused by the variations in feedstocks, key manufacturing parameters, capital and operating cost. The MSP decreases significantly along the increasing capacities. A sensitivity analysis exhibits that the lumber price, lumber preparing loss, plant capacity, and the installed costs of layering and gluing, finishing, and miscellaneous, are the top driving factors to CLT MSP. Supported by Geographic Information System, this study also studies the transportation cost of delivering CLT to customers under three CLT demanding levels (1%, 5%, 15%). The results show that the transportation cost is 1%–8% of the MSP. Lower demanding level or higher plant capacity can increase the transportation cost, larger plant capacity does not necessarily generate lower delivered cost.

KEYWORDS

Cross-laminated timber; techno-economic analysis; plant capacity; uncertainty; minimum selling price

1 Introduction

Currently, the reinforced concrete and steel dominate the structural systems of mid-rise buildings (e.g., commercial buildings) in North America [1,2]. Recently, cross-laminated timber (CLT) has attracted increasing attention for mid-rise buildings as an environmentally sustainable alternative to reinforced concrete and steel [3–6]. CLT is a prefabricated mass timber product with odd lumber (sawn lumber or structural composite lumber) layers (typically 3, 5, or 7) stacked crosswise (typically 90°) to form a solid panel [1,7–10]. The typical dimension of CLT panels can reach 0.30–3.05 meters in width, 0.10–0.25 meters in thickness, and up to 18 meters [11,12]. Over traditional reinforced concrete and steel, CLT has shown advantages in fire resistance and thermal performance [13–17], acoustic performance



[12,18–21], mechanical properties (e.g., bending stiffness and strength) [22–26], lower density [20,21,27], faster installation process [12,23,28], recyclability [3,29], and potential carbon storage [30,31]. Driven by these advantages, in the recent decade, the CLT market has been growing [11,32]. Energias reported that the global CLT market size was \$641 million in 2017 and forecasted to be \$1,833 million by 2024 with a compounded annual growth rate (CAGR) of 16.2% [33]. In North America, Ganguly et al. evaluated the demand for CLT panels in the Pacific Northwest (PNW) region to be 0.19 million m³/year by 2035 compared to around 0.008 million m³/year in 2016–2018 (less than 1% of annual PNW timber harvest) [32]. In the study by the Council of Western State Foresters (CWSF), the CLT demand in the CWSF region (17 Western US states and 6 US affiliated Pacific Islands) was estimated to be 0.26 million m³/year by 2020 and 0.52 million m³/year by 2025 [34]. In North America, by 2016, there were five CLT manufacturers in operation (three in the U.S. and two in Canada). The CLT manufacturer number in North America now increases to eleven among which five are in Canada (Structurlam Mass Timber Corporation, Nordic Structures, Kalesnikoff Mass Timber, Leaf Engineered Wood Products, and Element5 Co.,) and six are in the U.S. (IB X-Lam USA, Johnson Wood Innovations, SmartLam, Freres Lumber Co., Vaagen Timbers, and Sterling Lumber) [35–37]. Under this situation, understanding the economic viability of the CLT panels is important for the expansion of the CLT industry.

To evaluate the economic feasibility of CLT panels, techno-economic analysis (TEA) can be used as a widely adopted tool [38–40]. Two previous TEA studies explored the economic performance of CLT panels. Brandt et al. explored the minimum selling price (MSP) of 1 m³ CLT panels from softwood lumber and showed that the MSP was \$652/m³ and \$536/m³ for 52,000 and 87,000 m³/year plant, respectively [4]. In 2010, Bédard et al. evaluated the production cost of CLT from spruce lumber at a 30,000 m³ CLT/year plant and concluded the cost was \$679/m³ [41]. Another study by FPInnovations in 2013 briefly estimated the average CLT production cost to be \$678/m³ [11]. However, previous TEA studies on CLT have not considered the variations in lumber feedstock (e.g., moisture content, lumber price), manufacturing parameters (e.g., material loss, resin usage), and transportation cost of delivering CLT panels which is dependent on varied market demanding levels and plant capacities. These variations may have large impacts on the economic viability of CLT. Strengthening the understanding of the impacts of those variations can help the future designing and planning of the CLT plant and identify the key drivers of the cost, especially under varied future market conditions.

This study addressed the challenge by conducting a TEA for producing CLT from softwood lumber in the Southern U.S. MSP of CLT panels was selected as the economic indicator. This study also investigated the transportation cost of delivering CLT from the plant to consumers. The transportation route was optimized by a linear programming model where the road network information was provided by Geographic Information System (GIS). The mass and energy data of the CLT plant were generated from a process-based simulation model. The data ranges of key parameters were collected from the literature to analyze their impacts on the economic performance. To model these variations, Monte Carlo simulation (MCS) was used [38,42]. Scenario analysis was conducted to evaluate the effects on MSP and delivered cost (MSP plus transportation cost of delivering CLT) under different plant capacities and market demanding levels.

2 Methods and Materials

In this study, a TEA was performed to evaluate the minimum delivered cost of 1 m³ CLT panel which consists of two components, MSP out of the CLT plant gate and delivering transportation cost to the construction site. The MSP was calculated in a discounted cash flow rate of return (DCFROR) analysis, a widely adopted economic analysis tool in varied industries (see Section 2.2) [43–45]. The MSP is a critical indicator in evaluating the economic feasibility of a product by representing the minimum product selling price to reach the breakeven point in the cash flow [45]. In other words, the MSP indicates the

lowest selling price to cover all the production costs. In the DCFROR analysis, the capital costs and operating costs of the CLT plant were calculated based on the mass and energy balance generated by the process simulation model. The transportation cost was estimated by a mathematical programming model where the transportation distance was provided by the GIS model (see Section 2.3).

2.1 CLT Production

Fig. 1 shows the system diagram of the CLT plant. After softwood lumber arrives at the plant, lumber is unloaded by the forklift and stored in the warehouse. The forklift transfers lumber from the storage site to the lumber feeding system. In lumber preparation, lumber undergoes the visual grading and grouping process to ensure that the lumber in longitudinal layers reach visual grade No. 2 and the lumber in transverse layers reach visual grade No. 3 [46]. Then the lumber moisture content is measured. As required by the ANSI/ APA PRG 320-2019 standard, the moisture content of lumber need to be $12 \pm 3\%$, which is assumed to be the uncertainty range of lumber moisture content in this study (see Tab. 1) [46]. Following the grading and moisture detecting, lumber is trimmed or re-cut to remove defects [47,48]. The waste from lumber preparation can vary significantly based on previous studies and highly depend on the feedstock suppliers, but is controllable by selecting qualified suppliers [12,41,48]. The range of material loss in lumber preparation is documented in Tab. 1. The selected and grouped lumber is temporally stored for the next step, end-jointing. In the end-jointing, lumber is longitudinally end-jointed to make long continuous lumber [24]. In this study, finger-jointing was assumed to be the end-jointing type. Four-side planing is needed to meet the requirement of thickness tolerance for better bonding results [7,24]. The longitudinally assembled lumber is layered and glued for face bonding [28]. The resin was selected to be melamine formaldehyde (MF), as a commonly used resin in finger-jointing and face-bonding. The MF usage in this study was collected from the literature (see Tab. 1) [12,24,48,49]. After pressing, the finishing step includes planing and end cutting. Planing is needed to remove any excess resin and final uneven surfaces. Since CLT panels are highly prefabricated and customized for fast erection and minimal onsite cutting, Computerized Numerical Control (CNC) is commonly used [50]. CLT is then packaged and ready for transport to the construction site.



Figure 1: Flow diagram of the CLT plant

The variations and uncertainties of the key parameters for the CLT production were collected from the literature and documented in Tab. 1. The diesel consumption of hauling and conveying materials between unit operations was assumed 1.3 L/m^3 final CLT produced [51–53].

	Unit	Mea valu	n Minimum e	Maximum	Assumed distribution
Lumber Moisture content [46]	%	12	9	15	Triangular (9, 12, 15)
Lumber density at 12% moisture content [53]	kg/m ³	495	400	590	Uniform [400, 590]
Resin (MF) for finger-jointing and pressing [12,24,48,49]	kg/m ³ lumber input	6.1	5.3	6.9	Uniform [5.3, 6.9]
Planing shavings percentage [12,48]	%/m3 CLT input	4.0	3.6	4.5	Uniform [3.6, 4.5]
End cutting waste percentage [12,48]	%/m3 CLT input	12.8	12.2	13.4	Uniform [12.2, 13.4]
Total electricity consumption of CLT	kWh/m ³ final CLT	117.0	98.9	135	Uniform [98.9, 135]
production [12,41,48,49]	produced				

Table 1: Key parameters with variations and uncertainties in the CLT production

2.2 Economic Analysis of CLT Plant

This economic analysis focuses on the CLT plant with capacities ranging from $30,000-150,000 \text{ m}^3$ per year [4,41]. The mass balance data were fed into the economic analysis to determine the variable operating costs and equipment sizes that were used to scale the original purchased costs. The original purchased costs along with installing factors and scaling factors of each equipment were collected from the literature and manufacturer data. This study follows the n^{th} plant assumption which means a similar plant has been previously operated without unexpected startup delays and capacity loss [54,55]. Following Sections 2.2.1 and 2.2.2 will describe capital expenditures (CAPEX) and operating expenditures (OPEX).

A DCFROR analysis was established in EXCEL to calculate the MSP under varied scenarios [39,43–45,56]. Tab. 2 lists the assumptions and parameters used in the DCFROR analysis [54,57]. In the DCFROR spreadsheet, MSP is derived by setting IRR to be 10% and the Net Present Value (NPV) to be zero [45]. NPV was calculated by Eq. (1) [58,59], where a_t is the cash flow at time t with IRR r.

$$NPV = \sum_{t=0}^{n} \frac{a_t}{(1+r)^t}$$
(1)

2.2.1 CAPEX

The original purchased costs along with installing factors and scaling factors of each equipment were based on the literature and manufacturer information and then were scaled to the capacities by using scaling factors in this study. Tab. 3 shows the purchased costs and installed costs of the major areas at $30,000 \text{ m}^3$ CLT/year as an example. The detailed equipment list with scaling factors, purchased costs, and installed cost is available in Appendix A. Tab. S1. To adjust equipment purchase costs to the year of analysis 2018, plant cost indices by Chemical Engineering Magazine are used [60]. To account for the uncertainties of the equipment costs, this study adopts the data range to be $\pm 30\%$ which is commonly estimated as the accuracy of this scaling method in TEA [4,61].

Assumptions	Value
Year of analysis	2018
Internal rate of return	10%
Income tax rate	21%
Loan interest	8%
Loan years	10 years
Financing	40% by equity
Plant life	20 years
Plant construction time	36 months
Percentage of spending in year 1, 2, and 3	8% in year 1; 60% in year 2; 32% in year 3
Working capital	5% of fixed capital investment
Salvage value of plant	0
Start-up time	6 months
Revenues during start-up time	50%
Variable cost during start-up time	75%
Fixed cost during start-up time	100%

 Table 2: Economic assumptions for the CLT plant [54,57]

After the total installed cost (TIC) has been decided, there are several direct costs and indirect costs. These direct costs include warehouse, site development, and additional piping. Then the total direct costs (TDC) are the sum of TIC and these direct costs. The indirect costs contain prorated expenses, home office and construction fees, field expenses, project contingency, and other costs, which are calculated based on TDC [45]. Fixed capital investment (FCI) sums TDC and indirect costs. The land cost is assumed to be 60 acres at \$14,000 per acre [62]. Tab. 3 summarizes the assumptions in baseline costs related to direct and indirect costs. Tab. 4 lists the project cost assumptions.

Area	Purchased cost	Installed cost
Handling and preparation	\$984,479	\$1,554,528
End jointing	\$1,100,192	\$1,760,308
Layering and gluing	\$3,856,318	\$6,170,109
Pressing	\$675,980	\$1,081,568
Finishing	\$3,292,169	\$5,267,470
Miscellaneous	\$2,212,592	\$3,572,493
Total	\$12,121,730	\$19,406,475

Table 3: Purchased cost and installed cost (2018\$) of a CLT plant at 30,000 m³/year [41,45,63–65]

Assumptions	Value
Direct costs	
Warehouse	4.0% of ISBL
Site development	9.0% of ISBL
Additional piping	4.5% of ISBL
Indirect costs	
Prorated expenses	10% of TDC
Field expenses	10% of TDC
Home office & construction fees	20% of TDC
Project contingency	10% of TDC
Other costs	10% of TDC
Working capital	5% of FCI

Table 4: Project cost assumptions [45]

2.2.2 OPEX

The operating costs of the CLT plant contain two components. One is variable operating costs, including raw materials, waste stream charges, and fuel consumption. The other one is fixed operating costs, including labor cost and other overhead costs (i.e., maintenance and property insurance). For variable operating costs, the quantities of raw materials, waste streams, and energy consumption were decided by the process simulation. The variations and uncertainties in the prices of raw materials, waste stream charges, and fuels were collected from the literature and documented in Tab. 5 [66–71]. If the price is not in the year of analysis, then the Producer Price Index for chemical manufacturing is used to adjust the original prices [72]. The lumber price data were determined by the price range of 2018 in the U.S. [66,67]. It is noticeable that the lumber price could have much higher fluctuations. For example, the highest lumber price in 2020 under the COVID-19 pandemic situation recorded over \$400/m³ [66,67].

 Table 5: Variable operating costs and product prices (2018\$)

	Unit	Mean value	Minimum	Maximum	Assumed distribution
Lumber price [66,67]	\$ m ⁻³	142.5	123	162	Uniform [123, 162]
MF price [68]	\$ tonne ⁻¹	1540	1480	1600	Uniform [1480, 1600]
Electricity price [69]	cent per kWh	6.94	6.57	7.32	Uniform [6.57, 7.32]
Diesel price [70]	L^{-1}	0.84	0.79	0.89	Uniform [0.79, 0.89]
Waste disposal cost [71]	\$ m ⁻³	57.8	40.7	74.9	Uniform [40.7, 74.9]

For fixed operating costs, Tab. 6 exhibits the labor costs and other overhead costs at $30,000 \text{ m}^3$ CLT/year. The positions and salaries are based on the reports by the National Renewable Energy Laboratory (NREL) [54]. To adjust the salaries to the year of analysis, the labor index from the Bureau of Labor Statistics was used [73]. In this study, three shifts are assumed for the CLT plant. To account for the variations in operators needed, it is assumed 10–13 operators per shift for the plant at 30,000 m³/year.

Labor costs			
Positions	Salary	Number	Cost
Plant manager	184366	1	184,366
Plant engineer	87793	1	87,793
Maintenance supervisor	71489	1	71,489
Maintenance technician	50167	4	200,670
Shift supervisor	60201	1	60,201
Shift operator	50167	33 ^a	1,806,030
Yard employee	35117	1	35,117
Clerks & secretaries	45151	1	45,151
Total salaries			2,490,816
Benefits and overhead (90% of total salaries)			2,241,734
Other overhead costs			
Maintenance (3% of ISBL)			581,162
Insurance and taxes (1% of FCI)			255,322
Note: ^a Three shifts are assumed.			

Table 6: Fixed operating costs for the CLT plant at 30,000 m³ CLT/year (2018\$) [54]

2.3 Transportation Cost of Delivering CLT

2.3.1 Market Demanding of CLT

The market demanding of CLT panels in the southern U.S. is estimated by assuming the market share of commercial buildings at a county level based on the literature data [11,34,41,74,75]. Three different market demanding levels are modeled in this study: 1%, 5%, and 15%, representing low, medium, and high demanding level, respectively [11,34,41]. The annual CLT demanding at the county level in the southern U.S., is estimated by Eq. (2).

 $D_i = A_{commercial,i} \times F \times DL$

(2)

 D_i is the CLT demanding in county *i*; $A_{commercial,i}$ is the annual newly constructed floor area (m²) of commercial building in county *i*; DL is the market demanding level of CLT (1%, 5%, or 15%); *F* is the CLT usage factor (0.167 m³ CLT per m² floor area) that is evaluated based on the average value of the literature data [1,27,76,77]. $A_{commercial,i}$ is estimated by using the average U.S. new commercial building area per capita based on the Commercial Buildings Energy Consumption Survey (CBECS) data by U.S. Energy Information Agency (US EIA) [75]. In this study, the commercial buildings include traditional commercial buildings for religious worship, following the same definition given by US EIA [75]. An example of the county-level demanding results (1,339 counties) at 1% demanding level is presented in Fig. 2 (the results of 5% and 15% demanding levels are available in Appendix B. Figs. S1 and S2).

2.3.2 Transportation Distance

To estimate the travel cost at the county level, road distances between the CLT plant and geometric centers of counties within the whole south region were derived through Network Analysis in ArcGIS 10.6 [78]. In the road network analysis, the primary and secondary road system were considered and downloaded from the 2018 TIGER/Line shapefiles by US Census Bureau [79] (see Appendix B. Fig. S3).

The primary roads were the limited-access highways within the interstate highway system or under State management, and the secondary roads were main arteries within the U.S. Highway, State Highway, and County Highway systems [80]. For the average truck speed on two types of roads, it was assumed to be 113 km/h (70 mile/h) for all roads that contained "Hwy" (i.e., highway) in their full name and 89 km/hr (55 mile/h) for other non-highway roads, based on the report of U.S. Department of Transportation [81].



Figure 2: County-level CLT demanding results at 1% demanding level in the Southern U.S.

2.3.3 Transportation Cost Rate

The transportation cost T_i (\$/m³) for delivering 1 m³ CLT panels from the plant to county *i* (round trip) is estimated based on Eq. (3) [82,83]. The assumed values for the parameters in Eq. (3) are documented in Tab. 7. *l* and *u* is load time and unload time, respectively [83]. L_1 and L_2 the transportation distance of primary (i.e., Level 1) and secondary (i.e., Level 2) road, which is determined by the GIS model as shown in Section 2.3.2 v_1 and v_2 depict the average speed for Level 1 and Level 2 road. *c* describes the driver-based cost, including driver wages and benefits [82]; *p* is truck-based cost, including truck/trailer lease or purchase payment, repair and maintenance, insurance premiums, permits and licenses, tires, and tolls [82]; *f* is fuel cost based on the American Transportation Research Institute data (6.3 miles per gallon (2.7 L/km) for 60,00 lb operating weight) [82] and diesel price (\$3.18/gallon) by US EIA [84]. *m* is the weight load of CLT panels with an assumption of for 60,000 lb (27.2 metric ton) [82,83]; ρ is the average density of CLT panels.

$$T_{i} = \frac{\left(l + u + 2\left(\frac{L_{1i}}{v_{1}} + \frac{L_{2i}}{v_{2}}\right)\right)(c+p) + 2(L_{1i} + L_{2i})f}{m/\rho}$$
(3)

2.3.4 Least-Cost Route Determined by LP Model

An LP mathematical model was adopted to minimize the transportation cost of delivering the CLT panels. The input variables and decision variables are listed in Tab. 8. CLT demanding of county i in

each scenario, D_{is} , is derived based on the results of Section 2.3.1; the transportation cost T_i is derived from the results of Section 2.3.3. This study includes total 1,339 counties in L, 7 capacities of the CLT plant, and 21 scenarios in S (see Section 2.3.1). In this study, the LP problem is solved in MATLAB 2018 for each scenario.

Parameter	Value	Unit
Load time <i>l</i> [83]	0.5	h
Unload time <i>u</i> [83]	0.5	h
Average speed for Level 1 road v_1	88	km/h
Average speed for Level 2 road v_2	72	km/h
Driver-based cost c [82]	30.6	\$/h
Driver wage	23.5	\$/h
Driver benefit	7.1	\$/h
Truck-based cost p [82]	24.1	\$/h
Truck/trailer lease or purchase payment	10.4	\$/h
Repair and maintenance	6.7	\$/h
Insurance premiums	3.3	\$/h
Permits and licenses	1.0	\$/h
Tires	1.5	\$/h
Tolls	1.2	\$/h
Fuel cost <i>c</i> [82,84]	0.31	\$/km
Truck load m [82]	27.2	metric ton
CLT average density ρ [53]	495	kg/m ³

Table 7: Parameter values for transportation cost rate (2018\$)

Table 8: Input variables and decision variables of the LP model

Variables	Description
Input variables	
T_i	Transportation cost of delivering 1 m ³ CLT to county i
D_{is}	CLT demanding of county <i>i</i> in scenario <i>s</i>
L	Set of counties in the southern U.S.
Y_s	Capacity of the CLT plant in scenario s
S	Set of scenarios
Decision variables	
X _{is}	Volume of CLT delivered to county <i>i</i> in scenario <i>s</i>

There are two constraints involved in this problem. In constraint 1, the volume of delivered CLT panels to county *i* is no larger than the CLT demanding of county *i* in each scenario.

$$X_{is} \leq D_{is}, \quad \forall i \in L, \ s \in S$$

(3)In constraint 2, the total delivered CLT panels need to equal to the capacity of the CLT plant in each scenario.

$$\sum_{i} X_{is} = Y_s, \quad \forall s \in S \tag{4}$$

Hence, to minimize the average transportation $cost (\$/m^3)$, the LP model is formulated as follows:

$$\begin{array}{l} \min \ \sum\limits_i (T_i X_{is} / Y_s) \\ \text{s.t.} \ X_{is} \leq D_{is}, \ \forall i \in L, \ s \in S \\ \sum\limits_i X_{is} = Y_s, \ \forall s \in S \\ X_{is} \geq 0, \ \forall i \in L, \ s \in S \end{array}$$

2.4 Scenario Analysis

The scenario analysis, as shown in Tab. 9, was designed to explore the impacts of variations in plant capacity and CLT market demanding levels on the economic performance of producing CLT. The impacts of variations in other process parameters were explored by Monte Carlo simulation [48]. In this study, Monte Carlo simulation was performed for 1,000 iterations in each scenario using the probability density functions of parameters as shown in Tabs. 1, 3, and 6.

	Plant capacity (1,000 m ³ CLT/year)	CLT demanding level
Scenario 1-7	30, 50, 70, 90, 110, 130, 150	1%
Scenario 8-14		5%
Scenario 15-21		15%

Table 9: Scenario analysis

3 Results and Discussion

Fig. 3 exhibits the installed costs in each area, other direct cost, and indirect cost at varied plant capacities (30,000–150,000 m³/year). The error bars represent the 5th–95th percentile value range (P5– P95) of total capital investment from the Monte Carlo simulation. For varied plant capacities, increasing the capacity from 30,000 to 150,000 m³/year only raises the capital cost by 203%. Thus, increasing the plant capacity can lead to lower capital cost on a per cubic meter CLT basis. This further leads to the main driver of the decreasing MSP of CLT when increasing plant capacities (see Fig. 4). Among the installed costs of the equipment, layering and gluing (17% of the total capital investment), finishing (15% of the total capital investment), miscellaneous (9%-10%) of the total capital investment) are the major components. The other three areas account for less than 5% of the total capital investment. Besides the installed costs of equipment, the other direct cost (9% of the total capital investment) and indirect cost (38% of the total capital investment) contribute significantly to the capital investment. In this study, the variations in the equipment costs lead the total capital investment to vary 10% by P5-P95. Though the result range is smaller than the uncertainty range of equipment cost $(\pm 30\%)$, the uncertainty in capital investment needs to be considered in implementing the CLT plant.



Figure 3: Capital investment of the CLT plant under varied capacities



Figure 4: Operating cost of the CLT plant under varied capacities

Fig. 4 shows the operating cost of producing 1 m^3 CLT under varied capacities which consists of variable and fixed operating cost. The error bars represent the P5–P95 value range. Since the variable operating cost depends on 1 m^3 product basis, the variable operating cost does not change with varied plant capacities.

Among the variable operating costs, the lumber cost is the dominant part accounting for 85% of the total variable operating cost and 47%–68% of the total operating cost. The other material costs and energy costs are minor (less than 8% of the total operating cost). Hence, the lumber price can be a key factor that determines the total operating cost. On the other hand, the fixed operating cost, including labor cost and other fixed cost (maintenance, insurance and taxes), decreases along with the increased plant capacity. From 30,000 to 150,000 m³/year, the labor cost reduces from \$148.0 to \$37.8 per m³ CLT produced, and accounts for over 69% of the fixed operating cost. Hence, increasing the plant capacity can lead to the reduction of operating cost, which is a similar trend with the capital cost.

Fig. 5 shows the MSP of CLT at varied plant capacities. The box stands for the P5–P95 value range of the Monte Carlo simulation results with tails representing the minimum and maximum results. The overall MSP of CLT panels ranges from \$345 to \$609/m³ across all the capacity cases. Expanding the CLT plant capacity can significantly reduce the MSP of the CLT panels. For example, the median value of MSP at 30,000 m³/year is \$571/m³ (\$534–\$609/m³ P5–P95), compared to the median value \$376/m³ (\$345–\$410/m³ P5–P95) at 150,000 m³/year. This phenomenon is mainly driven by the reduction of capital cost and labor cost when the capacity is increased as mentioned above (see Figs. 3 and 4). The results presented in this study stay aligned with the literature data, approximately \$536–\$900/m³ [4,11,41]. The difference can be caused by varied wood type, lumber cost, labor employment, and plant location and capacity [4,11,41]. The uncertainties and variabilities from the manufacturing parameters, equipment cost, and operating cost, lead to the results varying by 6%–9% (based on P5 and P95).



Figure 5: The minimum selling price of CLT at varied plant capacities

Fig. 6 shows the delivered cost of CLT panels at varied plant capacities and demanding levels, with error bars showing the range of P5–P95. In Fig. 6, the delivered cost consists of MSP (solid bars) and transportation cost (pattern filled bars) at three demanding levels, namely 1% (orange bars), 5% (blue bars), and 15% (grey bars). First, compared to the MSP, the transportation cost of delivering the CLT panels is much smaller, accounting for 1%–8% of the delivered cost across all the cases. Second, the transportation cost increases as the demanding level decreases or the plant capacity increases. This is due to the decreased demanding level or increased plant capacity leads to longer transportation distances to deliver the CLT panels. For example, for a 150,000 m³/year plant, the transportation cost is \$33/m³ for 1%, \$15/m³ for 5%, and \$10/m³ for 15% demanding level. For 1% demanding level, increasing the capacity from 30,000 to 150,000 m³/year raises the transportation cost from \$15 to \$33/m³. Third, when considering varied demanding levels, larger plant capacity does not necessarily generate lower delivered cost. For example, the delivered cost at 150,000 m³/year with 1% demanding level (\$410/m³ mean value) is \$23 higher than 130,000 m³/year with 15% demanding level. Hence, the results show the necessity of considering the potential demanding conditions in implanting CLT plants.



Figure 6: The delivered cost of CLT at varied plant capacities and demanding levels

To further identify the key drivers of the economic feasibility for CLT panels, this study conducted a sensitivity analysis. The baseline was chosen as the 110,000 m³/year plant as shown in Fig. 7. In the sensitivity analysis, the parameters can be categorized into three groups, manufacturing parameters, operating cost parameters, and capital cost parameters. Among manufacturing parameters, the plant capacity and the lumber preparing loss are the key driving factors that affect the MSP. A potential increase in the preparing loss (due to trimmed defects or lumber below the quality requirement) from 7% to 14% can lead to a $19/m^3$ increase in MSP. Lumber price, the largest portion of operating costs (see Fig. 4), is another key driver for the MSP. Hence, lowering the feedstock cost, choosing qualified feedstock, and reducing the loss in lumber preparation can be potentially effective strategies to reach lower MSP. For the capital costs, the installed costs of layering and gluing, finishing, miscellaneous are among the top ones that affect the MSP, which stays aligned with the results shown in Fig. 3.



Figure 7: Sensitivity analysis results of MSP (baseline selected as the 110,000 m³/year plant)

4 Conclusions

This study explores the economic performance of producing CLT from softwood lumber in the Southern U.S. and considers the effects of variations in plant capacities, key manufacturing parameters, material and energy cost on MSP of CLT panels. The overall MSP ranges from \$345 to \$609/m³ across all the capacity cases from 30,000 to 150,000 m³/year. Enlarging the CLT plant capacity can significantly reduce the MSP due to the reduced capital cost and fixed operating cost per m³ CLT. The effects of variations in the feedstock, key manufacturing parameters, capital and operating cost, can cause a $\pm 6\%$ –9% range (P5–P95 value) in the MSP. This study also studies the transportation cost of delivering CLT from the plant to consumers supported by GIS. Three CLT demanding levels were included, 1%, 5%, and 15%. This study concludes that the transportation cost of delivering the CLT panels is much smaller (1%-8%) compared to the MSP. The transportation cost increases as the demanding level decreases or the plant capacity increases due to average longer delivering distances. Thus, when considering varied demanding levels, larger plant capacity does not necessarily generate lower delivered cost that consists of MSP and transportation cost. To identify the key drivers of the economic feasibility, this study performances a sensitivity analysis and shows that the lumber price, lumber preparing loss, plant capacity, and the installed costs of layering and gluing, finishing, and miscellaneous, are the top driving factors. This conclusion also exhibits the further direction of lowering the production cost of CLT panels.

Acknowledgement: The authors thank the support from North Carolina State University.

Funding Statement: The authors received no specific funding for this study.

Conflicts of Interest: The authors declare that they have no conflicts of interest to report regarding the present study.

References

- Robertson, A. B., Lam, F. C., Cole, R. J. (2012). A comparative cradle-to-gate life cycle assessment of mid-rise office building construction alternatives: Laminated timber or reinforced concrete. *Buildings*, 2(3), 245–270. DOI 10.3390/buildings2030245.
- Fatahi, B., Tabatabaiefar, S. H. R. (2014). Fully nonlinear versus equivalent linear computation method for seismic analysis of midrise buildings on soft soils. *International Journal of Geomechanics*, 14(4), 04014016. DOI 10.1061/(ASCE)GM.1943-5622.0000354.
- Liu, Y., Guo, H., Sun, C., Chang, W. S. (2016). Assessing cross laminated timber (CLT) as an alternative material for mid-rise residential buildings in cold regions in China—A life-cycle assessment approach. *Sustainability*, 8(10), 1047. DOI 10.3390/su8101047.
- 4. Brandt, K., Wilson, A., Bender, D., Dolan, J. D., Wolcott, M. P. (2019). Techno-economic analysis for manufacturing cross-laminated timber. *BioResources*, 14(4), 7790–7804. DOI 10.15376/biores.
- Gong, Y., Liu, F., Tian, Z., Wu, G., Ren, H. et al. (2019). Evaluation of mechanical properties of cross-laminated timber with different lay-ups using Japanese larch. *Journal of Renewable Materials*, 7(10), 941–956. DOI 10.32604/jrm.2019.07354.
- Chen, Z., Lu, W., Bao, Y., Zhang, J., Wang, L. et al. (2021). Numerical investigation of connection performance of timber-concrete composite slabs with inclined self-tapping screws under high temperature. *Journal of Renewable Materials*. DOI 10.32604/jrm.2021.015925.
- ANSI/APA PRG (2012). ANSI/APA PRG 320-2012 Standard for Performance-Rated Cross-Laminated Timber. https://www.apawood.org/ansi-apa-prg-320.
- 8. Wang, G. (2018). *Hygrothermal performance of southern pine cross-laminated timber (Ph.D. Thesis)*. North Carolian State University, USA.

- 9. Sun, J., Niederwestberg, J., Cheng, F., Chui, Y. (2020). Frequencies prediction of laminated timber plates using ANN approach. *Journal of Renewable Materials*, *8*(3), 319. DOI 10.32604/jrm.2020.08696.
- Yang, H., Ji, J., Tao, H., Shi, B., Hu, J. et al. (2021). Pull-out behaviour of axially loaded screwed-in threaded rods embedded in CLT elements: Experimental study. *Journal of Renewable Materials*, DOI 10.32604/ jrm.2021.016118.
- 11. FPInnovations (2013). CLT Handbook US Edition. <u>https://www.seattle.gov/dpd/cms/groups/pan/@pan/</u>documents/web_informational/dpds021903.pdf.
- 12. Puettmann, M., Sinha, A., Ganguly, I. (2018). CORRIM Report-life cyle assessment of cross laminated timber produced in oregon. <u>https://corrim.org/wp-content/uploads/2019/02/Life-Cycle-Assessment-of-Oregon-Cross-Laminated-Timber.pdf</u>.
- 13. Klippel, M., Schmid, J. (2017). Design of cross-laminated timber in fire. *Structural Engineering International*, 27(2), 224–230. DOI 10.2749/101686617X14881932436096.
- 14. Frangi, A., Fontana, M., Hugi, E., Jübstl, R. (2009). Experimental analysis of cross-laminated timber panels in fire. *Fire Safety Journal*, 44(8), 1078–1087. DOI 10.1016/j.firesaf.2009.07.007.
- 15. Schmid, J., König, J., Köhler, J. (2010). Fire-exposed cross-laminated timber-modelling and tests. *World Conference on Timber Engineering*, Trentino, Italy.
- 16. Hasburgh, L., Bourne, K., Peralta, P., Mitchell, P., Schiff, S. et al. (2016). Effect of adhesives and ply configuration on the fire performance of southern pine cross-laminated timber. *World Conference on Timber Engineering*, Vienna, Austria.
- 17. Hasburgh, L., Bourne, K., Dagenais, C., Ranger, L., Roy-Poirier, A. (2016). Fire performance of mass-timber encapsulation methods and the effect of encapsulation on char rate of cross-laminated timber. *World Conference on Timber Engineering*, Vienna, Austria.
- Asdrubali, F., Ferracuti, B., Lombardi, L., Guattari, C., Evangelisti, L. et al. (2017). A review of structural, thermophysical, acoustical, and environmental properties of wooden materials for building applications. *Building and Environment*, 114, 307–332. DOI 10.1016/j.buildenv.2016.12.033.
- 19. Mallo, M. F. L., Espinoza, O. A. (2014). Outlook for cross-laminated timber in the United States. *BioResources*, 9(4), 7427–7443. DOI 10.15376/biores.9.4.7427-7443.
- 20. Öqvist, R., Ljunggren, F., Ågren, A. (2012). On the uncertainty of building acoustic measurements-case study of a cross-laminated timber construction. *Applied Acoustics*, 73(9), 904–912. DOI 10.1016/j.apacoust.2012.03.012.
- Pérez, M. (2013). Acoustic design through predictive methods in cross laminated timber (CLT) panel structures in buildings. *INTER-NOISE and NOISE-CON Congress and Conference Proceedings*, vol. 247, pp. 5539–5547, Institute of Noise Control Engineering. Innsbruck, Austria.
- 22. Sharifnia, H., Hindman, D. P. (2017). Effect of manufacturing parameters on mechanical properties of southern yellow pine cross laminated timbers. *Construction and Building Materials*, *156*, 314–320. DOI 10.1016/j. conbuildmat.2017.08.122.
- Hindman, D. P., Bouldin, J. C. (2015). Mechanical properties of southern pine cross-laminated timber. *Journal of Materials in Civil Engineering*, 27(9), 04014251. DOI 10.1061/(ASCE)MT.1943-5533.0001203.
- 24. Gu, M. (2017). Strength and serviceability performances of southern yellow pine cross-laminated timber (CLT) and CLT-glulam composite beam (Ph.D. Thesis). Clemson University, USA.
- Okabe, M., Yasumura, M., Kobayashi, K. (2014). Estimation of bending stiffness, moment carrying capacity and internal shear force of sugi CLT panels. *Proceedings of World Conference on Timber Engineering*, Quebec City, Canada, pp. 10–14.
- Kramer, A., Barbosa, A. R., Sinha, A. (2014). Viability of hybrid poplar in ANSI approved cross-laminated timber applications. *Journal of Materials in Civil Engineering*, 26(7), 06014009. DOI 10.1061/(ASCE)MT.1943-5533.0000936.
- Gu, H., Bergman, R. (2018). Life cycle assessment and environmental building declaration for the design building at the University of Massachusetts. *General Technical Report FPL-GTR-255*. Madison, WI: US Department of Agriculture, Forest Service, Forest Products Laboratory.

- Brandner, R., Flatscher, G., Ringhofer, A., Schickhofer, G., Thiel, A. (2016). Cross laminated timber (CLT): Overview and development. *European Journal of Wood and Wood Products*, 74(3), 331–351. DOI 10.1007/ s00107-015-0999-5.
- 29. Passarelli, R. N. (2018). The environmental impact of reused CLT panels: Study of a single-storey commercial building in Japan. *World Conference on Timber Engineering*, Seoul, Korea.
- Dong, Y., Cui, X., Yin, X., Chen, Y., Guo, H. (2019). Assessment of energy saving potential by replacing conventional materials by cross laminated timber (CLT)—A case study of office buildings in China. *Applied Sciences*, 9(5), 858. DOI 10.3390/app9050858.
- Lan, K., Kelley, S. S., Prakash Nepal, Y. Y. (2020). Dynamic life cycle carbon and energy analysis for crosslaminated timber in the southeastern United States. *Environmental Research Letters*, 15(12), 124036. DOI 10.1088/1748-9326/abc5e6.
- Ganguly, I., Beyreuther, T., Hoffman, M., Swenson, S., Eastin, I. (2017). Forecasting the demand for cross laminated timber (CLT) in the Pacific Northwest. <u>https://www.cintrafor.org/publications/forecasting-the-</u> demand-for-cross-laminated-timber-clt-in-the-pacific-northwest.
- Energias (2018). Global cross laminated timber (CLT) market outlook, trend and opportunity analysis, competitive insights, actionable segmentation & forecast 2024. <u>https://www.energiasmarketresearch.com/global-cross-</u> laminated-timber-market-outlook/.
- Beck Group (2018). Mass timber market analysis. <u>https://www.oregon.gov/ODF/Documents/ForestBenefits/Beck-mass-timber-market-analysis-report.pdf</u>.
- 35. APA (2020). CLT manufacturers. https://www.apawood.org/cross-laminated-timber#:~:text=CLT Manufacturers, LLC Kalesnikoff Mass Timber%2C Inc.
- Espinoza, O., Buehlmann, U., Laguarda, M., Trujillo, V. R. (2016). Identification of research areas to advance the adoption of cross-laminated timber in North America. *BioProducts Business*, 1(5), 60–72. DOI 10.22382/bpb-2016-005.
- 37. Albee, R. R. (2019). Global overview of the cross-laminated timber industry (Master Thesis). Oregon State University, USA.
- Lan, K., Park, S., Kelley, S. S., English, B. C., Yu, T. H. E. et al. (2020). Impacts of uncertain feedstock quality on the economic feasibility of fast pyrolysis biorefineries with blended feedstocks and decentralized preprocessing sites in the southeastern United States. *GCB Bioenergy*, *12(11)*, 1014–1029. DOI 10.1111/gcbb.12752.
- Wright, M. M., Daugaard, D. E., Satrio, J. A., Brown, R. C. (2010). Techno-economic analysis of biomass fast pyrolysis to transportation fuels. *Fuel*, 89, S2–S10. DOI 10.1016/j.fuel.2010.07.029.
- Sahoo, K., Bilek, E. T., Mani, S. (2018). Techno-economic and environmental assessments of storing woodchips and pellets for bioenergy applications. *Renewable and Sustainable Energy Reviews*, 98, 27–39. DOI 10.1016/j. rser.2018.08.055.
- 41. Bédard, P., Fournier, F., Gagnon, S., Gingras, A., Lavoie, V. et al. (2010). Manufacturing cross-laminated timber (CLT) technological and economic analysis. https://library.fpinnovations.ca/en/permalink/fpipub39323.
- Shahrukh, H., Oyedun, A. O., Kumar, A., Ghiasi, B., Kumar, L. et al. (2016). Techno-economic assessment of pellets produced from steam pretreated biomass feedstock. *Biomass and Bioenergy*, 87, 131–143. DOI 10.1016/ j.biombioe.2016.03.001.
- Sahoo, K., Bilek, E., Bergman, R., Mani, S. (2019). Techno-economic analysis of producing solid biofuels and biochar from forest residues using portable systems. *Applied Energy*, 235, 578–590. DOI 10.1016/j. apenergy.2018.10.076.
- Swanson, R. M., Platon, A., Satrio, J. A., Brown, R. C. (2010). Techno-economic analysis of biomass-to-liquids production based on gasification. *Fuel*, 89, S11–S19. DOI 10.1016/j.fuel.2010.07.027.
- Humbird, D., Davis, R., Tao, L., Kinchin, C., Hsu, D. et al. (2011). Process design and economics for biochemical conversion of lignocellulosic biomass to ethanol: Dilute-acid pretreatment and enzymatic hydrolysis of corn stover (No. NREL/TP-5100-47764), National Renewable Energy Laboratory (NREL), Golden, USA.
- ANSI/APA (2019). ANSI/APA PRG 320-2019 Standard for Performance-Rated Cross-Laminated Timber. <u>https://www.apawood.org/ansi-apa-prg-320</u>.

- 47. Muszynski, L. (2017). Effective bonding parameters for hybrid cross-laminated timber (CLT) (Master Thesis). Oregon State University, USA.
- Chen, C. X., Pierobon, F., Ganguly, I. (2019). Life cycle assessment (LCA) of cross-laminated timber (CLT) produced in western Washington: The role of logistics and wood species mix. *Sustainability*, 11(5), 1278. DOI 10.3390/su11051278.
- 49. ASMI (2013). A life cycle assessment of cross-laminated timber produced in Canada. <u>http://www.athenasmi.org/</u>resources/publications/.
- 50. Popovski, M., Gavric, I. (2016). Performance of a 2-story CLT house subjected to lateral loads. *Journal of Structural Engineering*, 142(4), E4015006. DOI 10.1061/(ASCE)ST.1943-541X.0001315.
- 51. Patterson, D. W., Doruska, P. F., Posey, T. (2004). Weight and bulk density of loblolly pine plywood logs in southeast Arkansas. *Forest Products Journal*, 54(12), 145–149.
- 52. Patterson, D. W., Clark III, A. (1988). Bulk density of southern pine logs. Forest Products Journal, 38, 36-40.
- 53. Miles, P. D., Smith, W. B. (2009). Specific gravity and other properties of wood and bark for 156 tree species found *in North America*, vol. 38. US Department of Agriculture, Forest Service, Northern Research Station.
- 54. Dutta, A., Sahir, A. H., Tan, E., Humbird, D., Snowden-Swan, L. J. et al. (2015). Process design and economics for the conversion of lignocellulosic biomass to hydrocarbon fuels: Thermochemical research pathways with in Situ and ex Situ upgrading of fast pyrolyss vapors (No. PNNL-23823), Pacific Northwest National Laboratory (PNNL), Richland, USA.
- 55. Kazi, F. K., Fortman, J., Anex, R., Kothandaraman, G., Hsu, D. et al. (2010). *Techno-economic analysis of biochemical scenarios for production of cellulosic ethanol (No.* NREL/TP-6A2-46588). National Renewable Energy Laboratory (NREL), Golden, USA.
- 56. Ou, L., Kim, H., Kelley, S., Park, S. (2018). Impacts of feedstock properties on the process economics of fastpyrolysis biorefineries. *Biofuels, Bioproducts and Biorefining, 12(3),* 442–452. DOI 10.1002/bbb.1860.
- Jones, S. B., Meyer, P. A., Snowden-Swan, L. J., Padmaperuma, A. B., Tan, E. et al. (2013). Process design and economics for the conversion of lignocellulosic biomass to hydrocarbon fuels: Fast pyrolysis and hydrotreating bio-oil pathway (No. PNNL-23053; NREL/TP-5100-61178). Pacific Northwest National Laboratory (PNNL), Richland, USA.
- 58. Beaves, R. G. (1988). Net present value and rate of return: Implicit and explicit reinvestment assumptions. *The Engineering Economist*, 33(4), 275–302. DOI 10.1080/00137918808966958.
- 59. Osborne, M. J. (2010). A resolution to the NPV–IRR debate? *The Quarterly Review of Economics and Finance*, *50(2)*, 234–239. DOI 10.1016/j.qref.2010.01.002.
- 60. Chemical Engineering Magazine (2019). Plant cost index. <u>https://www.bing.com/search?q=Chemical+Engineering</u> +Magazine.+(2015).+Plant+Cost+Index.&cvid=fe1d10de53d04969b721e43428d8e2a8&aqs=edge..69i57. 337j0j9&FORM=ANAB01&PC=LCTS.
- 61. Peters, M. S., Timmerhaus, K. D., West, R. E. (2003). *Plant design and economics for chemical engineers*, vol. 4. New York: McGraw-Hill.
- 62. Tao, L., Markham, J. N., Haq, Z., Biddy, M. J. (2017). Techno-economic analysis for upgrading the biomassderived ethanol-to-jet blendstocks. *Green Chemistry*, 19(4), 1082–1101. DOI 10.1039/C6GC02800D.
- Pirraglia, A., Gonzalez, R., Saloni, D., Denig, J. (2013). Technical and economic assessment for the production of torrefied ligno-cellulosic biomass pellets in the US. *Energy Conversion and Management*, 66, 153–164. DOI 10.1016/j.enconman.2012.09.024.
- Turner, T. A., Harper, L. T., Warrior, N. A., Rudd, C. D. (2008). Low-cost carbon-fibre-based automotive body panel systems: A performance and manufacturing cost comparison. *Proceedings of the Institution of Mechanical Engineers, Part D: Journal of Automobile Engineering, 222(1),* 53–63. DOI 10.1243/ 09544070JAUTO406.
- 65. Alibaba (2020). Edge trimming machine. <u>https://www.alibaba.com/product-detail/45-degree-edge-banding-machinechina 62070871941.html?spm=a2700.galleryofferlist.normal offer.d title.4b02eb8eAsmedw&s =p&fullFirstScreen=true.</u>
- 66. Trading Economics (2019). Lumber price. https://tradingeconomics.com/commodity/lumber.

- 67. Federal Reserve Bank of St. Louis (2019). Producer price index by commodity: Lumber and wood products: Softwood lumber. https://fred.stlouisfed.org/series/WPU0811.
- 68. Alibaba.com (2019). Melamine formaldehyde price. <u>https://www.alibaba.com/showroom/melamine-formaldehyde-resins.html</u>.
- 69. US EIA (2019). Average price of electricity to ultimate customers by End-use sector. <u>https://www.eia.gov/</u>electricity/monthly/epm_table_grapher.php?t=epmt_5_6_a.
- 70. US EIA (2019). Weekly retail gasoline and diesel prices. <u>https://www.eia.gov/dnav/pet/pet_pri_gnd_dcus_nus_m.</u> <u>htm</u>.
- US EPA (2014). Municipal solid waste landfills economic impact analysis for the proposed New subpart to the New source performance standards. <u>https://www3.epa.gov/ttnecas1/docs/eia_ip/solid-waste_eia_nsps_proposal_07-2014.pdf</u>.
- 72. Bureau of Labor Statistics (2020). Producer price indexes. https://www.bls.gov/pPI/.
- 73. Bureau of Labor Statistics (2020). Labor index by bureau of labor statistics. https://data.bls.gov/cgi-bin/srgate.
- 74. United States Census Bureau (2019). Building permits survey. https://www.census.gov/construction/bps/.
- 75. US EIA (2016). 2012 commercial buildings energy consumption survey (CBECS) survey data. <u>https://www.eia.gov/consumption/commercial/data/2012/</u>.
- 76. Chen, Y. (2012). Comparison of environmental performance of a five-storey building built with cross-laminated timber and concrete. Sustainable building science program. University of British Columbia-Department of Wood Science, Vancouver, BC, Canada.
- Pierobon, F., Huang, M., Simonen, K., Ganguly, I. (2019). Environmental benefits of using hybrid CLT structure in midrise non-residential construction: An LCA based comparative case study in the US pacific northwest. *Journal* of *Building Engineering*, 26, 100862. DOI 10.1016/j.jobe.2019.100862.
- 78. ESRI (2020). ArcGIS 10.6. https://desktop.arcgis.com/en/arcmap/.
- US Census Bureau Department of Commerce (2018). TIGER/line shapefile, series information for the primary and secondary roads state-based shapefile. <u>https://catalog.data.gov/dataset/tiger-line-shapefile-2018-series-information-for-the-primary-and-secondary-roads-state-based-sh.</u>
- 80. US Census Bureau Department of Commerce (2009). 2009 TIGER/Line shapefiles technical documentation. https://www2.census.gov/geo/pdfs/maps-data/data/tiger/tgrshp2009/TGRSHP09AF.pdf.
- 81. Skszek, S. L. (2004). Actual speeds on the roads compared to the posted limits. <u>https://safety.fhwa.dot.gov/</u> speedmgt/ref_mats/fhwasa09028/resources/actual speeds on roadtopostedlimits.pdf.
- 82. Murray, D., Glidewell, S. (2019). An analysis of the operational costs of trucking: 2019 update. <u>https://</u> truckingresearch.org/wp-content/uploads/2019/11/ATRI-Operational-Costs-of-Trucking-2019-1.pdf.
- Wells, L. A., Chung, W., Anderson, N. M., Hogland, J. S. (2016). Spatial and temporal quantification of forest residue volumes and delivered costs. *Canadian Journal of Forest Research*, 46(6), 832–843. DOI 10.1139/cjfr-2015-0451.
- 84. US EIA (2020). U.S. No 2 diesel retail prices. <u>https://www.eia.gov/dnav/pet/hist/LeafHandler.ashx?</u> n=PET&s=EMD_EPD2D_PTE_NUS_DPG&f=M.

Appendix A. Supplementary tables

Equipment list	Scaling factor	Purchased cost	Installed cost	
	Handling and preparation			
Forklift	0.70	\$34,396	\$34,396	
Lumber feeding system	0.70	\$181,385	\$290,216	
Lumber moisture meter	0.70	\$30,796	\$49,273	
Lumber scanner	0.70	\$342,236	\$547,578	
Lumber grading station	0.70	\$284,056	\$454,490	
Trim saw	1.00	\$60,274	\$96,439	
Conveyors	0.70	\$51,335	\$82,137	
Subtotal		\$984,479	\$1,554,528	
	End jointing			
Block storage feeding	0.70	\$181,385	\$290,216	
Finger jointing system	0.70	\$867,472	\$1,387,955	
Conveyors	0.70	\$51,335	\$82,137	
Subtotal		\$1,100,192	\$1,760,308	
	Layering and glu	ing		
Edge gluing layering pressing	0.70	\$3,272,463	\$5,235,941	
Glue spreader	0.70	\$532,520	\$852,031	
Conveyors	0.70	\$51,335	\$82,137	
Subtotal		\$3,856,318	\$6,170,109	
	Pressing			
Panel pressing machine	0.7	\$675,980	\$1,081,568	
Subtotal		\$675,980	\$1,081,568	
	Finishing			
Planer	0.70	\$698,162	\$1,117,059	
Trimming machine	0.70	\$282,543	\$452,069	
CNC system	0.7	\$2,311,464	\$3,698,342	
Subtotal		\$3,292,169	\$5,267,470	
	Miscellaneous			
Dust collecting system	0.60	\$323,448	\$549,862	
Packing system	0.70	\$136,894	\$219,031	
Accumulator, feeder, conveyor	0.70	\$1,752,250	\$2,803,599	
Subtotal		\$2,212,592	\$3,572,493	
Total		\$12,121,730	\$19,406,475	

Table S1: Equipment list and cost (2018\$) of a CLT plant at 30,000 m³/year [41,45,63–65]
--

Appendix B. Supplementary figures



Figure S1: County-level CLT demanding results at 5% demanding level in the southern U.S.



Figure S2: County-level CLT demanding results at 15% demanding level in the southern U.S.



Figure S3: County-level route analysis of transportation in the southern U.S.