

DOI: 10.32604/cmes.2022.021783

ARTICLE



Bio-Inspired Optimal Dispatching of Wind Power Consumption Considering Multi-Time Scale Demand Response and High-Energy Load Participation

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Received: 04 February 2022 Accepted: 24 March 2022

ABSTRACT

Bio-inspired computer modelling brings solutions from the living phenomena or biological systems to engineering domains. To overcome the obstruction problem of large-scale wind power consumption in Northwest China, this paper constructs a bio-inspired computer model. It is an optimal wind power consumption dispatching model of multi-time scale demand response that takes into account the involved high-energy load. First, the principle of wind power obstruction with the involvement of a high-energy load is examined in this work. In this step, high-energy load model with different regulation characteristics is established. Then, considering the multi-time scale characteristics of high-energy load and other demand-side resources response speed, a multi-time scale model of coordination optimization is built. An improved bio-inspired model incorporating particle swarm optimization is applied to minimize system operation and wind curtailment costs, as well as to find the most optimal energy configuration within the system. Lastly, we take an example of regional power grid in Gansu Province for simulation analysis. Results demonstrate that the suggested scheduling strategy can significantly enhance the wind power consumption level and minimize the system's operational cost.

KEYWORDS

Biological system; multi-time scale; wind power consumption; demand response; bio-inspired computer modelling; particle swarm optimization

1 Introduction

China's wind power industry keeps a quick increase in recent years. According to the National Energy Bureau data, at December 2019, the country's total wind power installation capacity was 210 million kW, among which three provinces of Xinjiang, Gansu, Inner Mongolia had a capacity of 60.57 million kW [1], accounting for 28.84% of the total installed capacity. However, the problem of wind abandonment in the three provinces is also serious, and the total wind abandonment rate is as high as 28.7% [2]. The issue of blocked wind power consumption has become one of the constraints for the wind power market's expansion in China.



When traditional thermal power units' peak regulation capability is insufficient to consume wind power completely, using load-side resources to participate in system regulation can provide output space for large-scale integration of wind power [3–6]. Zhang et al. [7] regulates the load through price-based demand response (DR) to actively adjust the system peak and configure the energy storage device at the source side. As a result, the system operation cost is reduced, and the system wind is reduced. Tan et al. [8] combines price-based and incentive DR: it verifies that wind power absorption is significantly increased after the introduction of DR. Tan et al. [9] proposed a two-stage scheduling optimization model, in consideration of DR and energy storage system, to fix the problem by chaotic binary particle swarm optimization algorithm. It revealed that the synergistic effect of DR and energy storage systems could inhibit the uncertainty of wind power and lessen the system's wind curtailment rate. The above literatures have some valuable points in using load-side resources to ease the system's wind curtailment problem.

In July 2020, China's Northwest Power Grid has 14 high-capacity enterprises participating in market regulation, reaching a total peak capacity of 532,000 kW. Therefore, the use of high energy load in the northwest region to attack wind curtailment has certain practical significance [10–12]. Li et al. [13] proposed a 'source-load' coordinated scheduling model for high energy load and conventional power supply, which offers a novel approach to solving the issues of wind abandonment. Zhang et al. [14] designed a coordinated scheduling strategy of high-energy load and wind power to take into account the load side's risk constraint to solve the issue of load and wind power mismatch. In reference [15], taking the maximum wind power consumption rate as the objective function, a peak-valley electricity price decision model considering the contribution of high energy load in peak shaving is established to encourage enterprises to take an active role in peak shaving.

The above literature offers a new perspective on the study of high energy load participation in wind power consumption in Northwest China, but there are still the following deficiencies:

- (1) At present, most studies on high energy load only consider a single model rather than modeling it independently based on the high energy load's operation characteristics.
- (2) There is no consideration of the difference in the response speed of different types of high load energy to the dispatching signal.
- (3) The multi-time scale characteristics of high energy load and other demand-side resources are not combined to construct the multi-time scale optimization model of DR to engage in wind power consumption.

For solving the problems of the human real-world, researchers have resorted to nature and biology for a long time. The study of nature theories and principles such as biological structures and bionics bridges have brought development of many mathematical and metaheuristic algorithms by referring to these bio-inspired principles. Bio-inspired modeling researches computerized solutions from living phenomena or biological systems. They have great potential applications in areas such as Internet of Things (IoT) [16–20], Internet of Vehicles (IoV) [21,22], block chain [23–26], image processing [27–31], privacy-preserving [32–34], unmanned aerial vehicles (UAVs) [35–38], medical treatment [39–43] and communication [44,45]. An increasing number of bio-inspired algorithms have been developed in recent decades. Many intelligent algorithms have been adopted recently, such as artificial intelligence algorithms [46–48], the mathematical analytic methods [49–52], ant colonial algorithm [53,54], genetic algorithm [55], particle swarm algorithm, deep learning [56,57] and so forth. Previous studies introduced a mixed-integer linear programming approach to maximize system performance and improve system operational stability [58]. RM et al. [59] proposed an energy efficient cloud algorithm based on Internet of Everything via the wind-driven optimization algorithm and

firefly bio-inspired algorithm to handle this heavy flow of data traffic and process within the cloud computing edge. In reference [60], an optimal cluster head strategy is proposed via the employment of a hybrid WOA-MFO model, which optimizes the environmental and network factors. Similarly, the reference [61] designed an advanced approach for cluster head selection through an improved Rider optimization algorithm to optimize the delay minimization, energy sustainability in the IoT system. Neves et al. apply GA to minimize system operation costs in [62], comparing with other algorithms, PSO algorithm is considered more promising in dealing with multi-objective optimization problems. Kerdphol et al. applyed the PSO algorithm to optimize the MG energy storage system [63]. However, the basic PSO algorithm tends to easily fall into a local minimum. Thus, many improvements have been made to solve the disadvantage. To avoid the weaknesses of the PSO algorithm, the acceleration factor is used reasonably to improve the performance of the optimal operation in the power system.

In conclusion, this research examines the principle of high energy load participating in the system to absorb wind power and divides it into discrete adjustable load and continuously adjustable load according to the different operation modes of participating in DR. This study presents an improved bio-inspired algorithm for overcoming the obstruction problem of the large-scale wind power consumption. The main contributions of this work are summarized as follows: (1) The modeling of high energy load based on load characteristics has been designed to show the operation state. (2) The multi-time scale properties of high-energy load and DR are taken into account to minimize the operation cost and maximize the wind power consumption. (3) An improved bio-inspired PSO algorithm has been proposed to overcome the regionally optimal renewable energy power system problem.

2 Load Regulation Characteristics of High Load Energy

2.1 The Principle of High Load Energy-Absorbing Blocked Wind Power

When wind power is at high risk of failure and power generation is constrained, the wind power enterprises can lower the peak-valley difference of equivalent load by coordinating with the high-energy enterprises and adjusting the duration period of high-energy load to improve wind power consumption. High load energy could be used as a resource to absorb wind power specifically in the two aspects as follows:

- (1) With large adjustable capacity, wind power can be absorbed by increasing output when conventional load is low through load transfer.
- (2) The quick response: some high-energy loads can be quickly changed according to the fluctuation of wind power, with a high degree of automation.

In Fig. 1, Region 1 represents the peak regulation range of thermal power units. If the system's initial load curve is superposed with the negative wind power output curve, the system's equivalent load curve can be obtained. The equivalent load P_E expression is:

$$P_E = P_L - P_W \tag{1}$$

 P_L is the system's initial load value when the high load is not involved in regulation; P_W represents wind power output.



Figure 1: Principal diagram of high load energy accommodating impeded wind power

Region 2 represents the abandoned air volume of the system under the traditional control mode. It is apparent from Fig. 1 that the equivalent load value in $t_1 - t_2$ period is smaller than the minimum technical the thermal power unit's output, that is, in this period, the thermal power unit's peak regulation cannot completely suppress the wind power fluctuation, and only the wind power curtailment can be a solution to guarantee the system's operation safety. The abandoned air volume is:

$$E_{W} = \sum_{t=t_{1}}^{t_{2}} (P_{G,min} - P_{L} + P_{W}) \Delta t$$
⁽²⁾

When the high energy load is involved in the regulation and control, the power ΔP_H is transferred into the $t_1 - t_2$ period, the wind power blocked power will be reduced from Region 2 to Region 3, and the abandoned air volume is:

$$E'_{W} = \sum_{t=t_{1}}^{t_{2}} (P_{G,min} - P_{L} + P_{W} + P_{H})\Delta t$$
(3)

Eqs. (2) and (3) shows that the new wind power consumption after high-load energy load participating in regulation is:

$$E_{new} = \sum_{t=t_1}^{t_2} P_H \Delta t \tag{4}$$

Therefore, high load energy regulation can greatly minimize abandoned wind power while also improving the power grid's ability to absorb wind power.

2.2 Regulation Characteristics of High Load Energy

We divide high-energy loads into discrete and continuous types [64].

(1) Discrete high-energy load is the part that can reduce or increase quantitative load corresponding to the power grid dispatch center's instructions within a given time frame. However, the input or interruption of high-energy load needs a consistently stable period; once the adjustment is carried out, the load power must be maintained for a limited time. It is unable to respond frequently to the adjustment demands, so that is suitable for day-ahead scheduling mode. Take a silicon carbide enterprise as an example. The smelting furnace can be adjusted within the rated capacity range of $80\% \sim 120\%$, with a sustainable time of 4 h and a discrete adjustment time interval of not less than 1 h.

The formula of the discretely adjustable load is described as:

$$P_{DH}(t) = \sum_{i=1}^{J_{th}} \left(P_{DH,i}(t-1) + x_{DH,i} \Delta P_{DH,i}(t) \right)$$
(5)

where *t* is time, P_{DH} (t) denotes the total load of discretely adjustable load at t. N_{DH} denotes the number of discrete high-energy load units. $x_{DH,i}$ denotes the state variable of the i_{th} discretely adjustable unit, the unit participates in the regulation when the value *i* is 1. $\Delta P_{DH,i}$ is the regulation quantity of discretely adjustable load of the i_{th} unit.

(2) Continuous high energy load is the part that is continuously adjustable and has no time limit on power retention. This kind of load can be adjusted continuously many times in a certain time range and track wind power fluctuation. Thus, it is suitable for intra-day dispatching mode. Taking one ferroalloy enterprise as an example, its ore heating furnace can be adjusted within the rated capacity range of 90%~110%, with no strict restriction on adjusting time, and have frequent adjustment and high flexibility.

The formula of the continuously adjustable load is as follows:

$$P_{SH}(t) = \sum_{j=1}^{N_{SH}} x_{SH,j} P_{SH,j}(t)$$
(6)

where $P_{SH}(t)$ denotes the total load of continuously adjustable load at t. N_{SH} denotes the number of continuous high-energy load units. $x_{SH,j}$ denotes the state variable of the j_{th} continuously adjustable unit, the unit participates in the regulation when the value j is 1. $P_{SH,j}$ represents the load quantity of continuously adjustable load at t of the j_{th} unit.

3 Multi-Time Scale Model Architecture

3.1 Resource Classification of Demand Response

As discussed above, different kinds of high-energy loads show different response speeds, also for DR resources. There are two kinds of DR resources: price-based demand response (PDR) and incentive demand response (IDR) [65].

PDR refers to users' change of their electricity demand in reaction to the variation of retail electricity prices. This means a portion of transferable load shifted to the trough stage of electricity price through economic decisions to reduce electricity consumption during peak times. Generally, the user makes the electricity usage plan in accordance with the previous day's price. Therefore, PDR is generally determined in the day-ahead planning.

IDR refers to the DR that the implementation agency encourages users to reply quickly and cut load when system reliability is threatened or at electricity peaks make deterministic or time-varying policies. IDRs can be generally separated into the following two categories [66]:

Class A IDR: Response time is long; scheduling plan have to be made one day in advance and is determined in day-ahead scheduling [67];

Class B IDR: The short response time is determined in the day rolling schedule.

3.2 Multi-Time Scale Framework

Because of the increasing proportion of wind power integration, the traditional day-ahead scheduling method has difficulty solving the wind power consumption problem. Researches show that the multi-time scale scheduling scheme can alleviate the wind curtailment problem greatly [68].

To increase the system's capacity to absorb wind power and lessen operational costs, we design a multi-time scale day-ahead-in-day rolling scheduling model for DR of high load energy participating in wind power accommodation. The scheduling framework is shown in Fig. 2, and the multi-time scale scheduling flow chart is illustrated in Fig. 3.



Figure 2: Multi-time scale framework



Figure 3: Multi-time scale dispatching flow chart

- (1) Day-ahead scheduling plan: It has a time scale of 1 h and an execution cycle of 24 h. Because of the long start-stop time of thermal power units, the start-stop plan should be committed in the day-ahead dispatching. Moreover, PDR response quantity, class A IDR call volume, and discrete high-energy load call volume are supposed to be determined in the day-ahead scheduling. Then, the resource scheduling quantity settled in day-ahead scheduling is considered as the known quantities in intra-day scheduling.
- (2) Intra-day scheduling plan: In day scheduling plan rolls every 15 min [69] and each time for 4 h. The unit output of the first 15 min period is adjusted according to the updated ultra-short-term

forecast of wind power and load because the scheduling plan cannot be adjusted repeatedly. The output of the conventional thermal power unit is required to be determined, wind power generation output, IDR call volume of Class B, and continuous high-energy load call volume in the intra-day scheduling.

4 Multi-time Scale Scheduling Model

4.1 Day-Ahead Scheduling Model

4.1.1 Objective Function

The objective function of day-ahead scheduling is to minimize the total operating cost of the system, including thermal power unit operating cost $C_{Th,t}$, thermal power unit start-stop cost $C_{qt,t}$, two types of IDR resource call compensation cost $C_{IDR,t}$, two types of high-energy load unit switching cost $C_{HE,t}$, and wind curtailment cost $C_{qv,t}$. The relevant formulas are as follows:

$$f = \min \sum_{t=1}^{24} (C_{Th,t} + C_{qt,t} + C_{IDR,t} + C_{HE,t} + C_{qw,t})$$

$$= \sum_{t=1}^{N_T} \sum_{i=1}^{N_G} [i_{th}(P_{Gi,t})^2 + b_i P_{Gi,t} + c_i] + \sum_{t=1}^{N_T} \sum_{i=1}^{N_G} s_i (1 - u_{i,t-1}) u_{i,t} + \sum_{t=1}^{N_T} (k_{IDRA} |\Delta IDRA_t| + k_{IDRB} |\Delta IDRB_t|)$$

$$+ \sum_{t=1}^{N_T} \sum_{i=1}^{N_{DH}} c_{DH,i} \lambda_{DH,i} \Delta P_{DH,i} + \sum_{t=1}^{N_T} \sum_{j=1}^{N_{SH}} c_{SH,j} \lambda_{SH,j} \Delta PDR_{t,k} + \sum_{t=1}^{N_T} k_{PDR} P_{qw,t}$$
(7)

where N_T represents the total number of scheduling periods, the segmented amount of time-of-use electricity price curve, N_G represents the total number of conventional units. λ_i , k_{PDR} is the time-of-use electricity price of PDR at t; $PDR_{i,k}$ represents the response quantity of PDR; a_i , b_i and c_i denote the generation cost coefficients of the i_{th} thermal power unit, respectively; s_i denotes the start-stop cost coefficient of the i_{th} thermal power unit; $u_{i,t}$ is the running state coefficient of the i_{th} thermal power unit at t, and the value of 1 denotes the running state; $P_{Gi,t}$ is the dispatching output of the i_{th} thermal power unit; k_{IDRA} and k_{IDRB} represent the unit invoking cost of class A IDR resource and Class B IDR resource, respectively. $\Delta IDRA_t$ and $\Delta IDRB_t$ are the call volumes of class A IDR load and Class B IDR load at t time; $c_{DH,i}$ and $c_{SH,j}$ are the switching stages of discrete-continuous high-energy load units, respectively; $\lambda_{DH,i}$ and $\lambda_{SH,j}$ are the switching stages of discrete high-energy load and continuous high-energy load units, respectively, and the value of 1 denotes that the unit is put into operation, the value of 0 means that the unit is interrupted operation. $\Delta P_{DH,i}$ and $\Delta P_{SH,j}$ are the switching capacity of discrete highenergy load and continuous high-energy load, respectively; k_w represents the wind curtailment penalty cost coefficient; $P_{qw,t}$ denotes the wind curtailment power at t.

4.1.2 Constraints

(1) Active power balance constraints:

$$\sum_{i=1}^{N_G} P_{G_{i,t}}(t) + P_w(t) = P_L(t) + P_{DH}(t) + P_{SH}(t) + \Delta PDR_t + \Delta IDRA_t + \Delta IDRB_t$$
(8)

where $P_w(t)$ represents the wind power output at time t; $P_L(t)$ represents the predicted value of load power; $P_{DH}(t)$ represents the operating power of discrete high-energy load after coordinated control

optimization. $P_{SH}(t)$ represents the operating power of continuous high-energy load after coordinated control optimization. ΔPDR_t is the call volume of PDR.

- (2) The output constraint, climbing constraint and start-stop constraint of thermal power units are respectively referred to formulas (15)–(17) in reference [70].
- (3) Wind turbine output constraints

$$0 \le P_w(t) \le P_w^{per}(t) \tag{9}$$

(4) PDR constraints

For the electricity price DR, we select the widely used elastic matrix to calculate the electricity load after participating in the DR. Electricity price elasticity matrix E is obtained by the following formula:

$$\left[\frac{\Delta q_1}{q_1}\frac{\Delta q_2}{q_2}\dots\frac{\Delta q_m}{q_m}\right]^T = E\left[\frac{\Delta p_1}{p_1}\frac{\Delta p_2}{p_2}\dots\frac{\Delta p_m}{p_m}\right]^T$$
(10)

The left side of the Equation denotes the load changing rate; the matrix on the right side denotes the electricity price changing rate; E is the elastic matrix, whose main diagonal is the self-elasticity coefficient; the secondary diagonal is the mutual elasticity coefficient.

Upper and lower limit constraints on PDR resource volume are as follows:

$$\Delta PDR_t \le \lambda_{pdr} P_{load,t} \tag{11}$$

where λ_{pdr} is the load changing rate of after PDR.

(5) Upper and lower constraints on IDR resource call volume:

$$\begin{cases} 0 \le \Delta IDRA_t^+ \le \Delta IDRA_t^{+,max} \\ 0 \le \Delta IDRA_t^- \le \Delta IDRA_t^{-,max} \end{cases}$$
(12)

$$\begin{cases} 0 \le \Delta IDRB_t^+ \le \Delta IDRB_t^{+,max} \\ 0 \le \Delta IDRB_t^- \le \Delta IDRB_t^{-,max} \end{cases}$$
(13)

(6) The scheduling constraints of discretely adjustable high-energy load [71]:

1. Total load conservation constraints:

Т

$$P_{DH,i}^{0} = \sum_{t=1}^{n} P_{DH,i}^{\prime}(t)$$
(14)

The initial total load of discretely adjustable load i before scheduling; represents the quantity of discretely adjustable load *i* after scheduling.

2. Adjustment range constraints:

$$\Delta P_{SH,j}^{\min} \le P_{SH}(t) - P_{SH}(t-1) \le \Delta P_{SH,j}^{\max}$$
(15)

where $\Delta P_{SH,j}^{min}$ and $\Delta P_{SH,j}^{max}$ denote the upper and lower adjust limits of discrete high-energy load, separately.

$$-R_{SH,j}^{down} \le P_{SH}(t) - P_{SH}(t-1) \le R_{SH,j}^{up}$$
(16)

where, $R_{SH,j}^{up}$ and $R_{SH,j}^{down}$ are respectively the up and down ramp rates of discrete high-energy load.

4. Response time interval constraints

$$\lambda_{DH,i}(t) \cdot (\lambda_{DH,i}(t) - \lambda_{DH,i}(t-1)) \cdot (\Delta T \sum_{\tau=t-T_{g,i}}^{t-1} \lambda_{DH,i}(\tau) - T_{DH,i}^g) \ge 0$$
(17)

where $T_{DH,i}^{g}$ represents the minimum response time interval of discrete high-energy load. This formula represents that if load i want to change its operating state, it must maintain the same operating state in $T_{DH,i}^{g}$ time before changing.

5. Response time constraints

$$0 \leq \sum_{\tau=1}^{r} \left| \lambda_{DH,i}(\tau) - \lambda_{DH,i}(\tau-1) \right| \leq M_{DH,i}$$
(18)

where $M_{DH,i}$ represents the maximum allowable response times of discrete high-energy load i within the scheduling cycle.

(7) Continuously adjustable high-energy load scheduling constraints

1. Total load conservation constraints:

$$P_{SH,j}^{0} = \sum_{t=1}^{T} P_{SH,j}'(t)$$
(19)

where $P_{SH,j}^0$ represents the initial total load of continuously adjustable load j before dispatching; $P_{SH,j}(t)$ denotes the load of continuously adjustable load j after dispatching.

2. Adjustment range constraints

$$\Delta P_{SH,j}^{min} \le P_{SH}(t) - P_{SH}(t-1) \le \Delta P_{SH,j}^{max}$$
⁽²⁰⁾

where $\Delta P_{SH,j}^{min}$ and $\Delta P_{SH,j}^{max}$ are the lower and the upper adjust constraint of continuously adjustable highenergy load j, respectively.

3. Response speed constraints

$$-R_{SH,i}^{down} \le P_{SH}(t) - P_{SH}(t-1) \le R_{SH,j}^{up}$$
(21)

 $R_{SH,i}^{up}$ and $R_{SH,i}^{down}$ are the up and down ramp rates of continued high-energy load.

(8) Tie-line transmission power constraints

$$-P_{tie,t}^{max} \le P_{tie,t} \le P_{tie,t}^{max}$$
(22)

where $P_{tie,t}$ is the transmission power of the grid tie-line; $P_{tie,t}^{max}$ denotes the transmission power limit of the grid tie-line. Since the transmission power of the grid tie-line is bidirectional, its power limit constraint has positive and negative signs.

4.2 Intra-Day Scheduling Model

4.2.1 Objective Function

The objective function of intra-day scheduling is still the minimum system operation cost, including thermal power unit output cost $C_{Th,t}$, B class IDR call cost $C_{IDR,t}$, continuous high-energy load switching cost $C_{Sh,t}$, and wind curtailment cost $C_{qw,t}$. Since the start-stop plan of thermal power units, class A IDR call volume and discrete high-energy load call volume have been decided in day-ahead scheduling. Therefore, the start-stop cost of thermal power units, class A IDR calling cost and discrete high-energy load switching cost are constant in day-ahead scheduling and have not been written into the formula.

4.2.2 Constraints

(1) Active power balance constraints:

$$f = \min \sum_{t=1}^{96} (C_{Th,t} + C_{IDR,t} + C_{SH,t} + C_{qw,t}) = \sum_{t=1}^{N_T} \sum_{i=1}^{N_G} [a_i (P_{Gi,t})^2 + b_i P_{i,t} + c_i] + \sum_{t=1}^{N_T} k_{IDRB} |\Delta IDRB_t| + \sum_{t=1}^{N_T} \sum_{i=1}^{N_{SH}} c_{SH,i} \lambda_{SH,i} P_{SH,i} + \sum_{t=1}^{N_T} k_w P_{w,t}$$
(23)

where $P_{DH}(t)$, ΔPDR_t and $\Delta IDRA_t$ are constant.

(2) The thermal power unit constraints, fan constraints, B type IDR constraints, continuous high load call constraints and tie line transmission power constraints are the same as 4.1.2.

4.3 Optimization Algorithm

Commonly, the optimal operation of a power system can be formulated as a multi-objective or a single-objective function with multi-constraint optimization. The PSO algorithm is suitable for solving multi-objective optimization issues. It is often utilized in the solution of discontinuous and nonlinear problems. However, the basic PSO algorithm tends to result in local minimum. Thus, some improvement has been made to solve the disadvantage. To avoid the disadvantages of the PSO algorithm, the improved PSO method incorporates an inertia weight coefficient into the algorithm modeling, which allows for operational regulation and adjustment of the particles' flight speed. The PSO has been frequently used to improve the power system optimization procedure in comparison to other algorithms; the PSO achieves a higher level of computation accuracy with fewer repetitions. The flow diagram of the improved PSO is shown in Fig. 4 depicts the stage of optimizing the ultimate outcomes of operation costs.

The speed and position update formula in standard particle swarm optimization algorithm is:

$$v_{id}^{t+1} = \omega v_{id}^{t} + c_1 r_1 (p_{id}^{t} - x_{id}^{t}) + c_2 r_2 (p_{gd}^{t} - x_{id}^{t})$$
(24)

$$x_{id}^{t+1} = x_{id}^{t} + v_{id}^{t+1}$$
(25)

where ω means inertia weight,

$$\omega = \omega_{\text{start}} - \frac{\omega_{\text{start}} - \omega_{\text{end}}}{t_{\text{max}}} \times t$$
(26)

where ω_{start} is the initial inertia weight, ω_{end} is the termination inertia weight, t_{max} is the maximum number of iterations, and t is the current number of iterations.



Figure 4: Flow diagram of the proposed improved PSO

The influence of the particle's previous velocity on the current velocity is determined by the inertia weight. By adjusting the inertia weight, the global search ability and local search ability can be coordinated. Eq. (26) is a typical inertia weight decreasing strategy. Under this strategy, the global search ability is strong at the initial stage of iteration. If the best is not obtained at the initial stage, the local search ability will be strengthened with the decreasing, and the search results are easy to fall into the local optimum. Once trapped in the local optimum, it is difficult to jump out. In order to overcome this deficiency, a nonlinear dynamic inertia weight method is proposed in Eq. (27):

$$\omega(t) = \omega_{\text{end}} + (\omega_{\text{start}} - \omega_{\text{end}}) \exp\left(-k \times \left(\frac{t}{t_{\text{max}}}\right)^2\right)$$
(27)

5 Case Study

5.1 Model Overview

In this study, the improved IEEE-30 node system shown in Fig. 5 is used to simulate the above design strategy. It contains six thermal power units located at nodes 1, 2, 5, 8, 11, and 13, respectively, and a wind power unit with a capacity of 350 MW at node 8. There are one discrete high-energy load unit and two continuous high-energy load units at nodes 4, 7, and 10, respectively. Table 1 displays the operating parameters of each thermal power unit, and Table 2 shows the remaining parameters. Fig. 6 illustrates the time-of-use electricity prices diagram, Figs. 7a–7c demonstrate the total load prediction curve, and Figs. 8a, 8b illustrate the forecasting power output of wind power under positive and reverse peak regulation of wind power.



Figure 5: IEEE-30 system

Unit	The upper limit of output/MW	The lower limit of output/MW	Climbing rate/(MW·h ⁻¹)	Fuel cost factor		
				$a/(\$\cdot MW^{-2})$	$b/(\$\cdot \mathbf{MW}^{-1})$	<i>c</i> /\$
1	200	50	120	0.0059	3.15	58.66
2	80	20	48	0.0276	2.76	55.48
5	50	15	30	0.0984	1.57	49.84
8	35	10	21	0.0131	5.12	51.84
11	30	10	18	0.0393	4.72	43.53
13	40	12	24	0.0393	4.72	50.90

Table 1: Operating parameters of thermal power units

 Table 2: Other parameters of thermal power units

Parameter	Numerical value
Self-elastic coefficient of the elastic matrix	-0.2
Mutual elasticity coefficient of the elastic matrix	0.03
The upper limit of load change rate participating in PDR/%	7
The upper limit of load change rate participating in IDRA/%	5
The upper limit of load change rate participating in IDRB/%	3

(Continued)

Table 2 (continued)				
Parameter	Numerical value			
IDRA compensation cost factor/(\$/MW)	7.78			
IDRB compensation cost factor/(\$/MW)	9.45			
Abandonment cost coefficient/(\$/MW)	36.22			



Figure 6: Time-of-use price



Figure 7: (Continued)



Figure 7: (a) The day-ahead and daily load forecasting, (b) The day-ahead and daily wind power forecasting under reverse peak shaving, (c) The day-ahead and daily wind power forecasting under positive peak shaving



Figure 8: (a) Dispatching results under reverse peak regulation of wind power, (b) Dispatching results under positive peak regulation of wind power

5.2 Analysis of Scheduling Results

In both positive and reverse peak regulation scenarios, the results of the proposed scheduling strategy are compared and analyzed in Figs. 8a and 8b.

As demonstrated in Figs. 7 and 9a, 9b, in the reverse-peaking scenario, the high incidence periods of wind power are from 1:00 am to 10:00 am, 11:00 pm–12:00 pm, while the load demand is low at this time. Increasing the load demand at 1:00 am–10:00 am and 11:00 pm–12:00 pm is necessary by calling PDR and IDR to reduce wind curtailment. In the positive peak shaving scenario, the high-frequency period of wind power is between 10 and 19, which overlaps with the load utilization's peak period, and a large amount of wind power can be consumed without large-scale DR resource call. Compared with the peak inversion scenario, the DR resource transfer is reduced by 18.07%.



Figure 9: (a) Transferable energy with DR in the case of reverse peak shaving of wind power, (b) Transferable energy with DR in the case of positive peak shaving of wind power

In addition, although the total amount of transferable load of type B IDR is small, compared with PDR and type A IDR, type B IDR is more flexible and has a faster response speed. Therefore, the change of type B IDR in intra-day scheduling is relatively severe, which is suitable for some sudden situations or the suppression of wind power fluctuations in short time scales.

Figs. 10 and 11 show the calls of discrete high-load and continuous high-load under two wind power scenarios. For the discrete high-load energy load, when the wind power is in the reverse peak trend, the high incidence of wind power is mostly in the morning, so the discrete high-load energy enterprises will transfer part of the 13–24 h load to 1–12 h. When wind power shows a positive peaking trend, high-capacity enterprises will move a portion of the load during the low wind power period to the high wind power period (13:00–24:00). However, such load cannot be continuously regulated in a short time. The call trend for continuous high energy load is roughly the same as that of discrete high energy load in two wind power output scenarios. Moreover, due to its faster response speed, the continuous high load can alleviate the negative impact of large-scale wind power fluctuation in a brief duration in addition to peak load shifting.



Figure 10: Response comparison of discrete high energy load under reverse and positive peak shaving regulation of wind power



Figure 11: Response comparison of continuous high energy load under reverse and positive peak shaving of wind power

In summary, the proposed scheduling policy can fully utilize the time scale characteristics of high load and other DR resources to formulate a reasonable scheduling plan. It helps relieve the issue of wind curtailment and improves the system's economy.

5.3 Comparative Analysis with Different Scheduling Modes

To fully prove that the above scheduling method can efficiently lessen the wind curtailment rate and system's operation cost, we set up the following three different schemes for comparative analysis under two scenarios in which wind power output presents positive and reverse peak regulation, respectively.

Scheduling scheme 1: day-ahead dispatching strategy without participation in system regulation high-energy load.

Scheduling scheme 2: day-ahead dispatching strategy with high-energy load participation in system regulation.

Scheduling scheme 3: adopt the scheduling scheme in this paper.

The scheduling results of scheme 1 are illustrated in Fig. 12. The scheduling results of scheme 2 are illustrated in Figs. 13 and 14. The results of the three schemes are presented in Table 3.



Figure 12: (Continued)



Figure 12: Scheduling results of scheme 1, (a) Scheduling results of wind power with reverse peak regulation, (b) Dispatching results of positive peak of wind power, (c) Demand response resource call in reverse peak regulation of wind power, (d) Demand response resource call when wind power positive peak



Figure 13: (a) Scheduling results of wind power with reverse peak regulation, (b) Dispatching results of the positive peak of wind power

Based on Table 3, a small amount of DR resource calls cannot implement large-scale wind power consumption in scheduling scheme 1, especially under the reverse peak regulation scene in wind power peak time (1-10 h). This leads to serious wind curtailment; the wind curtailment rate reaches up to 12.47%. Therefore, the system reaches the maximum operating cost under this scheme, which is 49,538 dollars.



Figure 14: (a) Demand response resource call in reverse peak regulation of wind power, (b) Demand response resource call when wind power positive peak, (c) Response of discrete high load energy load, (d) Response of continuous high energy load

Scene	Scheduling scheme	/\$	Abandonment rate/%
Reverse peak shaving	Option 1	49538	12.47
	Option 2	44108	10.28
	Option 3	16815	8.92
Positive peak shaving	Option 1	26223	3.28
	Option 2	4990	2.91
	Option 3	2345	1.68

 Table 3: Comparison table of different scheduling schemes

Based on scheme 1, scheme 2 allows high-energy loads to engage in DR scheduling. Participation of high-energy loads can reduce the system wind curtailment according to the characteristics of high-energy load with large adjustable capacity and convenient control. Compared with plan 1, the wind curtailment rate was reduced by 0.37% and 2.19%, according with the positive and reverse peak regulation scenarios, respectively. As a significant proportion of wind power is consumed, the system

wind curtailment cost and thermal power unit output cost are reduced. Compared with Plan 1, the system's operation cost is reduced by 21,233 dollars and 5430 dollars under positive and reverse peak regulation, respectively.

Based on Plan 2, Plan 3 makes full use of the multi-time-scale characteristics of the highenergy load and other DR resources, which can make timely adjustments according to wind power fluctuations in a shorter time scale, and further decrease the wind curtailment rate of the system. The curtailment rate in scheme 3 is reduced by 3.55% and 1.36% under reverse peak regulation and reduced by 1.60% and 1.23% under positive peak regulation, respectively compared with that in schemes 1 and 2. At this time, both the wind curtailment rate and the system operation cost of Scheme 3 is the lowest, with the wind curtailment rate of 1.68% and the system operation cost of 2345 dollars.

To sum up, through the comparative analysis of three different schemes under two scenarios of forward and reverse peak shifting, the efficiency of the scheduling strategy designed in this work is verified for reducing the wind curtailment rate of the system.

6 Conclusion

To address the issues of large-scale wind power consumption and insufficient regulation capacity of traditional units, this paper constructs a bio-inspired computer model by fully exploring the multitime scale features of DR resources and constructs day-ahead and intra-day rolling scheduling models that include high-energy load in system regulation. The method can obtain the system's optimal scheduling plan. The main conclusions are as follows:

- (1) With the participation of high-energy load, the system's wind power accommodation rate is remarkably increased, and the peak pressure at the source side is effectively decreased. Under the two scenarios of forwarding peak regulation and reverse peak regulation, the system wind power curtailment ratio is decreased by 15.8% in comparison with the traditional scheduling mode.
- (2) The multi-time-scale scheduling model is adopted to make peak-load shifting at the slow response load side resources so that the wind power fluctuations in a short time scale can be suppressed, and the wind power accommodation ability is increased. In addition, the system's operation cost is also lessened due to the decrease of wind power curtailment ratio and the increase of prediction accuracy.

Funding Statement: We would like to express our gratitude to the editors and anonymous reviewers for their comments and suggestions. This research study is supported by the Program for Innovative Research Team (in Science and Technology) in University of Henan Province (No. 22IRTSTHN016) and the Hubei Natural Science Foundation (No. 2021CFB156) and the Japan Society for the Promotion of Science (JSPS) Grants-in-Aid for Scientific Research (KAKENHI) (No. JP21K17737).

Conflicts of Interest: The authors declare that they have no conflicts of interest to report regarding the present study.

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