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Evaluation of On-Line MPPT Algorithms for PV-Based Battery Storage Systems

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Abstract: This paper presents a novel Simulink models with an evaluation study of more widely used On-Line Maximum Power Point tracking (MPPT) techniques for Photo-Voltaic based Battery Storage Systems (PV-BSS). To have a full comparative study in terms of the dynamic response, battery state of charge (SOC), and oscillations around the Maximum Power Point (MPP) of the PV-BSS to variations in climate conditions, these techniques are simulated in Matlab/Simulink. The introduced methodologies are classified into two types; the first type is conventional hill-climbing techniques which are based on instantaneous PV data measurements such as Perturb & Observe and Incremental Conductance techniques. The second type is a novel proposed methodology is based on using solar irradiance and cell temperature measurements with pre- build Adaptive Neuro-Fuzzy Inference System (ANFIS) model to predict DC–DC converter optimum duty cycle to track MPP. Then evaluation study is introduced for conventional and proposed On-Line MPPT techniques. This comparative study can be useful in specifying the appropriateness of the MPPT techniques for PV-BSS. Also the introduced model can be used as a valued reference model for future research related to Soft Computing (SC) MPPT techniques. A significant improvement of SOC is achieved by the proposed model and methodology with high accuracy and lower oscillations.

Keywords: Photo-voltaic based battery storage systems; adaptive neuro-fuzzy inference system; maximum power point tracking; perturb & observe technique; incremental conductance technique; state of charge



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Nomenclature

V_{g}	Voltage of PV generator, in Volt.
I_{g}	Current of PV generator, in Ampere.
\tilde{P}_{g}	Output power of PV generator output power, in Watt.
I_{ph}	Cell insolation photo current, in Ampere.
I_{phg}	PV generator insolation photo current, in Ampere.
I_o	Cell reverse saturation current, in Ampere.
I_{og}	Reverse saturation current of PV generator, in Ampere.
R_s	Series resistance per cell, in Ohm.
R_{sh}	Shunt resistance per cell, in Ohm.
R_{sg}	Series resistance of PV generator, in Ohm.
N_s	Numbers of series- connected solar cells
N_P	Number of parallel-connected solar cells
q	Electron charge, 1.602×10^{-19} C
K	Boltzmann constant, 1.38×10^{-23} J/k
Т	Cell working temperature in, °C
A	Completion factor.
Λ	PV cell constant in, (1/V)
Λ_g	PV generator constant in, (1/V)
G	Solar insolation (radiation) level in W/m ² .
P_{max}	Maximum output power of PV module, in Watt
I_{mp}	Maximum current of PV module, in Ampere.
V_{mp}	Maximum voltage of PV module, in Volt.
I_{sc}	Short circuit current of PV module, in Ampere
V_{oc}	Open circuit voltage of PV module, in Volt
k_i	Temperature coefficient of I_{sc}
k_v	Temperature coefficient of V_{oc}
OCV	Battery open circuit voltage, in Volt
R_1	Battery parallel RC resistance, in Ohm
C_1	Battery parallel RC capacitor, in Farad
R_0	Battery internal resistance, in Ohm
V _c	Battery parallel RC voltage, in Volt
v_b	Battery voltage, in Volt
i_b	Battery current, in Ampere
D_{opt}	Optimum duty cycle of DC-DC Converter
a	Current ratio of DC-DC Converter
T_s	Sampling period in Sec

1 Introduction

By the end of 2020, the renewable generation power capacity of worldwide has been increased by 261 GW, which is 10.3% higher than 2019's. 64% Share of new renewable capacity installed in Asia. Solar energy continued to drive capacity expansion with an increase of 127 GW, which represents 22% as shown in Fig. 1 [1]. Solar PV alone accounts for more than 50% of all renewable power expansion [1]. Despite the expansion in PV systems, there are technical constraints due to continuous and sudden changes in climate conditions, so auxiliary systems are required to achieve good energy management. Energy storage technologies are the main key elements that can deal with these constraints [2,3]. There

are many Forms of Energy Storage Systems (ESSs) including mechanical, electrochemical, chemical, and thermal energy storage.



Figure 1: Renewable power capacity growth 2016–2020

A Battery storage system is the most activity in 2020 as shown in Fig. 2 due to easy deployment and reduction in cost [2].



Figure 2: Share of global energy storage installed capacity, by technology, 2019 and 2020

Besides, batteries ESS can be designed and produced for any rating, based on voltage and current availability [3], so it represents the second largest ESS technology by the capacity of 14.2 GW (7.5% of total operating storage capacity) [4].

There are 3 main types of conventional Batteries ESS include Lithium-Ion (Li-ion) batteries (92%), Sodium-sulphur (NaS) batteries (3.6%), and Lead-Acid (PpA) batteries (3.4%) [5].

Although Lead-Acid (PpA) batteries are simple to manufacture, easy to recycle, and capable of high discharge currents, besides have high efficiency (70%–80%), long calendar life (5–15 years), high specific power, and low cost per watt-hour, but they are limited using due to poor weight-to-energy ratio, slow charging (14–16 h) and its environmental risk (Pb is a poisonous metal) [6,7]

Also, Sodium-sulphur (NaS) batteries are of limited use because they must be operated at high temperatures (between 300°C and 350°C) which makes their operation dangerous and high costs [8,9].

Where Lithium-Ion (Li-ion) batteries, are the most extensively used technology in electrochemical ESS [10], due to their high energy density, high efficiency, fast charge/discharge, and attractive self-discharge rate (5% per month) [11].

After using Battery ESS, PV systems still suffer from nonlinear behavior or maximum power point variation with the climatic conditions, besides low conversion efficiency which is less than 17%. So, it becomes necessary to use the MPPT system to ensure more efficient energy management operation of PV-based Battery Storage Systems [12,13]. The main target of the MPPT is to reach the PV operating voltage close to the MPP under different climatic conditions. It has become the main component in PV power systems. There are many MPPT techniques that can be classified into three main types;

- Offline methods or Model-based methods, which are based on the parameters of the PV panel to generate the control signals, such as Computational methods (OCV method and SCC method) [14,15], and Soft Computing based methods (ANFIS based method and FLC based method) [16–19]. The first method is not suitable for fast changes in climate conditions and the second mainly depends on trial and error with prior training which can be time-consuming [20].
- 2) On-line methods or Model-free methods or hill climbing techniques (Perturb and Observe (P&O) and Incremental Conductance (IncCond)) which are based on instantaneous measurements of PV data. Despite climate conditions changes being rapidly detected, oscillations around the MPP are found [12,13].
- 3) The Hybrid methods which are based on two algorithms, first an offline method to get the initial operating point close to the MPP of PV, and the second online method to track the MPP faster but with more complexity and cost [20].

Due to cost, ease of implementation, faster dynamic response, model-free method and efficiency, online methods are more suitable for ESS although they suffer from oscillations around the MPP, which it's not an essential point to ESS.

This paper presents an evaluation study of conventional and novel SC online MPPT techniques for PV-BSS which can predict and track the MPP under rapidly changing environmental conditions in a short time with minimum error and low oscillations. Besides, a valued reference model is also introduced to be able to properly simulate the PV-BSS and study the different effects conditions on the battery SOC.

2 Mathematical Model of PV-BSS

The proposed PV-BSS introduced in this work mainly consists of a PV module, a DC-DC converter, and a Li-ion battery as shown in Fig. 3. Steady-state mathematical models for proposed PV-BSS and each component are introduced;

2.1 PV Module Model

The PV array has nonlinear voltage current characteristic that depends on solar radiation, cell temperature and cells connected pattern as shown below [21,22];



Figure 3: The Schematic diagram of the proposed system

$$I_{g} = GI_{phg} - I_{og} \left(e^{\Lambda_{g}(V_{g} + I_{g}R_{sg})} - 1 \right) - \left((V_{g} + I_{g}R_{sg}) / R_{shg} \right)$$
(1)

The electrical specification (at STC) of Siemens's SM55 PV solar module given by manufacturer and mentioned in Appendix can be used to find the five unknown parameters; reverse saturation current per cell I_o , radiation photo current per cell I_{ph} , completion factor A, Series resistance per cell R_s and shunt resistance per cell R_{sh} as follows [23]:

According to the short circuit conditions;

$$I_{sc} = I_{ph} - I_o \left(e^{\Lambda I_{sc} R_s} - 1 \right) - I_{sc} R_s / R_{sh}$$
⁽²⁾

According to the open circuit conditions;

$$I_{ph} = I_o \left(e^{\Lambda_g V_{oc}} - 1 \right) - V_{oc} / N_s R_{sh}$$
(3)

According to the Maximum power conditions;

$$I_{mp} = I_{ph} - I_o \left(e^{\Lambda_g (V_{mp} + I_{mp} N_s R_s)} - 1 \right) - (V_{mp} + I_{mp} N_s R_s) / N_s R_{sh}$$
(4)

According to the derivative of PV module current at MPP;

$$\frac{I_{mp}}{V_{mp}} = \frac{I_o \Lambda_g e^{\Lambda_g (V_{mp} + I_{mp} N_s R_s)} + 1/N_s R_{sh}}{1 + I_o \Lambda R_s e^{\Lambda_g (V_{mp} + I_{mp} N_s R_s)} + R_s/R_{sh}}$$
(5)

According to the derivative of PV module current at SC;

$$\frac{1}{R_{sh}} = \frac{I_o \Lambda_g e^{\Lambda I_{sc} R_s} + 1/N_s R_{sh}}{1 + I_o \Lambda R_s e^{\Lambda I_{sc} R_s} + R_s/R_{sh}}$$
(6)

By solving Eqs. (2) to (6) using a non-linear equation solver as shown in [24], so the electrical parameters of the PV array are known, the simulation model is built in Matlab/Simulink as shown in Fig. 4, and performance curves at different solar radiation and working temperature can be easily shown in Fig.5, but after taking into consideration the parameters that affected by different solar radiation and working temperature as following [25,26];

$$I_{ph} = \left[I_{ph} \Big|_{stc} + k_i \left(T - T_{stc} \right) \right] \left(\frac{G}{G_{stc}} \right)$$

$$(7)$$

$$I_o = I_o|_{stc} \left(\frac{T}{T_{stc}}\right)^3 e^{\left(\frac{qEg}{AK}\left(\frac{1}{T_{stc}} - \frac{1}{T}\right)\right)}$$
(8)

$$R_{sh} = \frac{G_{stc}}{G} R_{sh}|_{stc}$$
⁽⁹⁾



Figure 4: The simulation model of SM55 PV module at different solar radiation and working temperature



Figure 5: Power-Voltage characteristics of SM55 PV module at different solar radiation and working temperature

The comparison between the simulation results with the specification data given by the manufacturer as shown in Tab. 1 proves that the validity of the proposed simulation model

	$P_{max}(W)$	$I_{mp}\left(A ight)$	$V_{\scriptscriptstyle mp}\left(V ight)$	$I_{sc}(A)$	$V_{oc}\left(V ight)$
Specification data	55	3.15	17.4	3.45	21.7
Simulation results	54.811	3.155	17.361	3.455	21.691
Error (%)	0.344	0.159	0.224	0.145	0.042

Table 1: Simulation results with specification data for SM55 module

2.2 DC-DC Converter Model

Due to high sensitivity to changes in duty cycle D, a Boost converter is used. Ideally, (with negligible losses), the output voltage (battery voltage) to input voltage (PV voltage) ratio a in terms of duty cycle is given as follow [16];

$$a = v_b / V_g = 1 / (1 - D) \tag{10}$$

So the duty cycle *D* can be calculated as follows;

$$D = 1/(1+a)$$
(11)

2.3 Lithium-Ion Battery Model

There are many equivalent circuit models for lithium-ion batteries. The one-time constant model (OTC) can illustrate the dynamic characteristics of the battery so it is suitable to determine the state of charge (SOC) of the battery.

The OTC model mainly consists of three items including the voltage source V_{oC} , internal resistance R_o , and parallel RC sub circuit (R_1 and C_1) as shown in Fig. 6. The description of model operation is shown in the discrete time model which can be expressed by the below equations [27,28]:

$$v_{c,k+1} = v_{c,k} \cdot e^{-\frac{T_s}{R_1 C_1}} + R_1 \cdot \left(1 - e^{-\frac{T_s}{R_1 C_1}}\right) i_{b,k}$$
(12)

$$v_{b,k} = V_{OC} (SOC_k) - v_{c,k} - R_o . i_{b,k}$$



Figure 6: Battery OTC model equivalent circuit

By using the above two equations besides the parameters of the Li-ion battery cell mentioned in the Appendix; the simulation model is built in Matlab/Simulink as shown in Fig. 7 and the battery voltage and the SOC are shown in Fig. 8.

(13)



Figure 7: The simulation model of Lithium-Ion battery



Figure 8: Battery voltage and SOC of battery OTC model

3 Simulation Model of PV-BSS

The proposed PV-BSS with MPPT techniques was simulated in MATLAB/SIMULINK software environment as shown in Fig. 9. Initially, the proposed PV-BSS operates at D = 0.16

The variation of PV voltage, Battery voltage, Battery power, and SOC of battery without MPPT technique will be illustrated below from Fig. 10.



Figure 9: The simulation model of PV-EES



Figure 10: Operation of PV-BSS without MPPT technique at different solar radiation and temperature

These figures show the effects of the irradiance (G) and temperature (T) variation in 4 cases mentioned in Fig. 4 every 600 s. As shown in Figs.10a and 10b, every 600 s there is a change in PV current and voltage due to irradiance and temperature change. The change in PV output is accompanied by a change in battery voltage and current with a reciprocal ratio. So, the power of PV & Battery is approximately the same as shown in Fig. 10c.

Where Fig. 10d illustrates the SOC of the battery, it is easily noticed that the rate of charging is changed every 600 s as irradiance and temperature change. Also, the BSS takes 2400 s to reach SOC equal 48.7%.

4 Simulation Model of On-line MPPT Techniques

In this part; three different online MPPT techniques are discussed. P&O and IncCond techniques are conventional hill-climbing techniques that are based on measurements of PV voltage and currents then the duty cycle is varied until the MPP is reached. The third technique is a novel methodology based on using solar irradiance and cell temperature measurements with pre-build ANFIS model to predict the optimum duty cycle to reach MPP.

P&O, IncCond and ANFIS-based techniques are used as an online MPPT controller to investigate the proposed study under different environmental conditions, so intensive works are conducted.

4.1 P&O Technique

The P&O technique is based on periodical measurement of PV current I(k) and voltage V(k) to determine the actual PV output power P(k), then flowing steps are repeated until MPP is reached:

- 1) Perturb; varying the power converter duty cycle D up and down.
- 2) Observe; determining the output power variation (ΔP) sign and the PV voltage variation (ΔV) sign.
- 3) If ΔP and ΔV have different signs, the perturb step should be kept in the same direction otherwise the direction will be reversed.
- 4) For more accuracy, lower oscillation, and fast reaching to the MPP, variable step size is used [13]

The previous steps can be summarized in the flow chart of the P&O technique, which is shown in Fig. 11a. For every previous change in PV current and voltage due to irradiance and temperature change the optimum Duty cycle obtained by the P&O technique is shown in Fig. 11b.

4.2 IncCond Technique

The IncCond technique is based on periodical measurement of PV current I(k) and voltage V(k) to determine the actual instantaneous conductance I(k)/V(k), then flowing steps are repeated until MPP is reached [13]:

- 1) Varying the power converter duty cycle D up and down.
- 2) Determining the PV current variation (ΔI) and the PV voltage variation (ΔV) and incremental conductance $\Delta I / \Delta V$.
- 3) If $\Delta V \neq 0$ and $(\Delta I / \Delta V) < (-I / V)$, D should be increased otherwise D will be decreased.
- 4) If $\Delta V = 0$ and $(\Delta I. > 0)$, D should be increased otherwise D will be decreased



Figure 11: P&O MPPT algorithm

The previous steps can be summarized in the IncCond technique flow chart, which is shown in Fig. 12a

For every previous change in PV current and voltage due to irradiance and temperature change the optimum Duty cycle obtained by the IncCond technique is shown in Fig. 12b



Figure 12: IncCond MPPT algorithm

4.3 ANFIS-Based Technique

The ANFIS-based algorithm uses a periodical measurement of the radiation level and cell temperature as inputs of a network; and the optimal Duty cycle D_{opt} as an input of the network.

The optimal Duty cycle D_{opt} can be estimated by solving Eqs. (4), (5), (10), (12) and (13). Due to the nonlinearity, the complexity of the PV-BSS and ANFIS-based algorithm is to be employed. This can be mathematically expressed as follows;

$$v_{c,k+1} = v_{c,k} \cdot e^{-\frac{T_s}{R_1 C_1}} + R_1 \cdot \left(1 - e^{-\frac{T_s}{R_1 C_1}}\right) I_{mp,k} / a$$
(14)

$$aV_{mp,k} = V_{OC}(SOC_k) - v_{c,k} - R_o I_{mp,k}/a$$
(15)

So the ANFIS model can be built by using actual data of G, T, and D_{opt} that based upon a first order Takagi–Sugeno model consisting of five layers. The membership functions are chosen to be trimf membership function for all the inputs where it gives good outputs compared to the other membership functions With RMSE = 0.00045212.

For every previous change in PV current and voltage due to irradiance and temperature change the optimum Duty cycle obtained by ANFIS-based technique is shown in Fig. 13.



Figure 13: Optimum duty cycle with time with ANFIS-based MPPT algorithm at different solar radiation and working temperature

5 Operation of PV-BSS Based on On-Line MPPT Techniques

The operation of PV-based battery storage system using IncCond, P&O, and ANFIS based techniques under different environmental conditions is done below. Illustrating the performance characteristics of PV-BSS and evaluating the validity and the accuracy of proposed models under variable climates conditions are achieved by simulation works.

5.1 On-Line MPPT Techniques Evaluation

For every previous change in irradiance and temperature change, the PV and Battery voltage and current obtained by IncCond, P&O, and ANFIS-based techniques are shown in Fig. 14.

Tabs. 2 and 3 show a comparison between different MPPT algorithms and their effect on PV & Battery Voltage and current. From obtained data, it is easily deduced that ANFIS-based techniques is the best MPPT technique according to the range, standard deviation, and relation between mean, median and mode for instantaneous PV and battery voltage.



Figure 14: Voltage and current of PV-BSS with different MPPT algorithms at different solar radiation & temperature

PV voltage				Battery voltage				
	IncCond MPPT	P&O MPPT	ANFIS MPPT	MPP LOCUS	IncCond MPPT	P&O MPPT	ANFIS MPPT	MPP LOCUS
Mean	16.73	16.74	17.5	16.733	23.69	23.72	23.74	23.99
Median	17	17.15	17.88		23.79	23.82	23.89	
Mode	20.65	15.23	16.1		15.09	21.54	22.41	
Std	0.9286	0.7744	0.7126		0.8103	0.7775	0.7741	
Range	21.69	5.423	4.467	1.868	10.61	8.262	3.862	1.9889

 Table 2: MPPT techniques evaluation for instantaneous PV & Battery voltage

Table 3: MPPT techniques evaluation for instantaneous PV & Battery current

PV current				Battery current				
	IncCond MPPT	P&O MPPT	ANFIS MPPT	MPP LOCUS	IncCond MPPT	P&O MPPT	ANFIS MPPT	MPP LOCUS
Mean	38.42	36.96	38.76	38.889	25	24.76	25.23	26.91
Median	38.27	42.38	37.88		25.11	22.58	24.96	_
Mode	41.37	21.84	23.04		0	13.1	13.25	
Std	10.3	9.486	8.885		7.681	7.486	7.149	
Range	52.26	25.25	23.78	5.1	47.62	25.83	24.58	16.512

For Voltage waveform; ANFIS-based technique has a lower range and standard deviation which means lower oscillation as noticed in Tab. 2. Besides the mean, median and mode are approximately equal which means a more symmetrical voltage waveform. Also, lower overshot for ANFIS-based technique as noticed in Fig. 14a.

Also for the current waveform; ANFIS-based technique has a slight lower range and standard deviation which means lower oscillation as noticed in Tab. 3. But it is noticed that current has more oscillation than voltage waveform. Also the mean, median, and mode are not equal which means not symmetrical waveform. But still, ANFIS-based technique is slight best waveform as noticed in Fig. 14b

5.2 Results and Discussion

Fig. 15a and Tab. 4 show a comparison between different MPPT algorithms and their effect on Battery power. It is easily noticed that ANFIS-based technique is the best MPPT technique.



Figure 15: Power & SOC of BSS with different MPPT algorithms at different solar radiation & temperature

	IncCond MPPT	P&O MPPT	ANFIS MPPT	MPP LOCUS
Mean	697	591.2	608	649.66
Median	599.9	562.1	600.4	_
Mode	0	121	298.7	_
Std	196.9	182.5	192	
Range	1196	830	618.3	431.623

 Table 4: MPPT techniques evaluation for instantaneous Battery Power

where, Fig. 15b illustrates the SOC of the battery obtained by different MPPT techniques. It is easily noticed that a significant improvement of SOC as the BSS takes 2400 s to reach SOC equal 70.94%, 71.03%, and 71.73% for IncCond, P&O, and ANFIS based MPPT techniques respectively.

6 Conclusions

A novel approach for online MPPT for PV-BSS operation based on ANFIS Technique is discussed, implemented and assessed. Besides conventional hill-climbing techniques P& O, and IncCond techniques are also introduced and evaluated.

The main results present in this article can be summarized as shown below;

- 1) A valued reference model of PV-BSS is introduced with full analyses
- 2) Evaluation study of On-Line MPPT Algorithms of PV-BSS is introduced with full analyses
- 3) P&O, IncCond and ANFIS based techniques are presented
- 4) Significant increase of SOC for proposed methodology to 147.3% from (84.7% without MPPT to 71.73% with MPPT).
- 5) Get a novel SC method to predict the optimal duty cycle to track the MPP with variable climate conditions.
- 6) Approximately equal duty cycle prediction from SC MPPT model and analytical model with MSSE of 0.000083 for the worst case.
- 7) Then modeling of PV-BSS operation with P&O, IncCond and ANFIS-based techniques is discussed.
- 8) Also evaluation of P&O, IncCond and ANFIS-based techniques is introduced and ANFIS based technique is proved as the best online MPPT technique with lower oscillation.

This model may be very useful for more works such as studying the partial shading effects, different types of batteries, and discussing the effect of SC MPPT techniques on SOC.

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A Appendix A

The study system parameters are [29];

1-PV module data at STC	$C (G = 1000 \text{ W/m}^2 \text{ and } \text{T})$	r = 25°C)				
P _{max}	55 W					
I _{mp}	3.15 A					
V _{mp}	17.4 V					
I _{sc}	3.45 A					
V _{oc}	21.7 V					
k _i	1.2 mA/°C					
k _v	−0.077 V/°C					
2-PV module parameters	[16]					
Io	5.5118×10^{-6}	A				
I _{ph}	3.45 A					
A	1.7571					
R _s	$2.9 imes 10^{-3} \ \Omega$					
R _{sh}	$1.4857 \times 10^{6} \Omega$	2				
3-Battery parameters [16]						
SOC	OCV	R1	C1	R 0		
0	3.5076	0.004538	9984.6	0.0081501		
0.1	3.5659	0.004267	10102	0.0068234		
0.2	3.6113	0.004343	10211	0.0068773		
0.3	3.6499	0.004283	10188	0.0067141		
0.4	3.6821 0.004167 10172 0.0064051					
0.5	3.7128 0.004053 10193 0.0060162					
0.6	3.7991 0.004094 10185 0.0062861					
0.7	3.8839	0.004199	10117	0.0064136		
0.8	3.9764	0.004167	10132	0.0063683		
0.9	4.0802	0.004109	10130	0.0065124		
1	4.2007	0.004658	10207	0.0083997		