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# Intelligent Fuzzy Based High Gain Non-Isolated Converter for DC Micro-Grids

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> Abstract: Renewable electricity options, such as fuel cells, solar photovoltaic, and batteries, are being integrated, which has made DC micro-grids famous. For DC micro-grid systems, a multi input interleaved non-isolated dc-dc converter is suggested by the use of coupled inductor techniques. Since it compensates for mismatches in photovoltaic devices and allows for separate and continuous power flow from these sources. The proposed converter has the benefits of high gain, a low ripple in the output voltage, minimal stress voltage across the power semiconductor devices, a low ripple in inductor current, high power density, and high efficiency. Soft-switching techniques are used to realize that the reverse recovery issue of the diodes is moderated, the leakage energy is reused, and no new scheme is appropriated. To reduce conduction losses, minimum voltage rating MOSFETs with a low ONresistance can be utilized. The converter can supply the required power from the load in the absence of one or two resources. Furthermore, due to the high gain of boosting voltage, the converter works in an Adaptive Neuro-Fuzzy Inference System (ANFIS). The operation principle, steady-state analysis of the proposed converter, is given and simulated utilizing MATLAB/Simulink simulation software.

> **Keywords:** Renewable energy sources; DC micro-grid; multi-input converter; soft-switching techniques; high gain

## Abbreviations

ANFISAdaptive Neuro-Fuzzy Inference SystemCICoupled Inductor



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| Direct Current                                    |
|---|
| Duty Cycles                                       |
| Electric Vehicle                                  |
| Fuel Cell   |
| Fuzzy Inference System                            |
| Field Programmable Gate Arrays                    |
| Inductor-Capacitor                                |
| Leakage Inductance                                |
| Magnetizing Inductor                              |
| Metal Oxide Semiconductor Field Effect Transistor |
| Maximum Power Point Tracking.                     |
| Photovoltaic                                      |
| Switched Capacitor                                |
| State of Charge                                   |
| Voltage Multiplier                                |
| Zero Voltage Switching                            |
|   |

## 1 Introduction

The penetration of distributed generation sources is causing DC micro-grid technology to evolve. To satisfy the demands of the dc load, DC power generators generate a minimum output voltage, necessitating the use of high efficiency, high gain dc-dc converters [1]. The rising population's daily demand for electric energy is a major source of concern for the power sector. Hybridizing energy has picked up fame in grid-connected micro-grid [2,3]. Hydropower stations with intra/interannual control provide lots of benefits over other kinds of hydroelectric power, including faster grid response, flexibility, and compatibility in energy generation. For long-term hydropower operations, systematic recommendations on the energy ecosystem are presented in [4]. Another choice is to use a quadratic boost converter for applications requiring high gain [5]. Other than renewable energy conversion, high gain dc-dc converters are now utilized in a number of applications, including high-intensity discharge lamp ballasts for vehicle headlamps, battery backup systems, electric traction, and some medical equipment [6]. Different water-body-top PV plants are being reported in the literature [7,8]. The problem of a canal-top PV system and the main grid distributing power to match load demands were discussed in [9].

Numerous high voltage gain dc-dc converters are introduced in [10,11] to address the disadvantages of simple boost converters for high voltage step-up applications. The source of renewable energy expansion will largely catalyze the use of maximum boost converters with a more efficient and reliable for converting endless energies into a power grid [12]. High voltage spikes can cause the severe diode to reverse recovery problems also [13,14]. High voltage gain with canceling the input current ripple is presented [15]. Multi-inputs converters have been classified into two methods, isolated multi-input converter and non-isolated multi-input converter.

To achieve the required maximum voltage gain, various isolated dc-dc converter topologies have been proposed in the literature [16,17]. However, transformer core saturation is a problem with this type of converter. Hence, a non-isolated dc-dc converter can thus be utilized to reach a high gain of voltage while easy circuit and minimum cost [18]. Non-isolated high gain converters provide the following, Voltage Multiplier (VM) cell [19], Switched Capacitor (SC) [20,21], the quadratic boost [22], cascade boost [23]. Thus, the resonant inductor is coupled to the SC converter to neglect the problem of diode recovery and to restrict the maximum current [24].

In [25], high gain of voltage with minimum duty cycles are accomplished at utilizing capacitor charging strategies, and voltage spikes are disposed of on the most switch, an inactive voltage clamp circuit is utilized. In [26], comprehensively review and classification of different dc-dc step-up converters according to their characteristics and methods of increasing voltage. Dual input, dual output, low power converter application is presented in [27]. Based on this concept, a dc-dc converter for the hybrid energy storage framework in EV [28]. A new double input Zero-Voltage Switching (ZVS) converter comprised of two boost units in [29] can be connected to low-power applications such as portable devices. In [30], a multiphase non-isolated resonant large-gain converter has been proposed for applications of high-current with extensive load ranges.

A new topology of the interleaved boost converter block diagram will be located in Fig. 1. The proper controller is attempted to control the voltage output given to load under different working conditions. In [31], a new boost multi-input dc-dc converter is associated with the grid. Based on duty ratio selection, several coupled inductor-based step-up converter topologies have a high gain of voltage while reducing switch voltage stress [32,33]. In order to achieve the desired voltage conversion ratio, the coupled inductor's turn ratio is often increased, resulting in minimizing the current ripple; an input filter is needed [34]. The CI converters may bring about excellent performance by adopting voltage clamp circuits [35,36]. The converter offered in [37,38] offers a large boost converter through the use of CI and a voltage lift technique. It combines a soft-switching technique and coupled inductor using a parallel LC resonant tank circuit [39]. Non-isolated Quazi Z-source converter along with the CI [40] minimizes the stress of voltage between the components and across the elements and enhances the gain of voltage without limiting the duty cycle. In this paper, a multi input interleaved coupled inductor based non- isolated converter is designed and in order to attain high gain of voltage without a high turn ratio. The main converter topology proposed in Section 2 describes design considerations in Section 3, Simulation results and discussion in Section 4, and Section 5 conclusions.



Figure 1: Block diagram of a new topology of the interleaved boost converter

# 2 Proposed Converter Topology

The design of a multi-inputs interleaved DC-DC step-up converter along with coupled inductor is delineated in Fig. 2. This will expand the voltage gain, maintaining high power density and diminish the voltage stress on the power semiconductor devices, and moderate the current ripple.



Figure 2: Multi-inputs interleaved DC-DC step-up converter along with the coupled inductor

This is best suited for high-power application permits for a reduction in the ripple of the input current and conduction mode. The behavioral control portion of this paper of the converter is analyzed with reference to sources. The switching modes of the used converter are visible in Fig. 3.



Figure 3: The new converter switching signals

#### 2.1 Operation Modes

This section explains the proposed converter working principles. The new converter can be worked in three other ways utilizing the same circuit by controlling the like switches.

**State-1:** During this situation, FC and PV are green charging batteries and supplying power to load.  $S_1$ ,  $S_3$ , and  $S_4$  are ON and are driving within the mode as appeared in Fig. 4a. Magnetizing inductor ( $L_m$ ) stores energy. Besides,  $L_m$  and leakage inductance ( $L_k$ ) is charged at source voltage. When the coupling coefficient is 1. The Magnetic inductor current is directly increased.  $D_2$  and  $D_6$  don't conduct, they are reverse biased, and the voltage of the capacitor remains fixed. In either case,  $D_1$ ,  $D_3$ ,  $D_4$ , and  $D_5$  will run in this state. At last, load energy is provided by the capacitor output  $C_0$ .



Figure 4: Modes of operation (a) state-1 (b) state-2 (c) state-3

When the switch is turned on, each leakage inductance and the magnetization are loaded, and the following equation can be achieved.

$$\mathbf{V}_{\mathrm{in}} = \mathbf{V}_{\mathrm{Lk}} + \mathbf{V}_{\mathrm{Lm}} \tag{1}$$

where  $V_{Lk}$  and  $V_{Lm}$  are the voltage across the leakage inductance voltage and the magnetization inductance, respectively. In view of the coupling effect, the voltages across the leakage and magnetization inductances can be expressed as

$$V_{Lk} = k V_{in} \tag{2}$$

 $V_{Lm} = (1-k) V_{in}$ 

where k-coupling co-efficient and  $V_{in}$ -input voltage

*State-2:* In state-2 condition, FC and PV release the battery and provide energy to the load. The switch,  $S_4$ , is OFF, and  $S_1$ ,  $S_2$ ,  $S_3$  are ON, as appeared in Fig. 4b.  $D_5$  doesn't conduct, and after that, they are green reverse biased. During this state, the inductor  $L_1$  is charged by  $V_{PV}$ , and the magnetic inductor  $L_m$  discharges the energy to the output capacitor. Be that as it may, the diode of  $D_1$ ,  $D_2$ ,  $D_3$ ,  $D_4$ , and  $D_6$  are forward biased and conduct.

*State-3:* FC and PV power the load, whereas the battery is not utilized. In this situation, the system operates without green charging or discharging the battery. The switches  $S_1$ ,  $S_3$  are ON, and the remaining switches are OFF, as appeared in Fig. 4c. The diode of  $D_1$ ,  $D_3$ , and  $D_4$  is turned ON. The inductor  $L_1$  and  $L_m$  are green charged through control sources  $V_{PV}$  and  $V_{FC}$ , individually.

## 2.2 Controlling Techniques

In this article, a controller related to an ANFIS has emerged for a multi-input interleaved boost converter. The ANFIS is a conventional fuzzy system, except that at each stage, the calculations are performed by a layer of hidden neurons, a neural network to enhance the knowledge of the system. Provides learning skills and contains components of in relative parameters of ANFIS membership function and input and output vary with learning. Output errors are used to adapt to the required parameters using standard back-propagation algorithms. Fig. 5 shows a flowchart of the power management technique.



Figure 5: Flowchart of the power management technique

(3)

It is necessary to change the FIS structure by dividing the desired format. In work [41], ANFIS design and implementation reference model controller related MPPT utilizing FPGA for PV. Fig. 6 shows the new controller design of the controller for the output ON-OFF switch. The design of Fuzzy based controller to this proposed converter is unique. This is considered as one of the major limitation in this research work.



Figure 6: ANFIS controller design for output ON-OFF (a) Switch 1 and 3 (b) Switch 2 and 4

## **3** Design Considerations

Switch current to find out the minimum input voltage, duty cycle (D), for less source voltage is used because it has maximum switch current.

$$D = 1 - \frac{V_{IN(min)} \times \eta}{V_{OUT}} \tag{4}$$

 $V_{IN(min)}$ -Minimum input voltage, V<sub>OUT</sub>-Required output voltage,  $\eta$ -converter efficiency

The inductor value is calculated from the current and voltage ripple, respectively. The inductor value is characterized as

$$L = \frac{V_{IN} \times (V_{OUT} - V_{IN})}{\Delta I_L \times f_S \times V_{OUT}}$$
(5)

 $V_{IN}$ -Input voltage,  $f_s$ -switching frequency,  $\Delta I_L$ -Estimated inductor ripple current

$$\Delta I_L = (0.2 \text{ to } 0.4) \times I_{OUT(max)} \times \frac{V_{OUT}}{V_{IN}}$$
(6)

I OUT (max)-Maximum output current necessary.

The coupled inductor turns proportion plays a critical part in regulating the stress of current and voltage between power devices. The average magnetizing inductance current  $(I_{Lm(avg)})$  may be determined as follows

$$I_{Lm(avg)} = \frac{(N+1)I_{out}}{(1-D)}$$
(7)

N-turns ratio, Iout-output current

The magnetizing current ripple  $(\Delta I_{Lm})$  can be specified by

 $\Delta I_{Lm} = 0.15 \times I_{Lm(avg)} \tag{8}$ 

The magnetizing inductance depends on the source current and may be computed as follows

$$L_m = \frac{DV_{IN}}{f_s \Delta I_{Lm}} \tag{9}$$

Determining the turn's ratio plays a critical part in getting the gain of voltage, the stress of the voltage on the switch, and the diode.

The capacitor value is given by the taking after formula

$$C_{OUT(min)} = \frac{I_{OUT(max)} \times D}{f_s \times \Delta V_{OUT}}$$
(10)

 $C_{OUT(min)}$ -minimum capacitor output,  $\Delta V_{OUT}$ -Preferred ripple of the output voltage.

Fig. 7 depicts the proposed control scheme for E(k), DE(k), and the rule viewer using a membership function fuzzy controller. Fig. 8 appearance curves of the duty cycle and voltage gain. It can be observed that a new converter performs maximum gain of voltage without an especially a maximum turn ratio. Fig. 9 displays the power loss error compared to the power loss of the proposed converter. It can be noticed that the mainline losses of power are diode inductor losses, switch loss, and inductor losses. They are improving the efficiency of the new converter.



**Figure 7:** (a) Design of fuzzy (b) Input variable DE(k) Membership functions (c) Input variable E(k) Membership functions (d) Rule viewer



Figure 8: Voltage gain vs. duty cycle



Figure 9: Input voltage vs. power loss

# 4 Simulation Results and Discussion

To affirm the effectiveness of the new proposed is simulated utilizing MATLAB/Simulink software package. Each source inputs are configured in a 20 V. 24 V, 3-Ah lithium-ion battery that is utilized as an element of energy storage.

High power density, high reliability, act, and high-temperature recycling are the lithium-ion batteries characteristics. Be that as its one of demerits is the high cost [42]. Li-ion type batteries are utilized broadly due to their great act in practical electronic devices [43]. The proposed converter simulation parameters are appropriate in Tab. 1.

| Symbol                      | Parameters             | Range      |
|-----------------------------|------------------------|------------|
| $\overline{V_{PV}, V_{FC}}$ | Input voltages         | 20 V, 20 V |
| $\mathbf{V}_0$              | Output voltage         | 200 V      |
| $\mathbf{P}_0$              | Output power           | 400 W      |
| fs                          | Switching<br>frequency | 15.5 KHz   |

 Table 1: Proposed converter simulation parameters

(Continued)

| Table 1: Continued |                        |                |  |  |  |  |
|--------------------|------------------------|----------------|--|--|--|--|
| Symbol             | Parameters             | Range          |  |  |  |  |
| D                  | Duty cycle             | 0.81           |  |  |  |  |
| $L_{m}$            | Magnetizing inductance | 100 µH         |  |  |  |  |
| $L_k$              | Leakage inductance     | 200 µF         |  |  |  |  |
| $C_1, C_0$         | Capacitors             | 22 nF, 1200 µF |  |  |  |  |
| R <sub>L</sub>     | Load resistance        | 100 Ω          |  |  |  |  |

In order to fulfill the control battery state of charge (SOC), the ANFIS control mechanism is used. Here the battery to charger and discharge on their SOC, the ANFIS controller has a greater dynamic response, and it has the merits of less stable errors and faster response times. Comparative analysis has also been performed for better analysis of results; the results of the simulations confirm the newly implemented converter performance (Figs. 10 and 11) and show the transient behavior. Fig. 12 appears the output current and voltage waveform obtained from the proposed converter simulation. The system's output voltage remains very well regulated at the required level, with no overshoots. The output voltage of the system has a very low level of ripple Fig. 13.





Figure 10: Simulation results of input voltages and output voltage

Figure 11: Simulation result of the inductor current



SOC (% 50.0005 2005 50 0.02 0.04 0.06 0.08 0.1 0.12 0.14 0.16 0.18 0.2 0 Time (S) BATTERY CURRENT Current (A) 0 -50 100 0.02 0.04 0.06 0.08 0.12 0.14 0.16 0.18 0.2 0 0.1 Time (S) BATTERY VOLTAGE **/oltage (V)** 0.02 0.04 0.06 0.08 0.12 0.14 0.2 0.1 0.16 0.18 Time (S)

Figure 12: Simulation results of load current and voltage

Figure 13: Simulation results of battery SOC, battery current, and voltage

Moreover, the MOSFET voltage stress is lower than the output voltage. As a result of soft switching technology, turn-OFF switching losses in each switch would be reduced and helps to improve the system efficiency.

From Fig. 14, the normalized voltage stress with respect to the semiconductor is significantly less than with other converters. Inductor current sharing is obviously greater, which reduces the current ripple.



Figure 14: Switch voltage stress vs. duty cycle

This reduces the output capacitor's size and increases the converter's overall power density. Fig. 15 shows the converter efficiency. Subsequently, the proposed converter made it incredibly reasonable for connecting a renewable energy application that needed high voltage gain and efficiency. All of the

simulation results show that the proposed interleaved non-isolated great boost dc-dc converter control technique for renewable energy system applications will provide reasonable results even when converter operations change.



Figure 15: Output power and efficiency

## 4.1 Description

The following discussion points may be extracted from the simulations and case studies mentioned above.

- An impartiality comparison with previous research validates the constructed interleaved nonisolated coupled inductor-based high step-up dc-dc converter, as shown in Tab. 2.
- The simulation results illustrate the transient behavior of the newly implemented converter Figs. 10 and 11. The output current and voltage waveforms from the suggested converter simulation are shown in Fig. 12.
- The ANFIS controller (Fig. 6) has a fast response time, a better dynamic response, and it is utilized to monitor the output voltage variations.
- Voltage stress with respect to the semiconductor The ANFIS controller (Fig. 14) is significantly less than with other converters, and efficiency also improved (Fig. 14).
- A non-isolated interleaved high gain DC-DC converter with coupled inductor was proposed and to attain a high gain of voltage.

| Voltage<br>gain (M)<br>V <sub>out</sub> /V <sub>in</sub> | Voltage<br>stress on<br>switches | Diode<br>voltage<br>stress          | No. of<br>components |   |   | No. of<br>inductor |          | Input<br>current | Topologies         |
|--|----------------------------------|-------------------------------------|----------------------|---|---|--------------------|----------|------------------|--------------------|
|  |                                  |                                     | $\overline{S}$       | D | С | Sing               | gle Coup | pled             |                    |
| $\frac{N+1}{1-D}$  | $\frac{V_{out}-V_{in}}{6}$       | $5 	imes rac{V_{out} - V_{in}}{6}$ | 4                    | 6 | 2 | 1                  | 1        | Continuous       | Proposed converter |
| $\frac{2N+4}{1-D}$                                       | $\frac{1}{2N+4}$                 | $\frac{N+1}{(N+2)}$                 | 2                    | 4 | 4 | 0                  | 2        | Continuous       | [12]               |
|  |                                  |                                     |                      |   |   |                    |          |                  | (Continued)        |

**Table 2:** Execution comparison between other topologies and proposed converter

(Continued)

| Table 2: Continued                                       |  |                                      |                      |   |   |                    |   |                  |            |
|--|--|--------------------------------------|----------------------|---|---|--------------------|---|------------------|------------|
| Voltage<br>gain (M)<br>V <sub>out</sub> /V <sub>in</sub> | Voltage<br>stress on<br>switches                                 | Diode<br>voltage<br>stress           | No. of<br>components |   |   | No. of<br>inductor |   | Input<br>current | Topologies |
|  |  |                                      | S                    | D | С | Single Coupled     |   | oled             |            |
| $\frac{2(N+1)}{1-D}$                                     | $\frac{V_{out}}{2(N+1)}$   | $\frac{2(N+1)V_{out}}{2(N+1)}$       | 4                    | 2 | 3 | 0                  | 2 | Continuous       | [16]       |
| $\frac{3-2D}{1-2D}$                                      | $\frac{V_{\scriptscriptstyle out}-V_{\scriptscriptstyle in}}{2}$ | $\frac{V_{out}-V_{in}}{2}$           | 2                    | 4 | 3 | 1                  | 0 | Continuous       | [20]       |
| $\frac{2(N+1)}{1-D}$                                     | $\frac{V_{out}}{2(N+1)}$   | $\frac{NV_{out}}{N+1}$               | 2                    | 4 | 4 | 0                  | 2 | Continuous       | [24]       |
| $\frac{(ND+1)}{1-D}$                                     | $\frac{V_{out}}{1+ND}$   | $\frac{(1-D)NV_{out}}{(1+ND)V_{in}}$ | 1                    | 2 | 3 | 2                  | 1 | Continuous       | [39]       |
| $\frac{N+2}{1-D}$  | $\frac{V_{in}}{1-2D}$  | $\frac{(N+1)V_{in}}{1-2D}$           | 1                    | 4 | 5 | 1                  | 1 | Continuous       | [40]       |
|  |  |                                      |                      |   |   |                    |   |                  |            |

#### **5** Conclusions

A non-isolated interleaved high gain DC-DC converter with coupled inductor was proposed in this paper in order to attain a high gain of voltage without a high turn ratio. In the absence of one or two resources, the converter is capable of supplying the required power to the load. The modeled converter is in three separate operating states and is used to create a suitable controller. The gain of voltage, stress voltage on the switches and diodes, conduction losses, and performance of the proposed converter were all studied. The percentage of voltage stress on diodes and switches was lower in the proposed converter as compared to the output voltage, and low-voltage rated MOSFETs with a limited ON-resistance were supplied to minimize the loss of conduction. It is also possible to obtain a low-ripple continuous input current, and the ANFIS regulation technique would be used to monitor the output voltage variations. The converter process is evaluated and verified using Matlab/Simulink simulation.

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