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Physio-Mechanical Characterization of Recycled Polyethylene Terephthalate and Soda-Lime Glass Waste Composite for Roof Tile Application

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ABSTRACT

The research paper focuses on manufacturing composite materials from waste polyethylene terephthalate (PET) reinforced with soda-lime glass to provide a lightweight, less brittle, and high rust resistance when exposed to hazardous environment. In developing nations such as Nigeria, there is a significant surge in the volume of bottled water and other packaging materials used in households, leading to a rapid accumulation of biodegradable waste, that presents concerns such as the creation of landfills and health issues. PET are thermoplastic polymer that can be melted and shaped into various objects. This study involves the incorporation of soda lime glass with recycled PET with various weight proportions to create a composite for roof tile application. The processing phases encompass the gathering of discarded PET and glass, purification, fragmentation, glass treatment, composite fabrication, and physio-mechanical and microstructural characterization. The utilization of soda lime glass in the recycling of plastics led to the creation of cost-effective and efficient roof tile composites, while also decreasing environmental pollution. The density of the composite tile varied between 1.000242–1.600259 g/cm³ with 20 wt.% filler having the lowest density. The water absorption ranged from 0.12%–0.79%. Mechanical characterization results revealed that the hardness and tensile strength increased with increasing wt.% of reinforcement (soda-lime glass) with the highest values being 271 HBN and 12 N/mm² (peak) at 60 and 50 wt.% filler (soda-lime glass), respectively. The composite samples had similar impact strength which varied between 70–74 J. Fourier Transform Infrared (FTIR) analysis reveals the occurrence of chemical and mechanical improvement during the recycling process. The composites exhibited promising properties from the research and revealed that the addition of the reinforcement largely improves the properties.

KEYWORDS

Polyethylene terephthalate (PET); soda-lime glass; physical; mechanical properties; roof tile



1 Introduction

The global construction industry is facing increasing costs and resource demands, while plastic waste poses a significant environmental threat due to its non-biodegradable nature and pollution through incineration and landfill. Waste glass and polyethylene terephthalate (PET) bottles are consistently present in nearly all waste streams, often polluted with mixed-colour sources of varying compositions. Consequently, over 60% of these wastes are discarded in landfills and marine bodies causing sustainability. With 46 million tonnes of glass packaging in 2012 and 52 million tonnes of flat glass (mostly for buildings and automobiles) in 2009, the global market for glass packaging in containers accounted for about 85% of global output [1]. The global glass manufacturing market size was estimated at USD 106.44 billion in 2021. Nevertheless, with the emergence of new technologies in the glass production business, the degree of glass utilization has greatly grown to encompass solar panels, lighting applications, shelves, windows, appliances, and fiber optic cables. Glass waste originates from two sources: manufacturing firms that discard pieces that do not fit technical criteria or specialized retailers that sell glasses and accessories [2].

Matrix recycling is emerging as the most promising method for mitigating plastics' environmental consequences, particularly in end-of-life management [3]. The recycling process of PET and soda-lime glass significantly influences their properties and suitability for composite applications. Recycled PET (R-PET) can be effectively used as a filler in various composite materials, enhancing their mechanical properties. The transition from a linear economy to a circular economy model for managing recycled PET and soda-lime glass waste offers significant environmental, economic, and social benefits. The circular economy emphasizes reuse, recycling, and regeneration of materials, reducing waste and conserving resources. Recycling PET bottles through methods like mechanical downcycling, closed-loop glycolysis, and upcycling can minimize greenhouse gas emissions and enhance material circularity [4,5]. Recycling soda-lime glass can reduce carbon dioxide emissions by 5%, contributing to sustainable development and cost savings in raw materials [6]. Overall, adopting a circular economy model for PET and soda-lime glass waste not only mitigates environmental impacts but also promotes sustainable industry practices and economic resilience.

Additionally, combining R-PET with date palm fibers in unsaturated polyester (UP) composites enhances thermal behavior at high temperatures, although the flexural strength may decrease due to non-uniform filler distribution [7]. On the other hand, recycled soda-lime glass, when used as a filler in polytetrafluoroethylene (PTFE) composites, affects the dielectric, mechanical, and thermal properties. Increasing the volume fraction of recycled soda-lime glass reduces tensile strength but improves moisture absorption and density, with the lowest coefficient of thermal expansion observed at higher filler content [8]. Furthermore, using recycled PET as a matrix for glass fiber-reinforced virgin PET composites can significantly enhance crystallization kinetics and mechanical properties, making the material suitable for automobile applications [9,10]. Overall, the recycling process not only provides an environmentally friendly solution but also tailors the properties of PET and soda-lime glass for specific composite applications, enhancing their performance and expanding their utility in various engineering fields.

Despite their excellent mechanical and thermal qualities, PET composites have a low impact strength, limiting their use in a variety of applications. Numerous studies have demonstrated that the addition of various copolymers can significantly improve the impact strength of virgin and recycled PET [11,12]. These properties include PET being lightweight, cheap, non-corrosive, and non-biodegradable. It also has other properties which are low density, low moisture absorption, good creep, and chemical resistance [13]. Soda lime glass is valued for its affordability, chemical stability, and robust physical characteristics such as hardness, adaptability, and the unique feature of being recycled through multiple times of melt and reshaping without significantly losing quality [1,14]. The increasing

demand for materials used in building construction due to population growth has brought about the exploration of low-cost and economical ways of manufacturing these materials.

The roof covering is made of steel, concrete, aluminum, ceramic, and others which is a crucial element of a building's design since it provides all-around security while providing protection from the elements such as rain, sun, bad weather, etc., and contribute to the character of our townscapes from every angle [15,16]. However, the material has their various challenges ranging from noise, high expansion rate, corrosion, density, carbonization, etc. [17,18]. The utilization of polystyrene-based matrix composite as roof or pavement tiles has become prevalent with the integration of various reinforcements resulting in exceptional fracture toughness characteristics with excellent melt temperature on microcell diameter and density during injection molding [19]. Roof tiles made from plastic composite have some advantages as compared to traditional roof tiles such as low water absorption, high flexural resistance, low specific weight, and excellent resistance to hail and freezing [20].

The composite tiles offer a novel method for recycling waste plastic material in a sustainable and cost-effective manner, both in our daily lives and business. This can be utilized to construct structures that are lightweight, corrosion-resistant, chemically resistant, cost-effective to produce, have an extended lifespan, and, most importantly, address the societal problem of plastic waste [21]. An experimental investigation was conducted to examine the properties of roof tiles made from a combination of sand and recycled PET in different proportions. The results indicate that these plastic composite tiles exhibit excellent strength and absorbency, making them suitable for use in roof tiles [22]. This study explores the possibility of using glass as a substitute for natural aggregates in the construction industry, specifically roofing tiles. The focus is on addressing environmental concerns and analyzing the economic viability of this application. Additionally, the study aims to further develop post-consumer markets for recycled polymers and waste glasses by promoting recycling and reducing the use of landfills.

2 Materials and Methods

Recycled Polyethylene Terephthalate (R-PET) with 0.91 g/cm^3 density sourced from the waste water bottle containers as classified [23] accumulated within the University of Ilorin, which lies between latitude 8.4799°N and longitude 4.5418°E , Ilorin, Nigeria was washed with water, cleaned, dried and shredded into flakes. Soda-lime glass (in broken form) from industrial waste is characterized by its green color, which helps block ultraviolet light to preserve the quality of the beverages. The green tint is achieved by adding iron oxides during the glass manufacturing process and reuse as reinforcing fillers provides thermal insulation in addition to its irregular and micrometric predominant presence of Na, Si, and Ca elements [24]. The soda-lime glass particles were produced by manual crushing, hammer milling, and 70 h ball milling in line with sieved to get a particular range of particle size which was 100 microns as seen in Fig. 1a.

2.1 Composite Production

The composite production process flow is depicted in Fig. 1. The R-PET plastic was washed thoroughly to remove impurities, then shredded for an easy melting process loaded into a metallic pot, and placed on a gas burner. The soda-lime glass was pulverized in two stages. Firstly, it was milled with a locally made electrically motorized hammer mill machine to get a coarse glass particle. The coarse glass particle was further milled in a ball mill machine to get a fine particle. The fine glass particle was sieved to obtain a particle size of 100 microns particle size. Fig. 1b depicts the glass particles varied from 20 to 60 wt.% with respect to PET plastics using a mold with five different samples as designed in Table 1. It was subjected to an elevated temperature of about 260°C (melting temperature of PET plastic) which was maintained to avoid excessive entrapment of gases. The mixing was carried out at

110°C and 40 rpm for 10 min by a HAAKE internal mixer (HBI System 90, Chicago, MI, USA) [25] as presented in Fig. 1c. This was done to ensure an ideal dispersion and distribution of the particles. A mold of 120 mm × 120 mm × 3 mm was utilized to cast the composite slabs, with foil paper employed as the mold release agent. The cast composite samples were cured at room temperature for 24 h before conducting physical, mechanical, and morphological characterization as depicted in Fig. 1d.

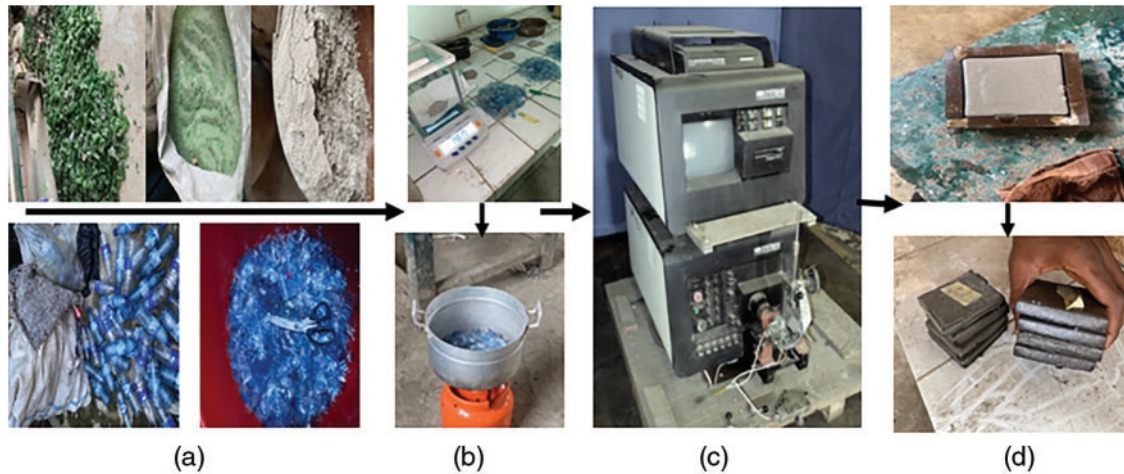


Figure 1: Composite preparation (a) material sorting and grinding (b) weighting and melting (c) mechanical mixing (d) mold samples

Table 1: The formulation used in this research

Sample composition	PET plastic (wt.%)	Soda-lime glass (wt.%)
PET80:G20	80	20
PET70:G30	70	30
PET60:G40	60	40
PET50:G50	50	50
PET40:G60	40	60

2.2 Physical Property Test of the Composite

2.2.1 Density

The mass of the samples was recorded using the water displacement method as per the ASTM D4052 standard. A predetermined volume of water was obtained using a measuring cylinder with a capacity of 250 ml. A single sample piece was submerged in the measuring cylinder, and the resulting increase in water level was measured and recorded. The composite volume is calculated by subtracting the initial known volume of water from the water containing the sample. Eq. (1) depicts the density of a particular piece of composite by dividing its mass by its volume. The identical technique was executed for all the other composites to acquire their densities, with a total of five specimens being utilised in each sample to calculate an average.

$$\text{Density } (\rho) \text{ (g/cm}^3\text{)} = \frac{\text{mass (g)}}{\text{Volume (cm}^3\text{)}} \quad (1)$$

2.2.2 Water Absorption and Thickness Swelling Tests

The test sample with 60 by 60 by 10 mm³ in accordance with ASTM D570-22 standard [26]. The samples were dried using by using an oven, they were then cooled and the weight of each sample was measured. Five samples from each combination were selected and subjected to a drying process in an oven for 24 h at 100 ± 3°C. The weight and thickness of dried specimens were measured with a precision of 0.001 g and 0.001 mm, respectively. Subsequently, the specimens were submerged in distilled water for one week and maintained at 22 ± 2°C. The weight and thickness of the specimens were measured following the removal of surplus water from their surface. The alteration in weight is documented and employed to compute the percentage water absorption with Eq. (2):

$$\text{Water absorption (\%)} = \frac{\text{final weight} - \text{initial weight}}{\text{initial weight}} \times 100 \quad (2)$$

Also, the value of the thickness swelling performed to investigate the increasing thickness with time due to moisture (water) absorption. The samples were taken out and dry clean after every 7 days and measure the dimensional changes with vernier calliper with the least count of 0.01 mm according to equation using the Eq. (3) [27,28].

$$\text{Swelling thickness (\%)} = \frac{\text{Wet thickness } (t_2) - \text{Dry thickness } (t_1)}{\text{Dry thickness } (t_1)} \times 100 \quad (3)$$

2.2.3 Porosity

The porosity of the samples was determined by soaking the samples in a bath of water and oil. Mass of the samples before and after soaking were determined and recorded. Porosity of the samples was calculated using the formula below; where m_1 is the mass of brick before soaking, m_2 mass of brick after soaking, ρ is the density of the liquid mix and V is the volume of the sample in Eq. (4).

$$\% \text{ Porosity} = \frac{m_1 - m_2}{\rho V} \times 100 \quad (4)$$

2.3 Mechanical Testing of the Composite

Hardness values of the composites was determined by Brinell hardness testing machine, using a hardened steel ball indenter load of 100 kgf [29]. Two different moulds were prepared for tensile and impact testing. The composite samples were shaped into dumbbell form for tensile tests, following the ASTM D638 guidelines. The experiments were conducted with a consistent 0.5 mm/min strain rate. The IZOD impact test was performed on composite samples using a fully instrumented Avery Denison test machine, following the ASTM D256-93 guidelines. This approach was used to measure the strength of composite samples under sudden load applications. The tests were conducted using three identical specimens, and the results presented are the average values obtained from testing all the composite samples.

2.4 Analysis of Composite Using Optical Microscopy and Fourier Transform Infrared Spectroscopy

The morphology of the composites was examined using an optical microscope (XL 30, Philips, Eindhoven, Netherlands). The analysis was conducted at a magnification of 200×. Changes in chemical structures and functional groups was characterized using ASTM E1252-98 (2013) with FTIR spectrometer (Perkin Elmer Spectrum 400, Waltham, MA, USA) using a resolution of 4 cm⁻¹ over the spectral range of 4000–650 cm⁻¹.

3 Results and Discussion

3.1 Physical Properties of the Composite

The density results obtained from the water displacement analysis of the particle-reinforced composite samples provide valuable insights into the composition and structural characteristics of each material. [Table 2](#) shows the density kept on increasing with an increase in weight composition of soda-lime glass which is in line with composite material made from recycled materials [30]. PET80:G20 shows the lowest density which was 1.000242 g/cm³ and kept increasing up to the composition of PET50:G50. The density value is implying that even with a higher glass content, the particle glass still contributes to maintaining a relatively low density far from the traditional roofing tiles [31]. The fourth sample containing an equal mix by wt.%, displays a significantly higher density of 1.600259 g/cm³ which was even higher than that of PET40:G60 which had a higher proportion of glass. This result indicates that at a balanced composition, the composite material gains considerable mass and density. However, all the samples exhibited a lower density as compared to traditional roofing tile materials such as clay, asphalt shingles, ceramic, and Aluminium [32].

Table 2: Results of physical property of composite samples

Sample composition	Density (g/cm ³)	Water absorption (%)	Porosity (%)	Thickness swell test (%)
PET80:G20	1.000242	0.12	0.30	0.0008
PET70:G30	1.000284	0.22	0.75	0.079
PET60:G40	1.000563	0.72	0.28	0.008
PET50:G50	1.600259	0.79	0.78	0.115
PET40:G60	1.000589	0.23	0.04	0.705

Secondly, the water absorption result highlights the excellent water-resistant properties of PET70:G30 composite exhibiting the lowest water absorption rate of all the samples 0.12%. The majority of PET composition in samples with PET70:G30 and PET60:G40 had the highest water absorption rate of 0.72% and 0.79% respectively which can be used for pavement tiles. The utilization of PET plastic and increasing fine aggregate such as glass as reinforcement increases the water absorption resistance rate [22,33]. The problems that moisture causes in buildings have advanced significantly. However, the sample with PET40:G60 water absorption rate would start to decrease because generally, glass has a lower water absorption as compared to PET plastic. The samples produced had a relatively lower absorption as compared to conventional roof tile materials such as clay tile, asphalt shingle, and ceramics tiles with water absorption of 10%, 1%, and 5%, respectively [20,34].

Thirdly, the porosity test in [Table 2](#) depicts that sample PET40:G60 with the highest glass composition particle displayed the lowest porosity of 0.04%. This is because of the volume fraction of the reinforcement used enhancing the packing density and minimizing gaps thereby reducing the chances of porosity occurring. Samples PET70:G30 and PET50:G50 displayed the highest porosity of 0.75% and 0.78%, respectively. The presence of pores affects mechanical properties such as strength, toughness, and stiffness [35]. The porosity was influenced by the processing condition during the production of the composite material such as stirring continuously which helps to get rid of the trapped gases [16].

Lastly, the samples exposed to the ambient environment and the thickness swell percentage results are recorded in [Table 2](#). PET80:G20 having the least amount of particle glass reinforcement showed an extremely low swell percentage of 0.0008% as compared to the other samples. The result suggests that

the material has excellent resistance to swelling when exposed to a high-temperature environment. The high PET content likely contributed to the resistance. It could be observed that the swell value increased with an increase in particle glass. PET50:50 swell of 0.115%. The result indicates that an increase in the composition of particle glass increases the swell rate up to 0.705% as seen in PET40:G60. The higher amount of particle glass in PET plastic may have reduced the effective glass transition temperature, increasing the composite's susceptibility to swelling. research has established that thickness swelling minimizes interfacial adhesion [28,36].

3.2 Result of Mechanical Testing of the Composite

Fig. 2 shows the tensile properties of the compositions, it was observed that at 50 wt.% of glass and PET (PET50:G50), loading, the maximum tensile strength of the composite was 12 MPa and the minimum tensile strength was 4.06 MPa when the weight of glass is 20% matrix which is greatly close to the traditional roof tiles [20,32]. PET50:G50 can withstand the highest stress at yield, the composite material starts to undergo permanent deformation and might have been influenced by greater interfacial bonding between the matrix and the reinforcement. The tensile strength is affected by the distribution and dispersion of the particles in the matrix [37]. PET40:G60 tensile strength decreased because ofglomeration because the most reinforced constituent is a particle. Reinforced agglomerations happened thus causing dispersion problems in PET, which led to a decrement in tensile strength [38].

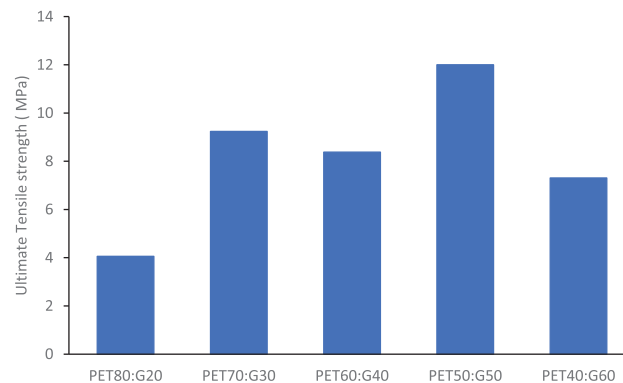


Figure 2: Tensile strength for samples

From the results obtained in Table 3, it was observed that the fine aggregate glass has a significant effect on the hardness properties of composite. The hardness Brinell number average value of the samples increased with increase in particle glass which is in line with studies in literature [39]. The rapid rise in hardness value was seen at 60 wt.% glass as seen PET40:G60 with a hardness value of 271 HBN. The hardness of a composite material increases with an increase in particle size being added to the matrix. Similarly, the impact resistance average value in Table 3 depicts that highest sample PET40:G60 exhibited the highest impact strength value of 74 J which may be the effect of toughening of the composite due higher percentage of particle glass could have acted as crack arrester, preventing the propagation of crack and enhancing the material's ability to absorb energy during impact [40]. On the other hand, PET70:G30 had the lowest impact energy value of 70 J. Furthermore, other samples were within the same range which could be adjudged to the fact that addition of reinforcement up to 6% increases the impact energy strength but above that, the impact resistance begins to reduce and hardness increase.

Table 3: Results of average hardness and impact of composite samples

Sample composition	Hardness (HBN)	Impact strength (J)
PET80:G20	180	73.5
PET70:G30	186	70
PET60:G40	203	71.5
PET50:G50	205	73.5
PET40:G60	271	74

3.3 Optical Microscopy and Fourier Transform Infrared (FTIR) Spectroscopy

The micrograph of the samples depicts reinforcement was dispersed evenly to a great extent as seen in Fig. 3. To support the interpretation of the mechanical results, a morphological study has been performed. Fig. 4 shows optical micrographs of the produced materials at the same enlargements ($\times 200$). The dark patches represent the matrix PET and the light patches are the particle soda-lime glass serving as reinforcement which dominance kept on increasing as the wt.% of particle glass was increased. The PET80:G20 micrograph depicts greater dispersal of the PET fraction and their potential interfacial bonding with the PET chain. The combination of RPET with a greater proportion of soda-lime glass composites enhances hardness and impact strength due to uniform reinforcement distribution as seen in the PET 40:G60 sample. Moreover, The FTIR spectra of PET plastic and soda-lime glass composite are shown in Figs. 4–6, respectively. The spectrum exhibited characteristic peaks associated with both PET and soda-lime glass. The peak of the C-H bending vibration is around 720 cm^{-1} which also decreases as the PET ratio decreases which is in line with the PET peak around 725 cm^{-1} observed in microplastics PET [41]. The corresponding PET peak includes C-H stretching vibrations, C=O stretching (carbonyl) vibrations, which appear strongly at 1638 cm^{-1} , and C-O-C stretching vibrations. Additionally, peaks 1000 cm^{-1} , associated with the Si-O stretching vibrations of soda-lime glass were observed. The relative intensity of these peaks provided insight into the composition of the composite, with higher intensities indicating a greater concentration of specific functional groups as found in similar studies [36,42,43]. The spectra of the PET80:G20 and PET70:G30 reveal similar trends PET60:G40, PET50:G50, and PET40:G60 revealed polymeric absorption bands with lower intensities than later composites. It implies that there has been compatibilization between the surface of the soda lime glass reinforcement and the RPET, therefore giving strong adhesion between the matrix and filler.

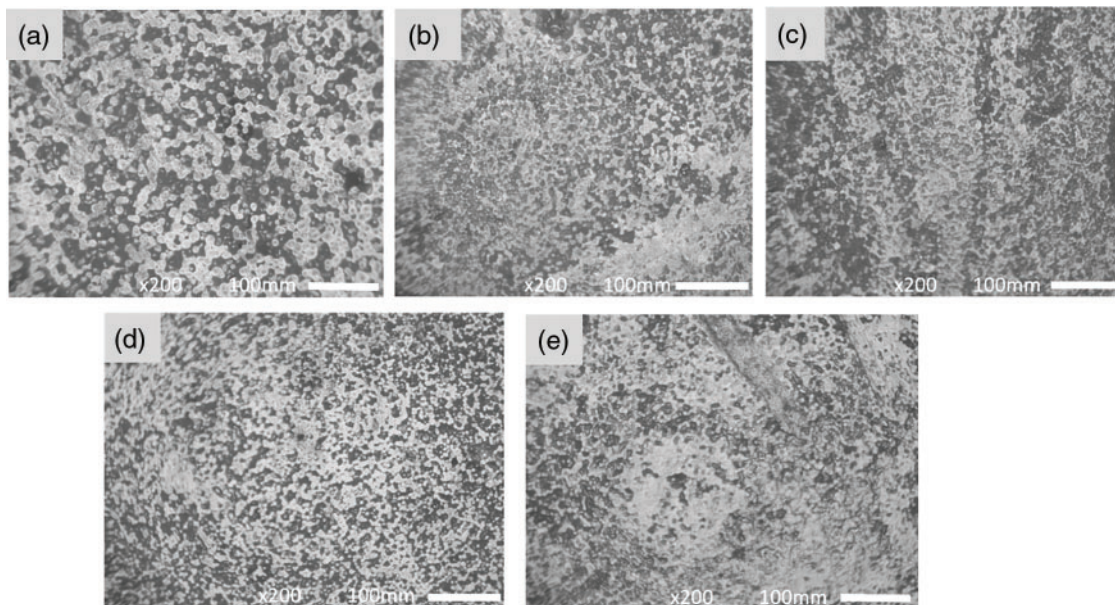


Figure 3: Microstructure at 200× (a) PET80:G20 (b) PET70:G30 (c) PET60:G40 (d) PET50:G50 (e) PET40:G60

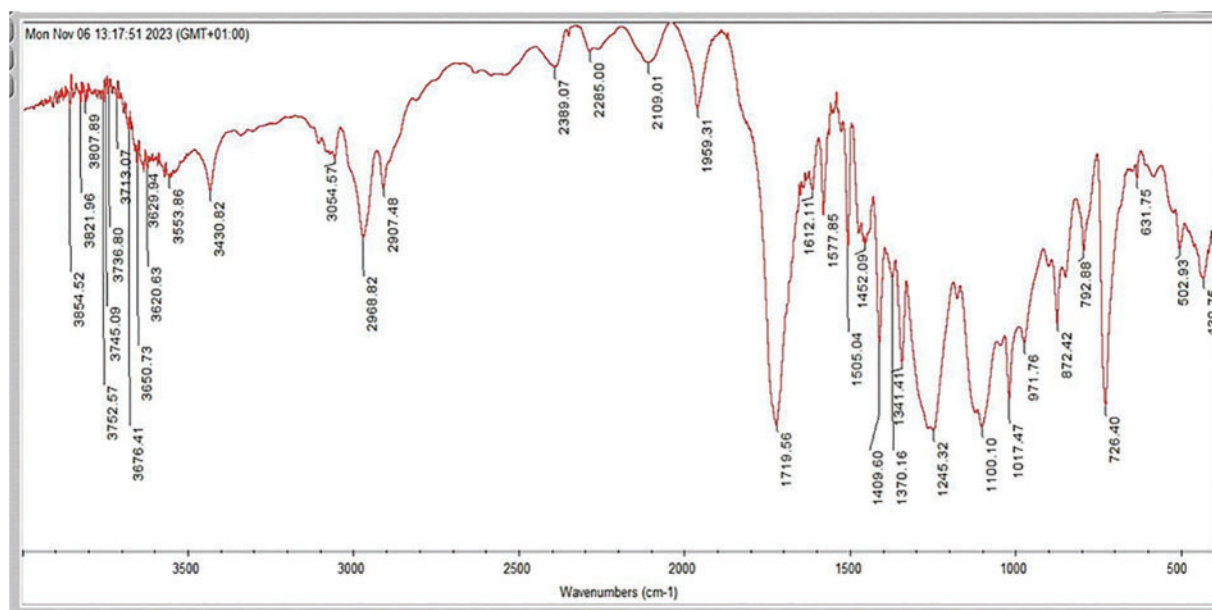


Figure 4: FTIR spectrum of PET80:G20

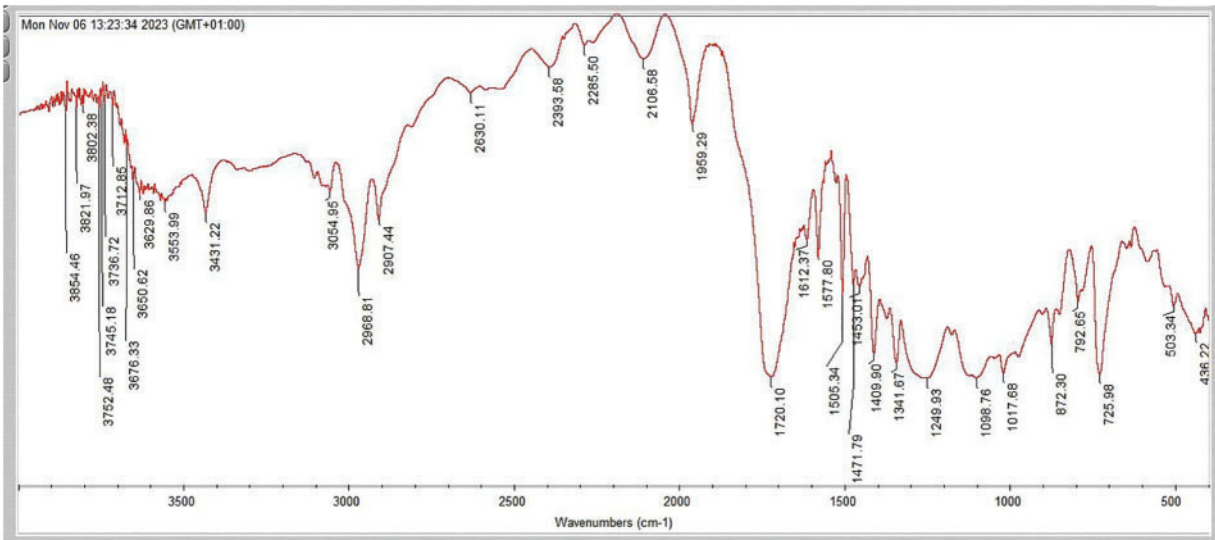


Figure 5: FTIR spectrum of FTIR spectrum of PET60:G40

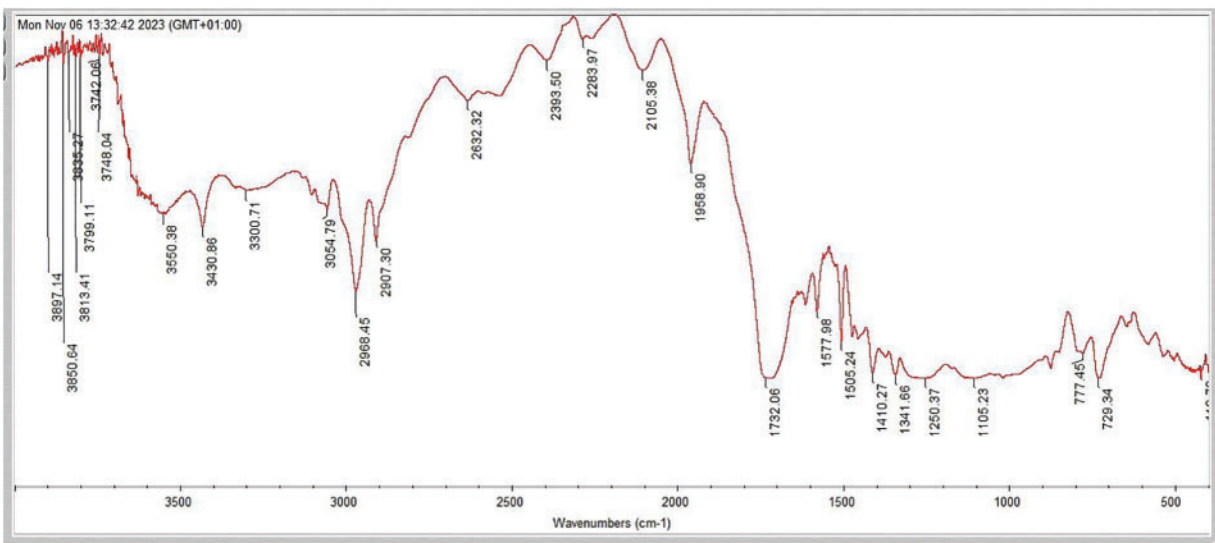


Figure 6: FTIR spectrum of PET40:G60

4 Conclusion

The worldwide market for composite roof tiles is growing rapidly since there is a rising need for long-lasting, visually appealing, and eco-friendly roofing materials. Market expansion is driven by increasing construction activity, widespread acceptance of green building techniques, and strict laws on sustainable building materials. Product innovation, technological advances, and the expansion of distribution channels will drive anticipated market growth in the upcoming years. The composite roof tiles market is anticipated to expand significantly to attract carbon credit. Polymer composite consisting of recycled polyethylene terephthalate plastic and soda-lime glass was successfully produced with different weight percentages of R-PET plastic and soda-lime glass with uniform microns size were utilized for this research. The following conclusion can be drawn:

- Physical characterization of the composite samples revealed that the density, water absorption, and swell increase with the increase in reinforcement.

- Microstructural examination of the composite showed that the reinforcement (soda-lime glass) was largely dispersed evenly.

- Mechanical characterization showed that the samples with higher composition of reinforcement possessed a better hardness and tensile strength. The impact strength of the samples was merely influenced by the varying composition with all samples having an almost similar impact strength value.

- Diverting waste PET plastic and soda-lime glass from landfills and repurposing them for building materials contribute to a reduction in the environmental impact of waste disposal and the extraction of biodegradable resources.

- The transformation of industrial ecosystems to a circular economy model can also provide competitive advantages such as higher productivity, better resource utilization, and market growth while delivering social, financial, and environmental benefits in developing countries.

The best recycling techniques for certain applications are essential for the evolution of sustainable recycling technology. Further studies of processing temperature or other manufacturing factors that can affect the efficiency in market scale such as melt flow index of the polymer-based composite. The investigation of thermal fluctuations and degradation for extended periods can substantially enhance an in-depth understanding of the mechanical properties.

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Ethics Approval: Not applicable.

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