



**ARTICLE**

# Enhancing Thermal Performance of Building Envelopes Using Hemp Wool and Wood Wool with Phase Change Materials

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## ABSTRACT

This study investigates the potential for enhancing the thermal performance of external walls insulation in warmer climates through the combination of phase change materials (PCMs) and bio-based materials, specifically hemp wool and wood wool. Experimental tests using the heat flow method (HFM), and numerical simulations with ANSYS Fluent software were conducted to assess the dynamic thermal distribution and fluid-mechanical aspects of phase change materials (PCMs) within composite walls. The results demonstrate a notable reduction in peak indoor temperatures, achieving a 58% reduction with hemp wool with a close 40% reduction with wood wool when combined with PCMs. Fluid-mechanical analysis indicates that PCMs act as efficient indoor temperature regulators by storing excess heat during hot periods and releasing it later during phase transitions. Furthermore, the homogeneous distribution of the liquid fraction and natural convection during phase change contribute significantly to the improvement in heat transfer rates, resulting in a 96% reduction compared to hemp wool and wood wool without PCMs.

## KEYWORDS

Bio-based materials; phase change material (PCM); heat flow method; thermal performance; external wall insulation; hemp wool; wood wool; ANSYS Fluent software; dynamic thermal distribution; fluid-mechanical analysis

## Nomenclature

$\rho$	Density ( $\text{kg}/\text{m}^3$ )
$\lambda$	Thermal conductivity ( $\text{W}/(\text{m}\cdot\text{K})$ )
$T$	Temperature (K)
$T_s$	Solidus temperature (K)
$T_l$	Liquidus temperature (K)
$T_{\text{out}}$	Outside temperature (K)
$T_{\text{in}}$	Inside temperature (K)
$t$	Time (s)
$C_p$	Specific heat capacity ( $\text{J}/(\text{kg}\cdot\text{K})$ )



L	Latent heat (kJ/kg)
$e$	Thickness (m)
HW	Hemp Wool
WW	Wood Wool
PCM	Phase Change Materials
HFM	Heat Flow Method

## 1 Introduction

The future of energy and sustainable construction is a growing area of interest and concern. According to the IEA's "World Energy Outlook 2022" report [1], enhancing the energy efficiency of buildings is crucial for achieving greenhouse gas emission reduction targets and combating climate change. The Global State of Buildings and Construction Report 2022 [2] indicates that the building sector contributes almost 40% of global energy consumption and about one-third of greenhouse gas emissions.

Various studies have focused on evaluating and improving the energy consumption of buildings by reducing heating and cooling needs. Hoseinzadeh et al. [3] underlined the importance of implementing specific strategies based on geographical and climatic conditions to achieve energy-saving improvements in buildings located in a mountainous, humid zone.

Researchers have evaluated insulation materials used in buildings to address energy losses through building envelopes. They highlight the importance of selecting appropriate insulation materials to enhance energy performance, taking into account their environmental aspects [4], and examining thermal inertia and insulation effectiveness in building structures [5].

The use of phase-change material (PCM) in exterior walls has been explored for their energy efficiency and CO<sub>2</sub> emissions reduction benefits [6], as well as their potential in enhancing thermal regulation in specific climatic conditions [7]. Research on PCMs demonstrates their ability to store and release substantial thermal energy, thereby attenuating temperature variations in buildings and reducing energy consumption [8]. El-Ganaoui et al. [9] have provided innovative analytical solutions to heat transfer problems involving phase changes and interfaces, forming the basis for numerous advances. Recent advancements in PCM technology highlight their potential for storing thermal energy in buildings [10,11]. Hekimoğlu et al. [12] noted the integration of PCMs into building cooling systems, which reduces the thermal load on air-conditioning systems and minimizes energy consumption, while Zhan et al. [13] focused on the integration of PCMs in buildings in hot climates.

Anter et al. [14] demonstrated the efficiency of integrating PCMs into building walls for thermal energy savings, highlighting the importance of optimizing the design, choice, and quantity of PCMs to maximize thermal benefits. M'hamdi et al. [15] analyzed the energy, environmental, and economic impacts of different building envelopes incorporating PCMs in different climates, showing that PCMs can reduce energy consumption and carbon emissions while offering economic benefits [16,17].

The potential of bio-based materials to enhance the sustainability and energy efficiency of buildings has also been studied [18–20]. These materials have demonstrated promising thermal and hygrothermal performances [21,22] and a low carbon footprint [23,24]. Using bio-based materials with PCMs improves energy performance in buildings [25], but careful assessment of their hygrothermal behavior is essential to prevent building deterioration [26,27].

Researchers have explored the combined use of PCMs with other insulating materials to enhance energy efficiency, such as dynamic insulation boards [28] and recycled waste paper in building enclosures, demonstrating potential for improved thermal performance and sustainability [29].

Recent studies have tackled the importance of fluid dynamics in these systems. Numerical simulations by Wang et al. [30] explored the coupling between solid-liquid phase change and thermal flow, providing valuable insights into fluid behavior in these materials. These studies also underline the crucial role of convection in the behavior of PCMs, as demonstrated by Lappa [31], with significant impacts on boundary conditions, material properties, and the integration of nanoparticles. A multi-physics modeling approach that considers the interactions between heat, mass, and fluid movement is necessary to study natural convection phenomena and heat transfer in phase change materials.

Optimizing material configurations is vital for maximizing building energy efficiency [32]. The application of new technologies, numerical modeling, and advanced simulation methods like Computational Fluid Dynamics (CFD) have been used to analyze and optimize thermal performance and design in buildings [33].

Zhou et al. [34] used CFD modeling to validate the thermal performance of dynamic Trombe walls incorporating PCMs, providing a better understanding of heat flows and more efficient solutions.

Integration PCMs and bio-based materials with advanced modeling techniques has shown promise in improving building efficiency [35]. Khoukhi et al. [36] focused on the effect of varying the dynamic thermal conductivity of insulation materials on temperature variation across wall assemblies.

While PCMs may have varying thermal performance depending on environmental conditions, they may be less effective in extreme climates or environments with minimal temperature variations [37]. To achieve thermal performance equivalent to conventional insulating materials, bio-based materials may require a greater thickness of insulating panels [38].

The importance of thermal performance in building envelopes is well-recognized for its impact on energy efficiency and occupant comfort. Traditional insulation materials often fail to provide adequate thermal regulation, especially in warmer climates.

While numerous studies have explored the use of PCMs and bio-based materials individually for thermal regulation, there is a significant research gap exploring the synergistic effects of combining these materials to maximize their benefits.

This article addresses this gap by investigating the potential benefits of combining PCMs with bio-based insulation materials, specifically Wood Wool (WW) and Hemp Wool (HW), in building envelopes to enhance thermal performance. By exploring the latent heat storage capabilities of PCMs and the natural insulating properties of bio-based materials, this research aims to develop sustainable and efficient insulation solutions.

This study's novelty lies in the experimental and numerical analysis of these composite materials, providing valuable insights into their thermal behavior and practical applications. The research subjects the wall to a sinusoidal outside temperature, simulating typical summer day weather in Morocco, through experimental analysis using the heat flow method and numerical simulations using ANSYS Fluent software. The study provides insights into the dynamic thermal distribution within the insulation wall, with thorough assessment of the thermal performance and fluid mechanical aspects associated with the transition phase change of the different scenarios to determine indoor temperature reduction and heat transfer decrease.

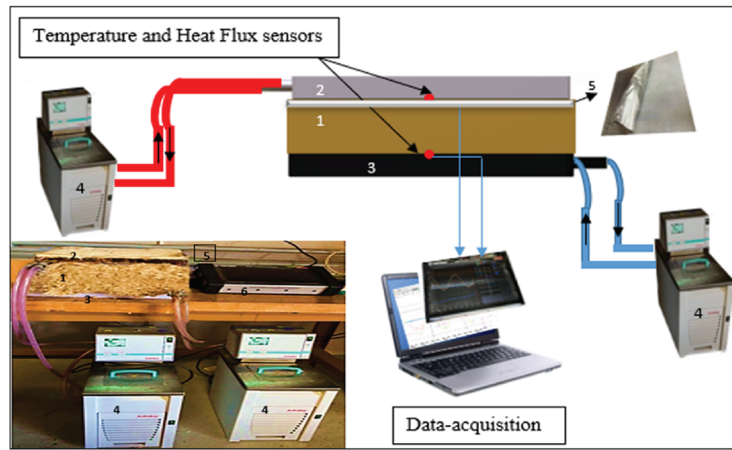
## 2 Materials and Methods

The Heat Flow Method (HFM) [39] experimental study investigates two different external wall insulation configurations using HW as the main material for its numerous advantages and thermal properties. The study also explores the impact of adding PCM on temperature variation to take advantage of its thermal storage capacity for regulating internal temperature.

HW, with its low thermal conductivity, helps limit heat transmission through walls, ultimately reducing the need for heating and cooling and lowering energy costs. PCM materials have the ability to store and release large amounts of heat energy by transitioning between solid and liquid phases. The study will analyze the thermal properties of HW and the effects of PCM integration, aiming to enhance insulation designs and optimize the thermal performance of buildings.

### 2.1 Experiment Model

The experiments focused on the thermal distribution within the external insulation wall. The heat flow method was utilized by placing the sample between two isothermal aluminum heat exchange plates connected to thermostatically controlled water baths [40], as illustrated in Fig. 1.



**Figure 1:** Experimental setup of HFM. 1: Insulation sample, 2: Isothermal heat exchange plate  $T_{out}$ , 3: Isothermal heat exchange plate  $T_{in}$ , 4: Thermostatically-controlled water baths, 5: PCM layer, 6: Data acquisition system DAS220/240, Seframviewer 3.6

The thermal response of the wall with and without the PCM layer was examined by collecting temperature measurements ( $T_{up} = T_{out}$ ,  $T_{low} = T_{in}$ ) using type K thermocouples on the underside, placed between the layers of PCM and biobased insulation, as well as on the top face and underside of the sample.

The heat flux is monitored by HFS sensors with dimensions of  $50 \times 50 \times 0.5 \text{ mm}^3$ ; on the upside and underside of the sample.

In Case 1 of the experiment, the sample consisted of HW ( $30 \times 30 \times 7 \text{ cm}^3$ ). In Case 2, a layer of PCM ( $30 \times 30 \times 1 \text{ cm}^3$ ) was added on top of the HW sample, resulting in a total dimension of ( $30 \times 30 \times 8 \text{ cm}^3$ ).

The upper part of the specimen underwent temperature variations ranging from  $20^\circ\text{C}$  to  $40^\circ\text{C}$  over time, following a sinusoidal pattern described in Eq. (8), while the temperature of the lower part remained constant at  $22^\circ\text{C}$  throughout the experiment. Data was collected at 60 s intervals over a 24 h period.

### 2.2 Computational Model

The distribution of temperature in a wall due to heat transfer by conduction in a transient regime is determined by the heat equation, also known as the thermal diffusion equation. This equation illustrates how temperature changes over time and space based on the thermal properties of the material. The simplified form of the basic linear heat Eq. (1), according to Fourier's law, is typically written as:

$$\frac{\partial^2 T(x, t)}{\partial x^2} = \frac{1}{a} \frac{\partial T}{\partial t} \quad (1)$$

$$\text{With } a = \frac{\lambda}{\rho C_p} \quad (2)$$

where the  $a$  is the thermal diffusivity of the material ( $\text{m}^2/\text{s}$ ).  $T(x, t)$  is the measured temperature (K);  $\lambda$  is the thermal conductivity ( $\text{W}/\text{m.K}$ ),  $\rho$  is the density of the considered material ( $\text{kg}/\text{m}^3$ ), and  $C_p$  is the specific heat capacity ( $\text{J}/\text{kg.K}$ ).

In the case of phase change material (PCM), such as melting/solidification phenomena, additional considerations and equations may be required:

The heat equation with convection become:

$$\frac{\partial T}{\partial t} + u \cdot \nabla T = \alpha \nabla^2 T \quad (3)$$

where  $u$  is the velocity vector of the fluid. If the dynamic field is concerned, additional melting/solidification model can be added, using well known models as Darcy law and other approximations to take into account the fluid flowing only in the liquid zone.

**Table 1:** Thermophysical material characteristics

	PCM [41]	Wood-Wool [42]	Hemp-Wool [43]
Density ( $\text{kg}/\text{m}^3$ )	810	50	40
Thermal conductivity for solid phase $\text{W}/(\text{m.K})$	0.18	0.046	0.04
Thermal conductivity for liquid phase $\text{W}/(\text{m.K})$	0.14	–	–
Specific heat capacity for solid phase ( $\text{kJ}/\text{kg.K}$ )	4	2.1	1.8
Specific heat capacity for liquid phase ( $\text{kJ}/\text{kg.K}$ )	3.8	–	–
Latent heat ( $\text{kJ}/\text{kg}$ )	136.2	–	–
Melting point ( $^{\circ}\text{C}$ )	28		
Freezing point ( $^{\circ}\text{C}$ )	10	–	–

### 3 Numerical Methodology

The simulation was conducted using ANSYS Fluent student version 2023 R2 software [44], allowing to analyze the temperature, velocity, liquid fraction and heat flux within PCM + (HW and WW) during phase change processes.

To model the temperature distribution using the heat Eq. (1), numerical methods, and assumptions about the wall material subjected to transient unidirectional heat transfer were taken into account [45,46].

The simulation of fluid flow and heat transfer in PCMs involves solving the Navier-Stokes equations Eq. (5) for fluid motion, coupled with the energy equation for heat transfer. Here, we consider the Boussinesq approximation for natural convection, which assumes that density variations are significant only in the buoyancy term.

The continuity, momentum, and energy equations for an incompressible fluid with phase change are as follows:

Continuity Equation:

$$\nabla \cdot u = 0 \quad (4)$$

Momentum Equation (Navier-stokes):

$$\frac{\partial u}{\partial t} + (u \cdot \nabla)u = -\frac{1}{\rho} \cdot \nabla P + \nu \nabla^2 u + g \quad (5)$$

where  $P$  is the pressure,  $\nu$  is the kinematic viscosity and  $g$  is the gravity.

To model the phase change, the enthalpy-porosity technique is often used. In this method, the liquid fraction  $f_s$  is determined based on the temperature field:

Energy Equation with phase change:

$$\frac{\partial T}{\partial t} + u \cdot \nabla T = \alpha \nabla^2 T + \frac{L}{C_p} \frac{\partial f_s}{\partial t} \quad (6)$$

$$f_s = \begin{cases} 0; & T \leq T_s \\ \frac{T - T_s}{T_l - T_s}; & T_s \leq T \leq T_l \\ 1; & T \geq T_l \end{cases} \quad (7)$$

where  $T_s$  and  $T_l$  are the solidus and liquidus temperatures, respectively.

Heat transfer analysis of the wall envelope was simulated by the user-defined function (UDF) representing outdoor temperature variation on a typical summer day, modeled as a sinusoidal temperature oscillation.  $T_{out}(t)$  Eq. (8), ranging from 20°C to 40°C. Using the same thermal properties as the thermal insulation materials detailed in Table 1.

$$T_{out}(t) = 303 + 10 * \sin(\omega t) \quad (8)$$

Here  $t$  is the time, and  $\omega = 2\pi/\tau$ , where  $\tau$  is the 24 h period.

The temperature evolution  $T(x, t)$  in the model was studied under certain assumptions [47]. These assumptions include considering laminar flow, neglecting radiation effects due to slow temperature changes, assuming adiabatic horizontal walls, and considering walls to be homogeneous and isotropic. In addition, the model assumes that the thermal properties of the material are constant in space and time and that there are no internal heat sources. These assumptions provide a simplified framework for understanding the temperature distribution within the system.

Boundary conditions for this case require a specific value to be specified, with both the external wall and inner wall having a Dirichlet condition as the type of boundary condition imposed.

### **Boundary conditions**

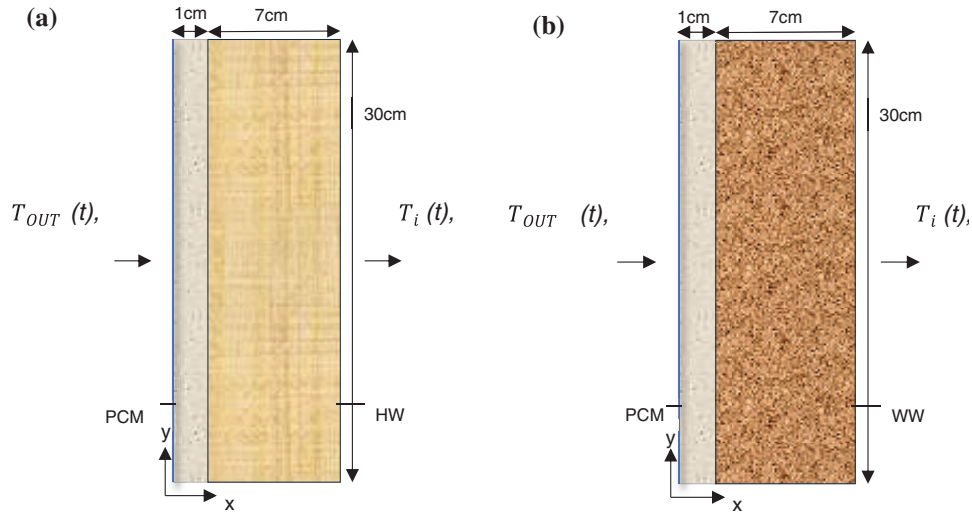
The bottom and top of the insulation wall are adiabatic:

$$-\lambda \frac{\partial T}{\partial y} = 0 \quad (9)$$

The temperature at  $x = 0$  is  $T(0, t) = T_{out}$ , and the temperature at  $x = e$  is set to 295.96 K.

The finite element method (FME) is used to solve these equations with ANSYS Fluent by discretizing the heat equations and solving them numerically on a mesh of the wall to determine the temperature distribution.

Geometric modeling was performed using the Design Modeler tool in ANSYS software. The study considered four different wall scenarios, as shown in Fig. 2. A quadratic mesh was then generated, comprising 40,000 elements for PCM/HW and PCM/WW, and 35,000 elements for HW or WW.



**Figure 2:** The schematic heat transfer of the insulation wall: (a) PCM + HW, (b) PCM + WW

Simulations were solved using a pressure-based and transient solver configured with implicit pressure and coupled operator splitting, along with a second-order upwind scheme.

Running the simulation allowed for calculating the temperature distribution across the walls and plotting the temperature evolution inside the wall over a 24 h period to analyze heat transfer through the wall.

## 4 Results and Discussion

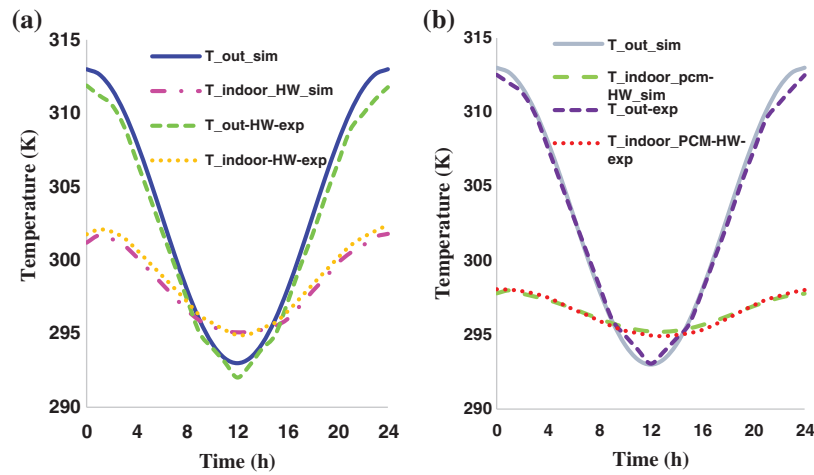
### 4.1 Model Validation

In the present study, simulation results were compared with experimental data for validation purposes, using two plates with imposed temperatures, one simulating outdoor conditions and the other indoor conditions. The test involved an envelope containing a 7-cm-thick layer of HW (Case 1). Subsequently, a multi-layer envelope was examined, consisting of a 1 cm layer of PCM added to the HW (Case 2). The dimensions of these configurations were  $30 \times 30 \times 7 \text{ cm}^3$  and  $30 \times 30 \times 8 \text{ cm}^3$ , respectively.

Fig. 3 depicts the measured temperature *vs.* time for HW and PCM\_HW on the top ( $x = 0$ ) and bottom ( $x = e$ ) surfaces of the sample in comparison with simulation results, where  $x = 0$  represents outdoor conditions and  $x = e$  represents indoor temperature. To validate the simulated results, the average error (AE) was calculated using Eq. (10):

$$\text{Average error (\%)} = \sum_{1, 2, \dots, N} \left[ \left\{ \left| \left( \frac{T_{\text{exp}} - T_{\text{sim}}}{T_{\text{exp}}} \right) \right| * 100 \right\} / N \right] \quad (10)$$

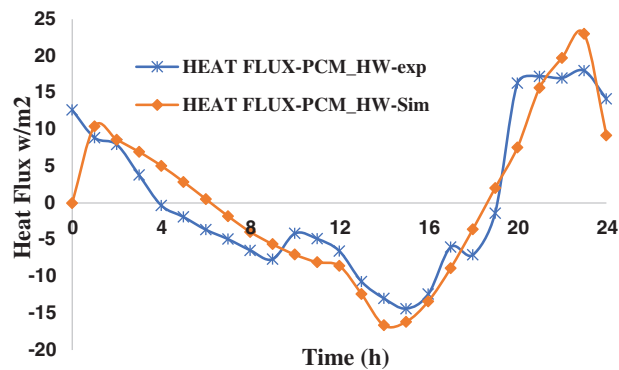
The average error of the numerical model is 0.14% in the first case and 0.06% in the second case. The small discrepancies between the experimental and numerical results may be attributed to the infiltration of free air into the HW layers. These low relative errors demonstrate the accuracy of the numerical model compared to the experiment, affirming its validity and reliability for further studies.



**Figure 3:** Comparison between the simulated and experimental temperature results for (a) HW and (b) HW with PCM

A 24 h test was conducted on a typical summer day using a reference insulating wall made of WW (Case 3). Subsequently, a similar test was performed by adding a layer of PCM (Case 4). Both tests were carried out utilizing ANSYS Fluent and adhering to the same numerical methodology outlined previously.

Fig. 4 compares the experimental and simulated heat fluxes for PCM + HW over 24 h period. Both data sets show similar profiles, with an initial peak (initial phase change), followed by a significant decrease with negative flux (liquid to solid), and then a rise towards the end (heat absorption). Some differences amplitude and timing are observed between the experimental and simulated results. These discrepancies could be attributed to various factors, such as simplifications in the simulation model, experimental measurement errors, or inherent material property variations.

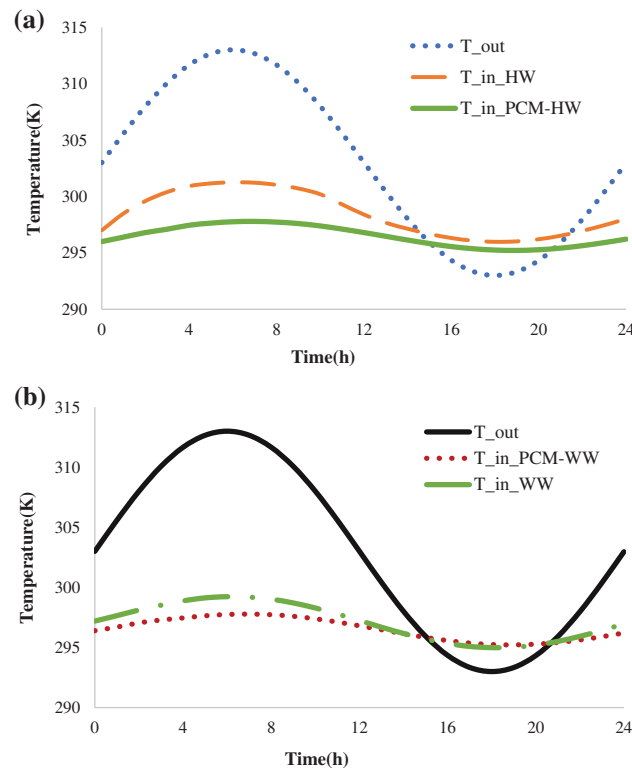


**Figure 4:** Comparison of experimental and simulated heat flux in PCM + HW composite over time

#### 4.2 Thermal Performance

Thermal performance was evaluated in this study by comparing the interior thermal characteristics, such as thermal amplitude, time lag, and decrement factor [48], for walls made of eco-materials (HW and WW) with and without a PCM layer. The graphs presented in Fig. 5. illustrate the impact of incorporating PCM into HW (a) and WW (b) walls insulation on the surface temperature. The results show that the addition of PCM layers help in reducing internal temperature variations and providing a more stable indoor surface temperature profile compared to HW and WW alone.





**Figure 5:** The impact of incorporating PCM into the HW (a) and WW (b) insulating wall on surface temperature

The thermal amplitude of PCM\_HW is 2.79 in comparison to HW 6.7, with a 58.36% reduction, and 2.56 for PCM\_WW in comparison to WW 4.25, with a 39.62% reduction.

The lag time for PCM\_HW and PCM\_WW is 1 h relative to the external environment, indicating that the addition of PCM helps to minimize overheating hours. The decrement factor for PCM\_HW and PCM\_WW was calculated to be 0.14 and 0.13, respectively, using the formula provided by Jin et al. [49]. The determination of the decrement factor is largely dependent on thermophysical properties and wall thickness [50]. A lower decrement factor indicates a higher level of indoor thermal comfort.

Fig. 6 illustrates the distribution of surface temperatures for different types of walls insulation: HW, WW, PCM + WW, and PCM + HW.

Walls with PCM layers (Cases 2 and 4) have a more uniform temperature distribution and lower temperatures, especially on the indoor side, as indicated by the blue areas in the contours. This highlights the effectiveness of adding PCM layers in enhancing the thermal regulation of wall insulations.

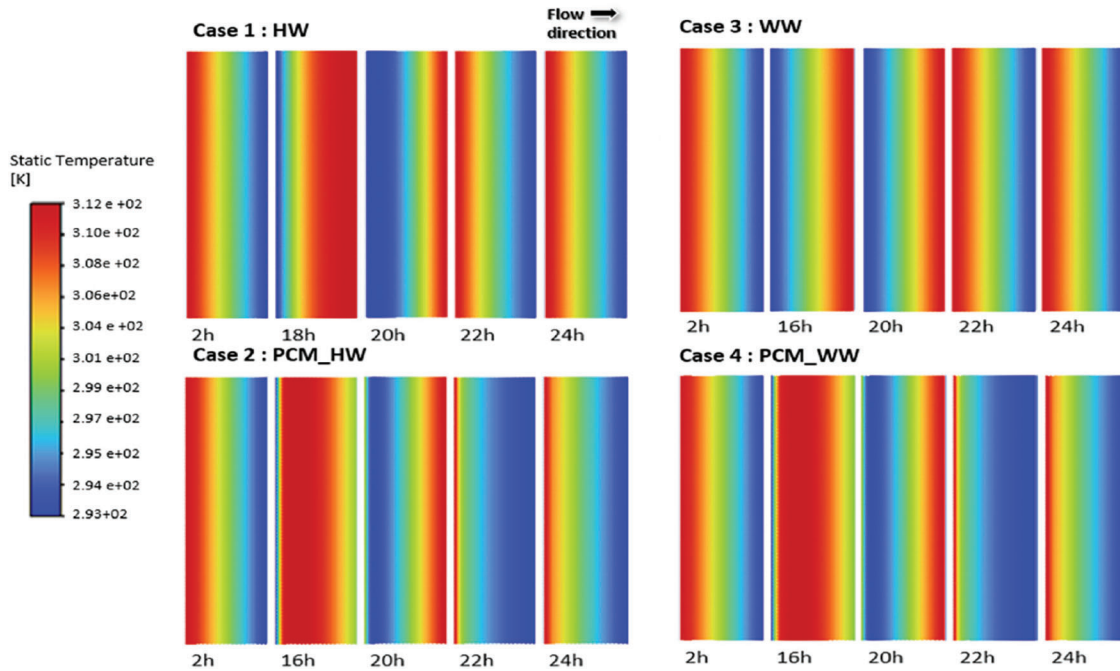
### 4.3 Fluid-Mechanical Aspect in Phase Change Materials

In this section, the fluid-mechanical properties of phase change material (PCM) used in conjunction with HW and WW are analyzed. Specifically, the velocity, liquid fraction, and heat flux within the PCM composites. These aspects are considered crucial for evaluating the thermal insulation performance and efficiency of PCM-based materials in various applications.

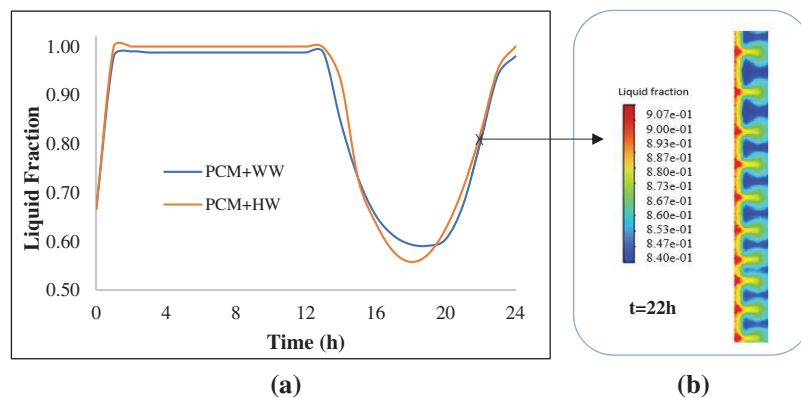
#### 4.3.1 Liquid Fraction Evolution

The liquid fraction allows visualizing the evolution of the liquid fraction in the phase change material (PCM), as shown in Fig. 7. The curves indicate similar melting and solidification cycles for PCM, with a

slight phase advance for PCM + HW compared to PCM + WW. The right visualization illustrates the contour of the liquid fraction distribution at  $t = 22$  h for both composite walls, where it's clearly shown the presence of wavy colors in the distribution suggesting natural convection effects within the PCM.



**Figure 6:** Temperature distribution within the wall insulation; Case 1: HW, Case 2: PCM\_HW, Case 3: WW and Case 4: PCM\_WW



**Figure 7:** (a) Liquid fraction distribution in PCM for PCM + HW and PCM + WW Composites (b) Liquid fraction distribution in the PCM part of the composite at  $t = 22$  h

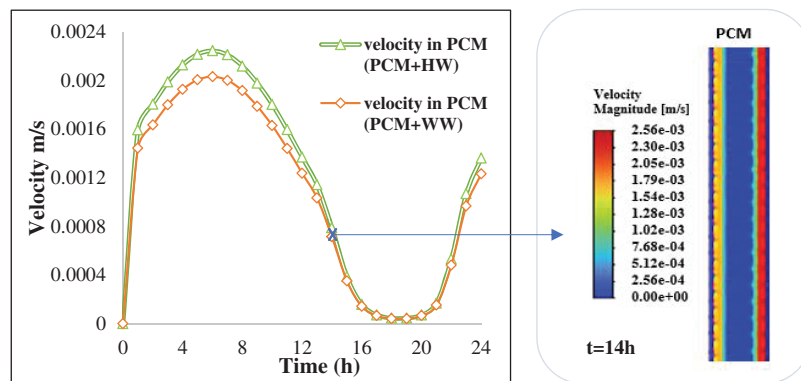
The faster progression towards a complete liquid state for PCM + HW can be attributed to the distinct thermal properties of HW and WW. Hemp wool's lower thermal conductivity ( $0.04 \text{ W/m.K}$ ) compared to Wood wool ( $0.046 \text{ W/m.K}$ ) results in less heat being conducted away from the PCM layer, allowing for more rapid melting. During the liquid phase, natural convection within the PCM helps in distributing the absorbed heat more uniformly across the wall. This phenomenon prevents localized overheating and contributes to a more uniform temperature across the external wall insulation.

Thus the incorporation of PCM in building materials, as observed in the studies by Mahdaoui et al. [51] and Hamdaoui et al. [52], significantly improves thermal performance by promoting balanced heat distribution and a more controlled phase transition.

#### 4.3.2 Velocity

Analyzing the velocity field helps study the natural convection effects within the molten PCM.

The graph in Fig. 8 shows the velocity distribution in PCM for both PCM + HW and PCM + WW composites over a 24 h period. The velocity curves for both composites are similar, with PCM + HW showing slightly higher velocities between 2 and 12 h.



**Figure 8:** Velocity distribution in PCM for PCM + HW and PCM + WW composites

Since the profile contour of velocity for both composites are similar, the velocity magnitude visualization at 14 h (right side of the figure) shows higher velocities near the edges of the PCM layer, suggesting the presence of convection currents within the melted PCM. This natural convection plays a crucial role in heat distribution within the composites.

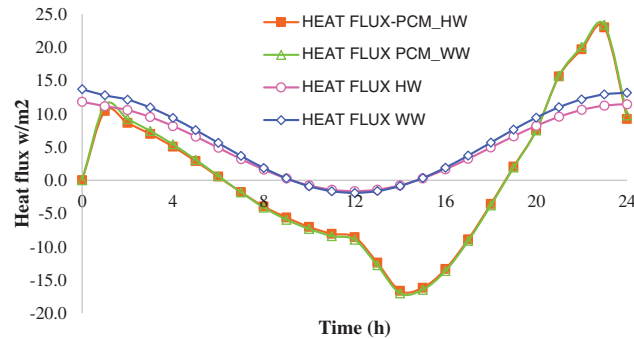
Due to the temperature gradients causing density differences in the molten PCM, higher velocities were noticed near the edges indicating the formation of boundary layers, where buoyancy-driven flow is strongest. This behavior aligns with studies on PCM in similar configurations. Soliman et al. [53] Observed comparable convection effects in their simulations of PCM confined in cylindrical enclosures under constant heat flux. However, adding bio-based materials (HW and WW) could improve heat storage and release by slightly enhancing convective movements without creating major imbalances. As described by Cheng et al. [54], enhancing the thermal conductivity of stabilized PCM can optimize underfloor heating systems, which could be similar to the effect observed with HW and WW.

#### 4.3.3 Heat Flux

Heat flux is a key parameter for evaluating the thermal performance of insulation materials.

Fig. 9 demonstrates the impact of integrating PCM on heat flux. The curves for the two composites with PCM + HW and PCM + WW are quite similar, suggesting that the PCM dominates the thermal behavior of the composite. The PCM composites show a period of significant heat absorption (negative flux), followed by a period of heat release (positive flux). This can be attributed to the high latent heat of the PCM allowing to absorb a significant amount of thermal energy during phase change and release it later. Achieving an average reduction of the heat transfer rate of 95.82% compared to WW without PCM and a decrease of 95,65% compared to HW without PCM. The results demonstrate the enhanced thermal management capabilities of PCM incorporated to biobased insulation materials. The studies by Bouzennada et al. [55] and Babaharra et al. [56] highlighted the importance of managing heat flux in PCM applications, claiming

that well-controlled heat flux improves the thermal storage capacity; the results of this study support these conclusions.



**Figure 9:** Comparison of heat flux in HW and WW insulation materials with and without PCM

## 5 Conclusion

This study asserts the significant potential of the combination PCM and biobased insulation materials to enhance the thermal performance of building envelopes.

The combination of phase change material (PCM) with biobased insulation materials resulted in significant reductions in temperature oscillations within walls. PCM\_HW exhibited a temperature decrease of 3.8 K, while PCM\_WW showed a reduction of 1.45 K compared to their respective reference wall insulation without PCM.

PCM composites demonstrated superior thermal management capabilities. The addition of PCM to both Hemp Wool and Wood Wool significantly improved their effectiveness as thermal insulation materials, providing more stable indoor temperatures. This enhancement in thermal stability contributes to improved occupant comfort and reduced energy needs for heating and cooling.

Regarding heat flux, the addition of PCMs resulted in a significant reduction in heat transfer rates. An average decrease of 96% for PCM + (HW, WW) compared to HW and WW without PCM.

The homogeneous distribution of the liquid fraction within the PCM layer and moderate velocities indicate efficient thermal energy storage and release process, which is crucial for maintaining consistent thermal performance in sustainable building applications and contribute to the effectiveness of the composite insulation system.

Future research will explore the hygrothermal performances of these materials, examining how PCM integration affects moisture management and thermal behavior over extended periods. Moreover, exploring the wider impact of PCM usage on sustainable construction and environmental management will provide valuable insights into their role in ecofriendly building solutions.

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**Author Contributions:** The authors confirm contribution to the paper as follows: conception and design: Salma Kouzzi; data collection: Salma Kouzzi; simulation: Salma Kouzzi, Mouniba Redah; analysis and interpretation of results: Salma Kouzzi, Souad Morsli; draft manuscript preparation: Salma Kouzzi, Mouniba Redah; writing: Salma Kouzzi, Souad Morsli, Mouniba Redah; review and editing: Salma Kouzzi, Mohammed El Ganaoui, Souad Morsli; supervision and administration: Mohammed El Ganaoui,

Mohammed Lhassane Lahlaoui. All authors reviewed the results and approved the final version of the manuscript.

**Availability of Data and Materials:** The datasets generated during and/or analyzed during the current study are available from the corresponding author on reasonable request.

**Ethics Approval:** Not applicable.

**Conflicts of Interest:** The authors declare that they have no conflicts of interest to report regarding the present study.

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