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Energy Optimization Strategy for Reconfigurable Distribution Network with High Renewable Penetration Based on Bald Eagle Search Algorithm

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ABSTRACT: This paper proposes a cost-optimal energy management strategy for reconfigurable distribution networks with high penetration of renewable generation. The proposed strategy accounts for renewable generation costs, maintenance and operating expenses of energy storage systems, diesel generator operational costs, typical daily load profiles, and power balance constraints. A penalty term for power backflow is incorporated into the objective function to discourage undesirable reverse flows. The Bald Eagle Search (BES) meta-heuristic is adopted to solve the resulting constrained optimization problem. Numerical simulations under multiple load scenarios demonstrate that the proposed method effectively reduces operating cost while preventing power backflow and maintaining secure operation of the distribution network.

KEYWORDS: Reconfigurable distribution networks; energy optimization management; bald eagle search algorithm

1 Introduction

The widespread application of new energy generation can effectively alleviate the problem of carbon emissions [1]. As renewable penetration increases, distribution networks must accommodate bidirectional power flows and more variable operating conditions, which complicates system control and reliability. As a result, the operation of the distribution network—and even the entire power system—is undergoing significant transformation. In this context, reconfigurable distribution networks are not only required to supply electricity to user loads, but also to accommodate and distribute power from distributed energy resources. Variations in the proportion and generation patterns of distributed generation make the direction of power flow uncertain, significantly increasing the complexity of operating and regulating reconfigurable distribution networks [2,3]. Meanwhile, current non-interruptible power supply technologies based on mobile generators and energy storage vehicles are insufficient to address issues such as power backflow that may arise in high renewable penetration distribution networks. However, the uncertainty of distributed generation and variable load profiles presents significant optimization challenges.

To address these challenges, researchers have proposed numerous optimization and energy management approaches. Reference [4] investigated the energy allocation problem in smart homes and microgrids with high penetration of renewable energy. By taking into account load demand, generation uncertainty, and market price fluctuations, a two-stage model was developed to achieve optimized energy scheduling; Reference [5] employed particle swarm optimization to optimize each artificial neural network and integrated it into an adaptive energy management system, with simulation results demonstrating improved microgrid performance. Reference [6] applied the slime mold algorithm, combined with the weighted



sum technique and fuzzy clustering, to optimize the operating costs and active losses of distributed generators in the distribution network, and its performance was validated against various other optimization algorithms. Reference [7] proposed a dynamic weight distributed algorithm based on primal-dual methods for comprehensive energy allocation, offering greater flexibility, reliability, and adaptability compared to traditional centralized algorithms. Reference [8] introduced a binary particle swarm optimization algorithm with an acceleration coefficient, aimed at minimizing losses in distribution network systems, and evaluated its convergence speed under different operating conditions. Reference [9] developed an enhanced whale optimization algorithm under the security constraints of reconfigurable distribution networks, which improved global convergence speed. Reference [10] presented a distributed, market-assisted restoration strategy for multi-energy distribution systems, integrating energy trading mechanisms with the system restoration process, and achieving efficient recovery and operation of electricity, heat, and gas systems through multi-agent collaborative optimization. The following Table 1 summarizes the differences between different optimization algorithms.

Method	Search capability	Convergence speed	Key features & advantages
Bald Eagle Search (BES)	Strong	Fast	Simulates eagle hunting behavior balancing exploration and exploitation; well-suited for real-time power regulation
Genetic Algorithm (GA)	Strong	Moderate	Based on natural selection and genetics; adaptable but prone to local optima
Particle Swarm Optimization (PSO)	Moderate	Fast	Simple to implement; fast convergence but prone to premature convergence
Ant Colony Optimization (ACO)	Moderate	Slow	Suitable for path optimization but computationally intensive

Table 1: Comparison of different optimization algorithms

Given the Bald Eagle Search (BES) algorithm's strong capability in handling complex nonlinear optimization problems and its fast convergence speed, it is particularly well-suited for the dynamic and multiconstrained nature of energy management in reconfigurable distribution networks. These characteristics enable BES to effectively balance exploration and exploitation, thereby enhancing solution quality while avoiding premature convergence. Accordingly, this study employs BES as the core optimization tool to achieve cost-optimal energy management while preventing power backflow.

This paper formulates an energy optimization framework for an reconfigurable distribution network that integrates incorporating photovoltaic (PV), wind, diesel generators, and electrochemical energy storage. The principal contributions are:

- (1) Development of mathematical models for PV and wind generation that capture key operational characteristics;
- (2) Construction of a practical state-of-charge (SOC) model for storage units representative of lead-acid battery behavior;
- (3) Incorporation of a power backflow penalty into the operating cost objective to mitigate reverse flows in high-penetration scenarios;

(4) Application of the Bald Eagle Search algorithm to obtain cost-optimal dispatch while satisfying technical constraints;

(5) Extensive simulation studies under residential and industrial load scenarios that validate the effectiveness of the proposed approach.

2 Mathematical Models of Different Parts in the Reconfigurable Distribution Network

The prerequisite for optimizing the energy of the reconfigurable distribution network is to clarify the power output, consumption, and storage components within the system. Therefore, the first step is to establish a corresponding mathematical model.

2.1 Mathematical Model of Wind Turbine

Wind turbines are the primary means of harnessing wind energy, capturing it through rotating blades and converting it into electrical power. According to Betz' theory, the maximum extractable energy from a wind turbine can be expressed as follows [11]:

$$\begin{cases} P_{m} = \frac{1}{2} \rho \pi R^{2} v^{3} C_{p} (\lambda, \beta) \\ \lambda = \frac{\omega_{m} R}{v} \end{cases}$$
 (1)

In the formula, P_m represents the mechanical output power of the wind turbine (W); ρ represents the density of air (kg/m³); R denotes the radius of the wind turbine blades (m); ν is the wind speed (m/s); ω_m represents the mechanical angular velocity of the wind turbine (rad/s); C_p is the wind energy utilization coefficient influenced by the blade tip speed ratio λ and pitch angle β . According to the Betz' limit, the maximum possible value of C_p is 0.593. The output characteristics of wind turbines can be described by the following mathematical model:

$$P_{wt}^{t} = \begin{cases} 0 & 0 \le v(t) \le v_{ci} \\ P_{wt,r} \frac{v(t)^{3} - v_{ci}^{3}}{v_{n}^{3} - v_{ci}^{3}} & v_{ci} \le v(t) \le v_{n} \\ P_{wt,r} & v_{n} \le v(t) \le v_{co} \\ 0 & v_{co} \le v(t) \end{cases}$$
(2)

In the above equation, P_{wt}^t represents the wind turbine output power at time t; $P_{wt,r}$ denotes the rated power, which is determined by the rated wind speed v_n ; v(t) is the Wind speed passing through the blades at time t; v_{ci} and v_{co} are the cut-in and cut-out wind speeds, respectively.

It can be observed that the output power of wind turbines is influenced by both the wind speed ν and the power coefficient C_p at time t. Among these, C_p can be flexibly regulated through the mechanical angular velocity ω_m of the generator, with a theoretical range of (0, 0.593) as defined by Betz's limit. In this model, the maximum value of C_p is first calculated based on the current wind speed to determine the output power of the wind turbine as the upper limit for energy management. Subsequently, C_p is adjusted dynamically according to actual demand to adjust the output power.

A wind power output model is then established using the average wind speed profile from a specific wind farm. The daily wind speed variation is illustrated in Fig. 1. A 24-s simulation was conducted to represent 24 h of real-time operation.

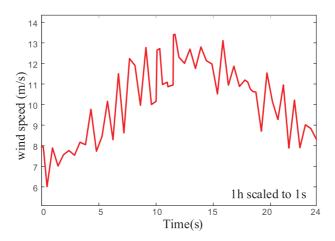


Figure 1: Daily wind speed curve

The simulation parameter settings for wind turbines are shown in Table 2 wind power generation simulation parameters.

Table 2: Wind power generation simulation parameters

Parameters	Value	Parameters	Value
R (m)	15.2	$P_{m \max}$ (kW)	120
v_n (m/s)	12	v_{ci} (m/s)	3
v_{co} (m/s)	15	ρ (kg/m ³)	1.29

The output curve of the wind turbine model obtained through simulation is shown in Fig. 2.

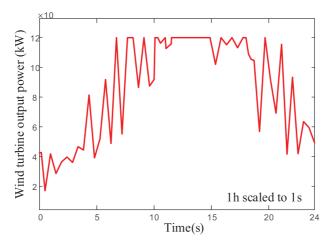


Figure 2: Maximum output power of wind turbines at different wind speeds

2.2 Mathematical Model of Photovoltaic Power Generation

Photovoltaic power generation converts solar energy directly into electrical power. The output power of a photovoltaic power generation unit can be expressed by the following equation [12].

$$P_{pv}^{t} = f_{pv}P_{pv,r}\frac{G(t)}{G_{s}}\left[1 + \kappa\left(T_{pv}(t) - T_{s}\right)\right]$$
(3)

In the formula, P_{pv}^t represents the photovoltaic output power at time t (kW); f_{pv} is the power derating factor of the photovoltaic power generation unit, which accounts for losses due to surface dust, rain and snow coverage, and natural aging, typically taken as 0.9; $P_{pv,r}$ is the rated power of the photovoltaic power generation unit (kW); G(t) denotes the solar irradiance received by the inclined surface at time t (kW/m²); G_s is the standard test condition irradiance, usually taken as 1; κ is the power temperature coefficient (%/°C), commonly taken as -0.47; $T_{pv}(t)$ is the surface temperature of the photovoltaic array at time t (°C); T_s is the array surface temperature under standard testing conditions, usually taken as 25°C.

The actual output power of photovoltaic generation is primarily influenced by solar irradiance [13], which typically follows a smooth, bell-shaped curve—gradually increasing to a peak and then declining. The irradiance received by the photovoltaic array at time t can be expressed by the following equation:

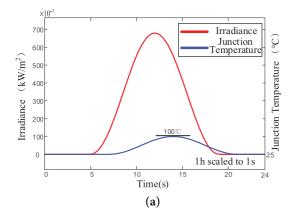
$$G_{t}(t) = \begin{cases} 0 & t < t_{p1} \\ \frac{G_{\text{max}}}{2} \left\{ 1 - \cos \left[2\pi \left(\frac{t - t_{p1}}{T_{pg}} \right) \right] \right\} & t_{p1} \le t \le t_{p1} + T_{pg} \\ 0 & t > t_{p1} + T_{pg} \end{cases}$$

$$(4)$$

where G_{max} is the maximum irradiance (kW/m²); t_{p1} is the sunrise time (h); T_{pg} is the duration of sunshine (h). According to Eq. (3), another key factor affecting the output of photovoltaic systems is the surface temperature of the photovoltaic unit during operation, which is primarily affected by solar irradiance. In summer, the rear surface temperature of photovoltaic modules can reach up to 70°C, while the working junction temperature can climb as high as 100° C. Typically, the highest temperature during the day occurs approximately two hours after the peak irradiance, so there is a relationship between T_{pv} and G(t) as follows:

$$T_{pv}(t) = k_T G_t(t) (24 + t - t_s)$$
(5)

where k_T is the temperature coefficient and t_s is the delay time, taken as 2 h. Taking t_{p1} as 5 h, G_{max} as 680 kW/m², and T_{pg} as 14 h, Then the following simulation results were obtained in Fig. 3.



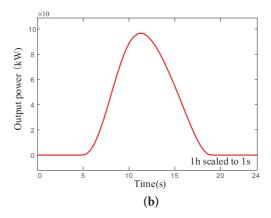


Figure 3: Photovoltaic power generation simulation curve. (a) Irradiance and junction temperature curves; (b) Daily output power curve of photovoltaic power generation

After obtaining the above two parameters, the photovoltaic power generation model can be constructed using Eq. (3), with a rated power of $P_{pv,r}$ set to 200 kW, and the above Fig. 3b photovoltaic power generation output curve can be obtained.

2.3 Mathematical Model of Diesel Generator

Emergency power supply vehicles are vital for fault repair and maintenance in reconfigurable distribution networks. Their core power supply unit is a diesel generator, which generally consists of a diesel engine, a synchronous generator, a fuel tank, and other parts [14]. Diesel generators are modeled in terms of fuel consumption vs. output power and generator dynamics. Fuel consumption is approximated by a linear/quadratic fuel curve characterized by intercept and slope coefficients [15]. The relationship between the actual output power P_{gen} of a diesel generator and the fuel consumption F is expressed as follows:

$$F = F_0 Y_{gen} + F_1 P_{gen} \tag{6}$$

In the formula, F_0 is the intercept coefficient of the fuel curve of the diesel generator (L/(kW·h)), typically set to 0.08415; F_1 is the slope of the fuel consumption curve for diesel generators (L/(kW·h)), which can be set to 0.246; Y_{gen} represents the rated power of the diesel generator (kW), set to 50 in this study. The diesel engine and generator are driven by a coaxial line, and there is inevitably a loss coefficient η during power transmission. Here, 0.95 is taken, and the following relationship exists:

$$P_e = \eta P_{gen} \tag{7}$$

where P_e is the synchronous generator output power. The synchronous generator is simplified and treated as a black box, where the input variables are the dq axis currents and the mechanical angular velocity, and the output is the electrical power P_e . Therefore, it is sufficient to establish a mathematical model that describes the power generation process. The following equation is the mathematical model of the output torque of a permanent magnet synchronous motor after coordinate transformation [16].

$$P_e = T_e \omega_m = \frac{3}{2} P_n \omega_m \left[\psi_f i_q + i_d i_q \left(L_q - L_d \right) \right] \tag{8}$$

where R_s is the stator resistance of the motor (Ω) ; i_{dq} is the stator current of the motor (A); ω_m is the mechanical angular velocity; ψ_f is the magnetic flux of a permanent magnet; L_{dq} represents the inductances along the direct and quadrature axes; P_n is the number of poles in the motor.

In the simulation, we adopt a simplified electromechanical model suitable for system-level optimization [17]. Given a fixed rated mechanical angular velocity, the stator current increases gradually to its rated value over time. The specific parameters of the motor used in the simulation are shown in Table 3.

Table 3: Main parameters of synchronous motor in diesel generator vehicles

Parameters	Value	Parameters	Value
ω_m (rad/s)	500	P_e (kW)	40
L_d (H)	0.0005	$i_{\max}(A)$	260
L_q (H)	0.0015	ψ_f (Wb)	0.1
P_n	2	-	

The following simulation curves were obtained, where Fig. 4a shows the current distribution curve and Fig. 4b shows the actual output power curve of the diesel generator. The maximum power of 40 kW was reached at 18 s during operation.

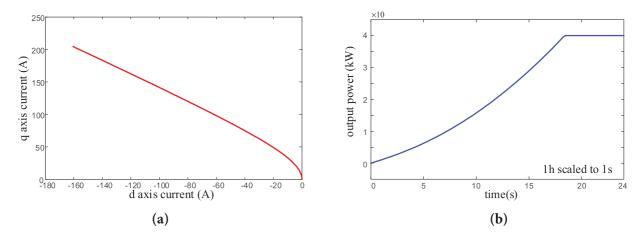


Figure 4: Simulation curve of diesel generator. (a) Current distribution curve; (b) Output power curve of diesel generator

2.4 Mathematical Model of Energy Storage Devices

Electrochemical energy storage, owing to its advantages of high energy density, rapid response capability, low maintenance costs, and operational flexibility, has emerged as the predominant direction for large-scale energy storage technologies. This study model electrochemical storage using a practical SOC update equation suitable for system-level optimization. The storage unit acts as an intermediate energy buffer; its SOC evolves according to charge/discharge power, efficiency, and self-discharge. The SOC of the battery is defined based on the charge/discharge current as follows [18].

$$SOC(t) = \frac{C_{re}(t)}{C_{bat}} = 1 - \frac{1}{C_{bat}} \int Idt$$
 (9)

In the above equation: $C_{re}(t)$ represents the remaining capacity of the battery at time t (A·h); C_{bat} is the total capacity of the battery (A·h); I is the working current of the battery (A). Accordingly, the SOC at time t and time t + 1 can be expressed.

$$\begin{cases}
SOC(t+1) = SOC(t) [1 - \sigma(t)] + \eta(t) \frac{I_{bat}(t)}{C_{bat}} \Delta t \\
I_{bat}(t) = \frac{P_{bat}(t)}{N_{bat}V_{bat}(t)}
\end{cases}$$
(10)

In the formula, $\sigma(t)$ represents the self-discharge rate. Due to the time scale contraction in the simulation study, one second was used to represent one hour. Therefore, a corresponding proportional transformation is applied, resulting in a value of 2.3148e-8; $\eta(t)$ is the charging and discharging efficiency at time t, generally ranging from 60% to 80%; $I_{bat}(t)$ is the charging and discharging current at time t (A); Δt is the discrete time interval; $P_{bat}(t)$ is the charging and discharging power of storage at time t; N_{bat} is the total number of battery series and parallel connections; $V_{bat}(t)$ is the battery terminal voltage at time t.

A black-box model is built based on Formula (10), with input of power P and the existing state of charge SOC(t), and output of remaining SOC(t) and charge discharge flag, with charge set to 1 and discharge set to

0. The structural diagram is shown in Fig. 5. The storage unit is modeled as an intermediate energy buffer for the purpose of system-level optimization, rather than detailed electrochemical modeling.

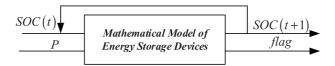


Figure 5: Energy storage black box model

Simulate the energy storage battery with the parameters shown in Table 4.

Parameters	Value	Parameters	Value
$\eta(t)$ (%)	70	C_{bat} (A·h)	5000
N_{bat}	6	$V_{bat}(t)(V)$	650
$\sigma(t)$ (%/day)	2.3148e-8	SOC(0) (%)	50
$SOC_{\min}(t)$ (%)	30	$SOC_{\max}(t)$ (%)	80

Table 4: Energy storage battery parameters

Due to the negligible self-discharge rate, it is omitted in this model. In the simulation, 24 s are used to represent 24 h, and accordingly, the total battery capacity is scaled down proportionally to 1.4 A·h. To simulate the operational behaviour of the energy storage system, the input power is randomly assigned positive and negative values, representing charging and discharging scenarios. As a result, the SOC profile shown in Fig. 6 is obtained.

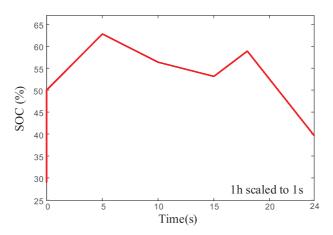


Figure 6: SOC simulation curve

3 Energy Optimization Strategy Based on Bald Eagle Search

The diversity of distributed power sources, together with variations in control characteristics, operating states, and costs, renders energy optimization in high-penetration reconfigurable distribution networks a complex, multi-constraint nonlinear programming problem [19]. To address this, the present study employs the Bald Eagle Search (BES) algorithm, a meta-heuristic optimization method, to achieve energy management optimization.

The entire system requires coordinated optimization of photovoltaic (PV) output, wind power output, and diesel generator output. Among them, wind power and diesel generator output are easy to adjust, while photovoltaic output is generally regarded as uncontrollable due to its dependence on solar irradiance. Consequently, wind power and diesel generators are treated as controllable assets to ensure overall power balance and cost-effective operation of the reconfigurable distribution network. The BES algorithm starts with population initialization, generating n bald eagles as candidate solutions. Each bald eagle carries two characteristic information P_i^w and P_i^g , which can be described using the following equation. Where P_i^w represents wind power output, P_i^g represents diesel generator output [20].

$$\boldsymbol{B}_{i} = \left[\begin{array}{cc} P_{i}^{w} & P_{i}^{g} \end{array} \right] \tag{11}$$

Based on the constraint conditions, randomly generate feature values according to the following formula.

$$P_i = \min + (\max - \min) \cdot \xi \tag{12}$$

Among them, P_i represents a specific characteristic of a bald eagle, while 'max' and 'min' denote the upper and lower bounds of this characteristic, respectively. ξ is a random number in the optimization algorithm, with a value range of [0,1], and is updated after each value is taken. The BES algorithm simulates different stages of bald eagle hunting: spatial selection, prey search, and hunting, and then iteratively obtains the optimal solution.

Selection stage: Bald eagles choose the best hunting space rich in prey, which is expressed as follows:

$$\boldsymbol{B}_{i,new} = \boldsymbol{B}_{best} + \alpha \times \xi \times (\boldsymbol{B}_{mean} - \boldsymbol{B}_i) \tag{13}$$

Among them, \mathbf{B}_{best} is the previously determined optimal search area; α is the control parameter, usually taken as 1.5~2.0; \mathbf{B}_{mean} is the average position of all bald eagles, which is the mean of their respective eigenvalues; \mathbf{B}_i is the original position of the *i*-th bald eagle; $\mathbf{B}_{i,new}$ is the current location of the *i*-th bald eagle after this update.

Search stage: Simulate a bald eagle discovering prey and use spiral acceleration search to determine the optimal hunting position. The position update is achieved through the following equation.

$$\boldsymbol{B}_{i,new} = \boldsymbol{B}_i + m(i) \times (\boldsymbol{B}_i - \boldsymbol{B}_{mean}) + n(i) \times (\boldsymbol{B}_i - \boldsymbol{B}_{i+1}) \tag{14}$$

$$\begin{cases}
 m(i) = \frac{mr(i)}{\max(|mr|)}; nr(i) = \cos[\theta(i)] \times r(i) \\
 mr(i) = r(i) \times \sin[\theta(i)]; r(i) = R \times 2 \cdot \xi + \theta(i) \\
 n(i) = \frac{nr(i)}{\max(|nr|)}; \theta(i) = a \times \pi \times 2 \cdot \xi
\end{cases}$$
(15)

where m(i) and n(i) represent the position of the i-th bald eagle; r(i) and $\theta(i)$ respectively describe the polar diameter and polar angle in the spiral path; a and R are parameters for determining the spiral path. Hunting stage: Based on the optimal position from the previous stage, accelerate and pounce on the prey, and update the formula as follows.

$$\boldsymbol{B}_{i,new} = \boldsymbol{\xi} \times \boldsymbol{B}_{best} + m_w(i) \times (\boldsymbol{B}_i - p_1 \times \boldsymbol{B}_{mean}) + n_w(i) \times (\boldsymbol{B}_i - p_2 \times \boldsymbol{B}_{i+1})$$
(16)

$$\begin{cases}
 m_{w}(i) = \frac{mr(i)}{\max(|mr|)}; nr(i) = r(i) \times \cosh[\theta(i)] \\
 mr(i) = r(i) \times \sinh[\theta(i)]; r(i) = \theta(i) \\
 n_{w}(i) = \frac{nr(i)}{\max(|qr|)}; \theta(i) = a \times \pi \times 2 \cdot \xi
\end{cases}$$
(17)

Among them, $m_w(i)$ and $n_w(i)$ represent prey coordinates, p_1 and p_2 represent motion parameters, usually taken as 2.

These three stages form the iterative process of the Bald Eagle Search algorithm. Each iteration will continuously retain the optimal feature values under the set goal until the expected goal is met or the number of iterations is reached to stop.

To better illustrate the effectiveness of the optimization algorithm in terms of search breadth and avoidance of local optima, the figure below presents the search areas covered by the vulture population during the search phase after 10 and 50 iterations. It can be seen from Fig. 7 that, irrespective of whether 10 or 50 iterations are performed, the vulture population follows a spiral trajectory while seeking the optimal solution. Even after only 10 iterations, a relatively high coverage of the search space is achieved. Moreover, as the number of iterations increases, the search density continues to rise and the overall search range expands. This indicates that the vulture optimization algorithm exhibits certain advantages in convergence speed and in avoiding local optima.

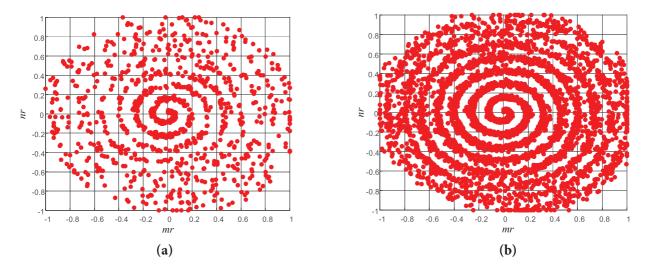


Figure 7: Distribution of bald eagle positions under different iteration times. (a) Results After 10 Iterations; (b) Results After 50 Iterations

4 Objective Function and Constraints

This paper considers renewable energy source such as solar, wind and power generation vehicles as the source of the reconfigurable distribution network, and regards energy storage systems as intermediate stations for energy transfer, with the goal of minimizing the operating costs of distributed resource output. Under the constraints of power generation operation and unit power balance, by reasonably arranging the output of distributed resources, the reconfigurable distribution network can achieve the lowest operating costs without experiencing power outages.

4.1 Objective Optimization Function

The energy optimization objective function is as follows.

$$\min C_{all} = \omega_1 \cdot \left(c_w \cdot \sum_{i=1}^d P_i^w + c_g \cdot \sum_{i=1}^q P_i^g + c_v \cdot \sum_{i=1}^s P_i^v \right) + \omega_2 \cdot c_s \cdot \left| \Delta P_{diff} \right|$$
 (18)

$$\Delta P_{diff} = P_{load} - \sum_{i=1}^{d} P_i^w - \sum_{i=1}^{q} P_i^g - \sum_{i=1}^{s} P_i^v$$
(19)

 C_{all} represents the total operating cost generated by each energy storage unit and power generation source within the reconfigurable distribution network; P_i^w denotes the output power of the *i*-th unit among a total of *d* wind power generation units, and c_w is its operating cost coefficient; P_i^g is the output power of the *i*-th unit in the total *q* generator units, c_g is its operating cost system; P_i^v is the output power of the *i*-th unit among a total of *s* photovoltaic power generation units, and c_v is its operating cost coefficient; ΔP_{diff} is the power difference, used to describe the additional cost generated by the energy storage system when the output of distributed resources is unequal to the load. It is obtained from Eq. (19), with c_s as its cost coefficient. This term is added to the objective function as a power backflow penalty, aiming to prevent the occurrence of power backflow in reconfigurable distribution networks. Therefore, a relatively large cost coefficient is assigned to this term; Additionally, ω_1 , ω_2 is a weight coefficient used to describe the importance of the relationship between distributed resource output and energy storage systems; P_{load} is the load power demand. All cost coefficients are expressed in units of 10,000 yuan/kW.

The cost coefficients c_w , c_g , and c_v of each source need to be defined, where c_w , as the cost coefficient of wind power generation, is related to the operating status of the wind turbine. Assuming a linear relationship between c_w and C_p , the specific expression is as follows:

$$c_w = \frac{k_1}{C_p + 0.25} \tag{20}$$

 C_p , as a key parameter for controlling the output power of wind power generation, will vary with changes in power during the energy optimization process, so c_w will also vary with changes in actual output power. The cost coefficient of c_g as a diesel generator vehicle is mainly reflected in the fuel cost of the diesel generator vehicle, which can be expressed in the form of a quadratic function as follows.

$$c_g = k_2 \left(\frac{P_g}{P_{gmax}}\right)^2 + k_3 \frac{P_g}{P_{gmax}} + k_4$$
 (21)

where P_g represents the output power of the permanent magnet synchronous motor, and $P_{g \max}$ is the maximum output power.

As an uncontrolled part, the cost coefficient c_v of photovoltaic output can be directly taken as a constant coefficient. The operating cost coefficient c_s of the energy storage system should be set to a relatively high value to prevent power backflow and insufficient output. The cost coefficients k_1 , k_2 , k_3 , and k_4 in Eqs. (20) and (21) can be taken as needed.

4.2 Constraints

(1) Power balance constraint

$$P_{load} = \sum_{i=1}^{d} P_i^w + \sum_{i=1}^{q} P_i^g + \sum_{i=1}^{s} P_i^v + \Delta P_{diff}$$
 (22)

All the power emitted by distributed resources plus the power absorbed by the energy storage system must match the load power demand and meet the power balance constraint.

(2) Wind power generation constraints

$$C_{p\min} \cdot \frac{P_{\max}^{w}}{C_{p\max}} \le P_i^{w} \le C_{p\max} \cdot \frac{P_{\max}^{w}}{C_{p\max}}$$
(23)

Among them, P_{max}^{w} represents the maximum output power of the wind turbine, which is taken as 120 kW. $C_{p \, \text{min}}$ represents the maximum value of wind energy utilization coefficient which is taken as 0.593. $C_{p \, \text{max}}$ represents the minimum wind energy utilization coefficient, which is taken as 0.

(3) Photovoltaic power generation constraints

$$0 \le P_i^{\nu} \le P_{\max}^{\nu} \tag{24}$$

Among them, P_{max}^{ν} represents the maximum output power of photovoltaic power generation, which is taken as 100 kW here.

(4) Photovoltaic power generation constraints

$$0 \le P_i^g \le P_{\max}^g \tag{25}$$

Among them, P_{max}^g represents the maximum available output power of diesel generator, which is taken as 60 kW here.

5 Simulation Verification

Based on the aforementioned analysis, a simulation model has been developed, comprising four key components: the energy optimization management module, the distributed resource output module, the energy storage module, and the daily load module. The distributed resource output module incorporates the previously described models of photovoltaic systems, wind power generation, and diesel generators.

The daily load model is designed to simulate load variations under different operational scenarios. The energy storage module represents the energy absorption and release capabilities of energy storage vehicles or devices within the reconfigurable distribution network. The energy optimization management module is an optimization module that applies the bald eagle search algorithm. The overall simulation model is illustrated in Fig. 8.

The parameters mentioned above will continue to be used, and the values of the remaining parameters are shown in Table 5. The number of iterations is 50 times.

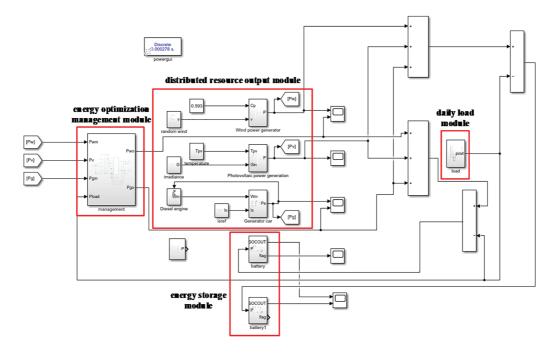


Figure 8: Overall simulation diagram of energy optimization control in the reconfigurable distribution network

Parameters	Value	Parameters	Value
α	2	k_1	0.75
a	10	k_2	0.5
R	1.5	k_3	-0.125
p_1	2	k_4	0.3
p_2	2	c_{v}	2
c_s	8	ω_2	0.6
ω_1	0.4		

Table 5: Simulation parameters

To investigate the applicability and generalizability of the optimization algorithm under different load conditions, simulation studies were conducted for two scenarios: a typical residential load and an industrial steel plant load. The results are shown in Fig. 9.

According to the simulation results, it is observed that before optimization, both wind power and diesel generator outputs operated at their maximum power levels. As shown in Fig. 9c,h, this resulted in the output power from distributed resources exceeding the energy storage system's capacity during the periods of 9–17 and 8–19 s, respectively. Simultaneously, Fig. 9e,j indicates that due to the high cost coefficient assigned to energy backflow from the storage system, the overall operating cost increased significantly during these intervals. Without appropriate control measures, such conditions may lead to power backflow and other operational issues that could jeopardize the stability of the reconfigurable distribution network.

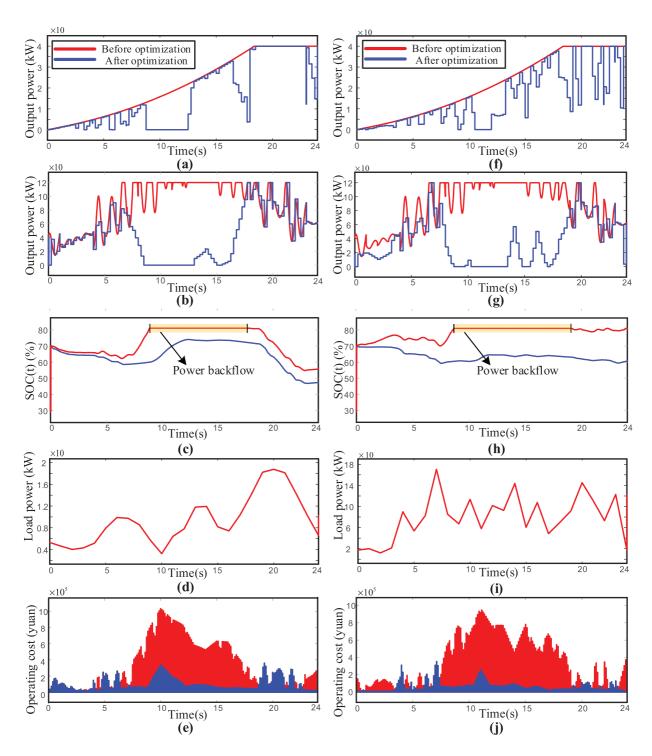


Figure 9: Energy optimization simulation results. (a) Optimization curve of diesel generator output; (b) Optimization curve of wind turbine output; (c) Energy storage system charge state change curve; (d) Ordinary residential load curve; (e) Comparison chart of operating costs of distribution network; (f) Optimization curve of diesel generator output; (g) Optimization curve of wind turbine output; (h) Energy storage system charge state change curve; (i) Steel plant load curve; (j) Comparison chart of operating costs of distribution network (The above figures all adopt a time scaling in which one hour is equivalent to one second)

After applying the optimization algorithm, Fig. 9a,b,f,g demonstrates that the outputs of wind and diesel generators are effectively adjusted in response to load variations. As a result, the energy storage system's SOC, shown in Fig. 9c,h, remains within the safe operating range of 30% to 80%. This achieves effective energy optimization management, prevents power backflow, and significantly reduces the operating cost of the reconfigurable distribution network. The simulation results confirm the effectiveness of the Bald Eagle Search algorithm in managing energy distribution under complex and dynamic conditions.

6 Conclusion

This paper applies the BES optimization algorithm to enhance energy management in reconfigurable distribution networks with high penetration of renewable energy, aiming to minimize operating costs while preventing power backflow. The study begins by establishing mathematical models for each component within the reconfigurable distribution network, followed by the formulation of an operating cost objective function that incorporates power backflow penalties. The BES algorithm is then employed to optimize energy redistribution effectively. Simulation results validate the proposed method's accuracy and effectiveness, demonstrating its potential to enhance both the economic performance and operational safety of high-renewable-penetration distribution networks. In future research, we plan to conduct comparative studies of various mainstream optimization algorithms focusing on aspects such as convergence speed and avoidance of local optima. Moreover, the proposed BES-based optimization framework could be further extended to explicitly address uncertainties in renewable generation and load demand. Potential approaches include scenario generation, which models multiple possible operating conditions; robust optimization, which ensures stable performance under worst-case scenarios; stochastic programming, which incorporates the probabilistic nature of uncertainties; and fuzzy control, which provides a rule-based way to handle imprecise or incomplete information. Integrating such techniques would enhance the adaptability and practical relevance of the proposed strategy in real-world reconfigurable distribution networks with high renewable penetration.

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Abbreviations

BES Bald Eagle Search
SOC State of Charge
PV Photovoltaic

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